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# Electrical resistivity of nickel, iron and iron-silicon alloy melts at high pressure with implications for the thermal conductivity of the Earth's core

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A thesis submitted in partial fulfillment of the requirements for the Doctor of Philosophy degree in Geophysics

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## Abstract

The Earth's liquid outer core (OC) is composed of Fe alloyed with up to 10% Ni and a small fraction of light elements. However, the effect of light elements such as Si on the transport properties of liquid Fe-alloy in Earth's OC is not clear. Thermal conductivity ( $\kappa$ ) and related electrical resistivity ( $\rho$ ) are the least constrained parameters in OC. Therefore, the characterization of transport properties of Ni, Fe and Fe-Si at high pressure has important geophysical implications for the Earth's core. The  $\rho$  of solid and liquid Ni, Fe and Fe 4%Si was measured at pressure and temperature up to 12 GPa and 2100 K, respectively. All experiments were conducted in a large volume multi-anvil press and the measurements were carried out using the new adaptation of the 4-wire method. A standard Consortium on Materials Properties Research in Earth Sciences (COMPRES) octahedron cell was used as the pressure medium, while the internal components were redesigned to permit the preservation of the liquid sample geometry, to contain the melt and minimize the effect of diffusive contamination. In the solid state, the  $\rho$  of solid Fe and Ni exhibits the familiar pressure-dependent decrease after the Curie temperature ( $T_c$ ). The anomalous  $\rho$  of Fe-4.5wt%Si above  $T_c$  is strongly modulated by temperature and pressure, and it is attributed to the phase transitions and structural ordering in the alloy. The  $\rho$  of liquid Ni remains constant at the onset of melting at all pressures. While  $\rho$  of liquid Fe decreases up to 5 GPa, it remains invariant along the melting boundary after the  $\delta$ - $\gamma$ -liquid triple point. The  $\rho$  of liquid Fe-4.5wt%Si remains constant along the melting boundary and matches 120  $\mu\Omega\text{cm}$  for pure liquid Fe within the experimental uncertainties. The results are interpreted in the context of pressure dependent icosahedral short range ordering (ISRO) in liquid 3d metals and alloys. Based on this, it is postulated that  $\rho$  of Fe-alloys along the melting boundary remains invariant up to Earth's inner core boundary. The  $\kappa$  at the core-mantle boundary and inner core boundary were calculated using the Weidemann-Franz law.

## **Keywords**

electrical resistivity, liquid transition metal, high pressure, Earth's core, nickel, iron,  
silicon

## Co-Authorship Statement

The core of this dissertation is based on three manuscripts:

1. **Chapter 2:** Silber, R. E., Secco, R. A. and Yong, W. (2017) Electrical Resistivity Measurements of Solid and Liquid Ni up to 9 GPa, JGR-Solid Earth, 122, doi:10.1002/2017JB014259
2. **Chapter 3:** Silber, R. E., Secco, R. A., Yong, W. and Littleton, J. (2018) Electrical resistivity of liquid Fe to 12 GPa: Implications for heat flow in cores of terrestrial bodies, Nature Scientific Reports, 8, 10758, doi: 10.1038/s41598-018-28921-w
3. **Chapter 4:** Silber, R. E., Secco, R. A., Yong, W. and Littleton, J. (2018) Heat flow in terrestrial cores from invariant electrical resistivity of Fe-Si on the melting boundary, manuscript prepared for submission to a peer-reviewed journal

In each of the studies above, I performed research that included design and fabrication of experimental components, running high pressure experiments in a 3000 ton multi-anvil large press, and carrying out post-experimental work (e.g., cell sectioning, microscope analyses). I analyzed the results, and was solely responsible for the interpretation of the results. I also wrote the manuscripts and subsequent revisions. Rick Secco provided instrumentation, materials and lab facilities and provided feedback on the manuscripts. Wenjun Yong (Chapters 2-4) and Joshua Littleton (Chapters 3-4) assisted with experiments and provided feedback on the manuscripts.

## **Dedication**

To my Family

## Acknowledgments

While they say that it is the journey and not the destination that matters, I would beg to disagree. There is a great sense of accomplishment when one successfully reaches that destination and opens up a new chapter. I want to express my deep gratitude to my thesis advisor, Dr. Rick Secco, who had a vision and enough confidence in me to entrust me with the project of this magnitude. I also want to thank Dr. Secco for his input and suggestions that greatly improved my published work. I would like to thank my Advisory Committee, Dr. Sean Shieh and Dr. Tony Withers, for their support. Furthermore, I would like to express my great appreciation to my colleagues, and present and past labmates, Dr. Wenjun Yong, Joshua Littleton, Dr. Tim Officer, and Dr. Innocent Ezenwa, for making this journey fun. My thanks also goes to Jon Jacobs for his assistance in experimental parts fabrication at the beginning of my journey. Also big thanks to Marc Beauchamp and Stephen Wood, who have helped me in my sample analyses. I would like to thank many academics, students and staff in the Department of Earth Sciences, whom I have interacted with over the years. I apologize for not naming you all, but you know who you are. Finally, I want to thank my wife and my children for their immense patience, love, and support that have made my success possible. Last, but not least, I want to thank (not) about 50 academics in the field of high pressure geophysics and related fields, for their “good manners” and “timely” responses to my postdoc inquiries, as those have steered me in the right direction after all. Sometimes trials and tribulations indeed make you a stronger character and a stronger researcher.

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## List of Symbols

$ e $	Electron mean free path
$A$	Area
$A_r$	Proportionality factor
$C_P$	Heat capacity at constant pressure
$D$	Sample length
$e$	Electron charge
$g$	Gravitational acceleration
$I$	Current
$k$	Boltzmann's constant
$k_F$	Fermi wave vector
$k_{total}$	Total experimentally measured thermal conductivity
$L$	Lorenz number
$L_o$	Sommerfeld value ( $2.44 \cdot 10^{-8} \text{ W } \Omega \text{ K}^{-2}$ )
$m^*$	electron effective mass
$n$	Charge carrier number density
$P$	Pressure
$q_{cond}$	Adiabatic heat flow
$R$	Resistance
$r$	Planetary core radius
$R_H$	Hall coefficient
$S_F$	Area of the Fermi surface
$T$	Temperature
$T_C$	Curie temperature
$T_m$	Melting temperature
$V$	Voltage
$v_F$	Fermi velocity

$\gamma$	Linear factor of temperature dependent electronic contribution to the heat capacity
$\varepsilon_d$	Energy of the d-band electrons
$\varepsilon_F$	Fermi energy
$\kappa$	Thermal conductivity
$\kappa_e$	Thermal conductivity, electronic component
$\kappa_p$	Phonon component of thermal conductivity
$\rho$	Electrical resistivity
$\rho_{\text{liquid}}$	Electrical resistivity in liquid
$\rho_{\text{solid}}$	Electrical resistivity in solid
$\sigma_e$	Electrical conductivity
$\tau$	Conduction electron relaxation time
$\phi$	Seismic parameter
$\hbar$	Planck constant
$\alpha$	Thermal expansion

# Chapter 1

## 1. Introduction

*Shall I refuse my dinner because I do not fully understand the process of digestion?*

- Oliver Heaviside

### 1.1. Background

High-pressure laboratory experiments aim to constrain the physical, chemical and structural properties of matter under extreme compression. However, despite continuous technological advances, high-pressure research faces a wide range of challenges. Some of those challenges stem from understanding the responses and the behavior of compressed matter on a quantum level to incorporating and interpreting that knowledge in order to understand the behavior of macrosystems under extreme pressures ( $P$ ) and temperatures ( $T$ ) in planetary interiors. Indeed, the parameters, such as physical, chemical and structural properties, strongly influence the behavior of transport properties. Recently, there has been a reinvigorated interest in thermal conductivity and related electrical resistivity of the iron (Fe) alloys in the Earth's core. These parameters are some of the least constrained quantities in mineral physics. For instance, the importance of thermal conductivity lies in the fact that it controls the spatio-temporal and thermal evolution along with dynamics of the core. It plays a role in the present-day heat flow out of the Earth's core and the type of convection of the liquid alloy that generates the geomagnetic field. Thermal conductivity also imposes a critical constraint on the age of the inner core and overall thermal and spatio-temporal evolution of the Earth's deep interior (Williams, 2018). Better understanding of thermal conductivity of the liquid outer core for example, enables more comprehensive knowledge on the core cooling process and the rate which in turn powers mantle convection, and subsequently plate tectonics. The rest of this chapter reviews the key aspects related to this work, starting with the properties of the Earth's interior.

## 1.2. The Earth's Core

Conceptually, the Earth's core may be considered analogous to a giant furnace that provides heat to the rest of the planet and plays an instrumental role in supporting the existence of life. The radius of the liquid outer core is  $3.485 \cdot 10^6$  m (e.g., Gubbins et al., 2015), while the radius of the comparatively smaller inner core is  $1.221 \cdot 10^6$  m. The total mass of the core is  $1.94 \cdot 10^{24}$  kg, while the mass of the outer core is  $1.84 \cdot 10^{24}$  kg (e.g., Davies, 2015). The volume occupied by the core is about 16.3% of the Earth's total volume. Furthermore, seismological observations show that out of that percentage, 15.6% belongs to the outer core and only 0.7% to the inner core (e.g., Zhang et al., 2016).

Due to experimental challenges, many of the core parameters remain poorly resolved. For example, the temperature at the core side of the core-mantle boundary (CMB) is not satisfactorily constrained. The estimates range from 3500 K to about 4500 K (e.g., Lay et al., 2008), although recent work helps narrow that temperature range from 4000-4500 K (Anzellini et al., 2013). The temperatures at the inner core boundary (ICB) are estimated to be 5500-6000 K (Anzellini et al., 2013).

It is well-established that in addition to ~5-10% of Ni (Poirier, 1994), the core contains a small amount of light elements that is necessary to account for the density in the liquid outer core and solid inner core that is about 8% and 4% less than in the density of pure Fe, respectively. Cosmochemical, geophysical and seismological constraints suggest that the light elements meeting that criterion are Si, S, C, O, H, and Mg (McDonough and Sun, 1995; Zhang et al., 2016; Litasov and Shatskiy, 2016; O'Rourke et al., 2017). However, the exact compositional makeup and ratio of those elements in the outer core are still strongly debated (e.g., Tateno et al., 2018). The presence of light elements is also considered to lower the melting temperature of Fe at the core conditions (Zhang et al., 2018).

Paleomagnetic evidence shows that the Earth's magnetic field has been in existence for 4.2 Gyr (Tarduno et al., 2015). It is generated by the convective motion of the liquid alloy in the outer core. The convective motion of the liquid alloy induces the current and it is



essentially a mechanism that converts the kinetic energy of the flow into generation of the magnetic field. The helical motion of the liquid metal alloy in the outer core is roughly co-axial with the Earth's rotational axis and forms tangent cylinders (Taylor columns) to the "stationary" inner core. However, during the cooling of the core, thermal conductivity regulates if the amount of heat conducted through the OC toward the CMB is adiabatic, super-adiabatic or sub-adiabatic through the outer core. The conductive regime dictates whether the convection is thermally or compositionally driven (e.g., Davies et al., 2015; Gubbins et al., 2015; Labrosse, 2015). If the conductive heat flow is sub-adiabatic, the core is thermally unstable, and the thermal convection is a dominant contribution to the overall convective process. This assumption was valid for low estimates of thermal conductivity (e.g., Stacey and Anderson, 2001; Stacey and Loper, 2007). However, recently revised values of high thermal conductivity strongly suggest that the main mechanism driving core convection comes from the compositional buoyancy flow. Freezing and growth of the inner core removes Fe from the molten alloy and frees up light elements that move upward from the ICB toward the CMB.

The situation is further complicated in terms of the energy budget of the core. High values of thermal conductivity require that the core cools at a fast rate, which leaves only limited energy budget for the geodynamo (Davies, 2015; Davies et al., 2015; Labrosse, 2015; Gubbins et al., 2015). The high thermal conductivity regime also suggests that the core temperature was much higher in the geological past, which is difficult to reconcile from a theoretical perspective. Moreover, high thermal conductivity suggests that the formation of the inner core took place relatively recently (~500 Myr) (Nimmo, 2015). A young inner core presents a significant complication, as its growth is closely tied to the compositional convection processes generating the geodynamo and the uninterrupted existence of the magnetic field throughout most of Earth's geologic time. Thus, accounting for the existence of the magnetic field in the past 4.2 Gyr is theoretically challenging in the presence of recent high values of thermal conductivity.

Mantle convection plays an important role in cooling of the outer core, and the lower mantle is important in the convection of the outer core liquid alloy as it modulates the amount of heat conducted across the CMB (Olson et al., 2015; Olson, 2016). However,

the heat flow across the CMB is not uniform (French and Romanowicz, 2015) and depends on the presence and distribution of heterogeneous regions such as D'', which have different composition and higher thermal conductivity than the rest of the CMB (Ammann et al., 2014). The recently discovered post-perovskite phase in the lower mantle (thought to be stable in D'') has significantly higher thermal conductivity than perovskite (Hirose et al., 2015). The presence of thermal heterogeneities in the lower-most mantle can disrupt potential stratification at the top most core (Davies et al., 2015). This agrees well with seismic measurements (e.g., Lay et al., 2008) indicating a well-mixed outer core. An additional uncertainty in the heat flow across the CMB comes from the Fe substitution in ferropericlase and the subsequent high to low spin crossover, which is capable of a drastic reduction in the value of thermal conductivity (Ohta et al., 2017). Recent models of mantle convection suggest that the mantle is capable of absorbing thermal energy from the core in the range 10-13 TW (Olson et al., 2015; Olson, 2016).

### **1.3. Thermal Conductivity and Electrical Resistivity of Liquid Transition Metals and Alloys at High Pressure**

#### **1.3.1. General Background**

To understand the behavior of liquid metals and alloys at extreme pressures and temperature conditions corresponding to the Earth's core, both experimental and theoretical efforts are necessary. Even though high-pressure science has experienced a significant development in the past several decades, direct experiments on liquid metals and alloys at the core conditions are still out of reach. Nevertheless, diamond anvil cell (DAC) experiments on solid matter can frequently reach the outer core pressure (e.g., Gomi et al., 2013; Ohta et al., 2016; Gomi and Hirose, 2015; Anzellini et al., 2013; Morard et al., 2018). Appreciable progress has also been made in theoretical and numerical approaches which can even simulate the conditions in the interior of "Super" Earths (e.g., Smith et al., 2018). However, the dynamics and structure of liquid transition metals under extreme pressures and temperatures are not entirely resolved. While

theoretical evaluation of transport properties of solids is more successfully achieved due to the advantages given by the translational symmetry and lattice periodicity over the long-range order, liquids are much more difficult to model. For example, the absence of long range order makes the job of simulating the electron scattering processes very challenging. However, there has been a significant development in recent years resulting from appreciably higher computational capacity and more sophisticated theoretical treatments of transport properties of liquids under high pressure. That is reflected in recent studies of electrical resistivity and thermal conductivity of Earth's outer core (e.g., de Koker et al., 2012; Pozzo et al., 2012).

From the fundamental perspective, pressure and temperature antagonistically compete for the control over transport properties of liquid transition metals and alloys. Pressure reduces the amplitude of ionic vibrations (reasonably analogous to the lattice vibrations in solids) and increases the parameters in inverse space, such as the size of the Brillouin zone (e.g., Templeton, 1966). Energy of atomic bonds is also modified by compression, because atoms come closer together. Conversely, temperature increases the amplitude of ionic vibrations in the liquid and increases the kinetic energy of the fluid components. The problem of fully characterizing transport properties in liquid metals under high pressure is not yet resolved completely. The structural and dynamical aspects of 3d-liquid transition metals and their alloys diverge from simple metals (e.g., Lee and Lee, 2016), especially under pressure. Some of those peculiarities in liquid transition metals, related to the existence of unfilled 3d bands, include the presence of the icosahedral short-range order (ISRO) structures. Because of their unique nature, the existence of these structures has been experimentally confirmed only in recent years (Schenk et al., 2002) and need to be included in evaluating the thermal conductivity and empirically related electrical resistivity of the Earth's core alloys.

### **1.3.2. The Relationship Between Thermal Conductivity and Electrical Resistivity**

Thermal conductivity ( $\kappa$ ) is inversely related to electrical resistivity ( $\rho$ ) through the Wiedemann-Franz law:

$$\kappa = LT/\rho \quad (1.1)$$

where  $L$  is the Lorenz number (corresponding to the theoretical Sommerfeld value,  $L_o = 2.44 \cdot 10^{-8} \text{ W } \Omega \text{ K}^{-2}$ ) and  $T$  is temperature. This relation is generally applicable to metals and alloys where transport of both charge and heat is achieved primarily by electrons. Electrical resistivity is determined from Ohm's law:  $\rho = \frac{V}{I} \left( \frac{A}{D} \right)$ , if the voltage ( $V$ ) drop measured across a sample with a current ( $I$ ) are experimentally known. The parameters in parenthesis represent the area  $A$ , perpendicular to long axis of the cylindrical sample with length  $D$ . This simple expression carries within it the elements of quantum mechanics, such as relaxation time between electron collisions and it holds for any conductive material, provided that the mean free path is well constrained.

The Earth's core cannot be sampled directly, and consequently almost everything that is known about its properties comes from indirect measurements such as seismic velocity measurement profiles, chosmochemical constraints and mineral physics. Iron meteorites might serve as reasonable proxies for core composition (McDonough and Sun, 1995). In the same context, the direct measurement of thermal conductivity of compressed solid and liquid metals at core conditions is very challenging (Konôpková et al., 2016). However, the measurements of electrical resistivity are significantly easier from the experimental perspective, but challenging nevertheless (Ohta et al., 2016).

### 1.3.3 Thermal Conductivity of Liquid Transition Metals

Thermal conductivity of liquid transition metals is substantially different from thermal conductivity in a crystalline state. In solid metals, for example, the lattice vibrations (or phonons) contribute substantially to thermal conductivity. However, in liquid metals, the contribution of (analogous) ionic vibration is negligible and heat transport is carried by electrons as noted earlier. This is advantageous as it allows the application of Wiedemann-Franz law to estimate the thermal conductivity at conditions where it cannot be directly measured. However, to do that, a reliable experimental value of electrical resistivity of liquid metal should be available. Nevertheless, that is not the only problem in determining thermal conductivity of liquid metals and alloys. The scattering of

electrons is relatively well understood in metals in the solid state (Abrikosov, 2017). The scattering contribution in ordered solids with long range order may be from impurities, electron-electron scattering, scattering by lattice vibrations and in ferromagnetic transition metals, scattering by magnons (Abrikosov, 2017). The scattering in liquid transition metals is greatly more complicated because of a highly disordered environment. While the scattering of electrons in molten metals and alloys may take place by ionic vibrations and electron-electron scattering, there are still mechanisms of electron scattering that are not well understood (Mott, 1972). Some of those scattering mechanisms can be attributed to the unfilled 3d electron band and inherently related local structures in the melts. Another scattering mechanism which may affect transport properties in molten metals and alloys is the presence of ISRO structures in liquid transition metals and alloys (Li et al., 2017). These structures have potential to affect the resistivity because they act as scattering centers.

Finally, at high pressures and temperatures in the outer core, the electron scattering might be inelastic where charge is preserved but not energy. Consequently, the value of the Lorenz number in the Wiedemann-Franz law would be affected and the value of thermal conductivity calculated from measured electrical resistivity would generally have a high degree of uncertainty (Williams, 2018). While this has been discussed extensively by Pourovskii et al. (2017) and Xu et al. (2018), the extent of inelastic scattering under core conditions still remains unresolved. Additionally, the presence of light elements is considered to increase the electrical resistivity (and subsequently decrease thermal conductivity), but their overall contribution to the liquid alloy behavior at high pressures is not clearly resolved.

#### **1.3.4 Experimental Measurements of Electrical Resistivity and Thermal Conductivity**

Early efforts in measuring electrical resistivity and evaluating thermal conductivity of Fe and Fe-alloys under very high pressures were limited to shock wave experiments (Keeler and Mitchell, 1969; Matassov, 1977; Bi et al., 2002). However, the values of thermal conductivity obtained from these shock wave measurements diverge significantly and it

is difficult to determine which value can be taken with a high degree of confidence. A recent trend in experimental measurements, initiated by Seagle et al. (2013) and Gomi et al. (2013), involves a DAC measurement of electrical resistivity on decompression. The resistivity values obtained at room temperature are then used in Bloch-Grüneisen equation to account for the effects of temperature on electrical resistivity. The subsequent values of resistivity at high temperatures were then used in the Wiedemann-Franz law to obtain thermal conductivity. While the effect of light elements on electrical resistivity at room temperature and pressure is significant, and justify the use of Matthiessen's rule (e.g., Gomi et al., 2013; Seagle et al., 2013; Gomi and Hirose, 2015; Gomi et al., 2016; Suehiro et al., 2017; Zhang et al., 2018), there are considerable doubts regarding its validity at high pressure and temperature (e.g., Gomi et al., 2016). The validity of the Bloch-Grüneisen formula in the liquid state, or even in the solid state at very high temperatures, is not clear especially in the case of the observed resistivity change at phase transitions, which may be associated with either increased or reduced structural ordering (e.g., Baum et al., 1967) and in the context of resistivity saturation. In principle, while the obtained values of both electrical resistivity and thermal conductivity in all these studies vary, the differences are usually within experimental uncertainties. Most of these studies report very low resistivity for pure Fe (generally below 90  $\mu\Omega\text{cm}$ ) and marginally increased resistivity for Fe-alloys. The low values of electrical resistivity in turn produce a high value of thermal conductivity in the outer core. However, in a recent study, thermal conductivity of pure Fe was measured at conditions close to the outer core (Konôpková et al., 2016). The results contradict the studies mentioned above and indicate that Fe at the core conditions may have very low thermal conductivity ( $33 \pm 7 \text{ W/mK}$ ), in line with earlier semi-theoretical estimates (e.g., Stacey and Anderson, 2001; Stacey and Loper, 2007). This indeed shows the need for a direct measurement of electrical resistivity of liquid Fe and its alloys at high pressure, as a sensible way to better constrain the value of electrical resistivity (and by extension, calculated thermal conductivity) in the liquid outer core. However, there are only very few examples of such studies (Secco and Schloessin, 1989; Ohta et al., 2016), with significantly diverging results. Of course, obtaining thermal conductivity from the measured electrical resistivity is predicated on the fact that the Wiedemann-Franz law holds to the core conditions.

## 1.4 Aim of This Thesis

The main aim of this work was to measure experimentally the high pressure electrical resistivity and evaluate thermal conductivity of solid and liquid transition metals Fe and Ni as the two main constituents of the Earth's outer core. The emphasis was placed on measuring electrical resistivity along the melting boundary (as a potential anchoring point analogous to the inner core boundary). This is in part motivated by the theoretical reasoning reported by Stacey and Anderson (2001) who suggested invariant electrical resistivity of simple metals along melting boundary. In addition, the goal was to resolve the behavior of the binary Fe-4.5wt%Si alloy, considering that Si is believed to be the dominant light element in the outer core (e.g., Litasov and Shatskiy, 2016). Better understanding of thermal conductivity of the liquid outer core, for example, enables more comprehensive knowledge of the core cooling process and the rate which in turn powers the mantle convection, and subsequently plate tectonics.

The electrical resistivity of solid and liquid Ni was investigated first (Chapter 2), as Ni is an electronic analogue of Fe. The potential scattering mechanisms contributing to electrical resistivity of liquid transition metals at high pressure along the melting boundary were examined. Subsequently, the electrical resistivity of solid and liquid Fe at pressures up to 12 GPa was measured and values were used to calculate temperature dependent thermal conductivity values (Chapter 3). The implications were examined with respect to small planetary bodies and moons in the solar system.

Finally, measurements of electrical resistivity on solid and liquid Fe-4.5wt%Si were done at pressures 3-9 GPa (Chapter 4). The behavior of electrical resistivity along the melting boundary was compared with the behavior of Ni and Fe. Based on the results obtained in this work, a new mechanism is proposed which governs the electrical resistivity of liquid Fe and its alloys to the inner core conditions. The reasoning based on these results and recent developments in understanding the structural and dynamical properties of liquid transition metals along the melting boundary will be extensively discussed in later chapters in this thesis. It should be noted that the mechanism contributing to the electrical resistivity of transition metals, and in particular Fe and its alloys, along the melting

boundary, has never been examined previously. To the best of my knowledge, this work is indeed the first ever to consider the effects of local short-range ordering on electrical resistivity of liquid transition metal and alloy at high pressure.

The conclusions and the recommendations for future work are presented in Chapter 5. This thesis also includes Appendix, with additional figures illustrating the methods and the consistency of parts fabrication.

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## Chapter 2

### 2. Constant Electrical Resistivity of Ni Along the Melting Boundary up to 9 GPa

*The scientists of today think deeply instead of clearly. One must be sane to think clearly, but one can think deeply and be quite insane.*  
- Nikola Tesla

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#### 2.1. Introduction

Recent advancements in both theoretical and experimental techniques at core-relevant pressure ( $P$ ) and temperature ( $T$ ) conditions have resulted in revised estimates of core electrical resistivity (Pozzo et al., 2012, 2013; de Koker et al., 2012; Gomi et al., 2013; 2016; Gubbins et al., 2015; Ohta et al., 2016) which are lower than that previously accepted (Stacey and Anderson, 2001; Stacey and Loper, 2007). These lower values of electrical resistivity require higher than expected values of thermal conductivity, in excess of  $90 \text{ Wm}^{-1}\text{K}^{-1}$  as calculated by Pozzo et al. (2012), deKoker et al. (2012) and Gomi et al (2013).

Conversely, the results from the most recent experimental work on solid iron (Konôpková et al., 2016) indicate that the thermal conductivity of iron at the core-mantle boundary (CMB) and the inner core boundary (ICB) is  $33 \text{ Wm}^{-1}\text{K}^{-1}$  and  $46 \text{ Wm}^{-1}\text{K}^{-1}$ , respectively. These values are close to the earlier estimates by Stacey and Loper (2007). Notably, Gomi et al. (2016) obtained the electronic thermal conductivity at the CMB from electrical resistivity measurement that is a factor of three higher than the direct experimental measurements of total thermal conductivity by Konopkova et al. (2016).

The possible reason(s) for the discrepancy between the two difficult-to-make experimental studies has been discussed (Dobson 2016) but is yet to be resolved. High values of core thermal conductivity yield high values of core adiabatic heat flux (Nimmo, 2015; Davies et al., 2015; Olson, 2016). Further review and discussion on thermal models of core evolution and implications of thermal conductivity on core ages are given by Davies et al. (2015) and references therein. The implications of these recently revised parameter values have non-trivial impact on core evolution and energetics and involve such fundamental questions as the age of the inner core and the main power source for the Earth's dynamo (Gubbins et al., 2015).

The secular cooling of the core and the release of light elements along with latent heat of crystallization at the ICB (Labrosse et al., 2001) drive the magneto-hydrodynamic convective processes in the outer core and are instrumental in generation of the geodynamo (Labrosse and Macouin, 2003). The thermal power available to drive the geodynamo comes from the heat flow by convection in excess of the heat conduction down the adiabatic gradient (Stevenson, 2003; Labrosse, 2003; Nimmo, 2007). A geodynamo powered mainly by compositionally-induced buoyancy or chemical convection requires an inner core (IC) at least as old as the geomagnetic field. Recent studies have shown the field has existed for at least 3.5 Ga (Tarduno et al., 2010; Biggin et al., 2011) and perhaps as long as 4.2 Ga (Tarduno et al., 2015). Recent simulations suggest the dynamo underwent a transition from weak-field non-dipolar dynamo to strong-field dipolar dynamo at a 650 Ma, which was interpreted as a signal of the nucleation of the IC (Driscoll, 2016). In addition, mantle global circulation models yield internally consistent estimates for the time variations in heat loss from the core, which is critical input for calculating the evolution of the core, and predict the age of the IC to be 0.4 - 0.95 Ga for the case of no radioactive heating in the core (Olson, 2016). This discrepancy in IC age estimates and geomagnetic field age appears to call on thermal convection as a major contributor to the geodynamo energy balance. If heat loss from the core is taken to be known, then thermal conductivity of the core is thus a key parameter in assessing the adiabatic heat flux in the core which allows the heat flux carried through convection to be calculated.

Stacey and Anderson (2001) presented an elegant thermodynamic argument which suggested that the electrical resistivity for pure metals is constant along the melting curve. The electronic component of the thermal conductivity  $\kappa_e$ , of a metal can be calculated from electrical resistivity using the Wiedemann-Franz law,  $\kappa_e = LT/\rho$ , where  $L$  is the Lorenz number (with a theoretically defined constant value called the Sommerfeld value,  $L_0$  of  $2.44 \cdot 10^{-8} \text{ W}\Omega/\text{K}^2$ ) and  $\rho$  is the electrical resistivity. A constant value of electrical resistivity on the melting boundary of a metal, where liquid structural effects are absent at sufficiently high pressures, may be a powerful means to apply robust low pressure determinations of electrical resistivity to ICB conditions. Making some reasonable assumptions for a value for  $L$  for Fe (Secco, 2017), thermal conductivity at the ICB could thus be calculated from low pressure measurements of electrical resistivity of Fe on its melting boundary (Powell, 1953; van Zytveld, 1980; Secco and Schloessin, 1989).

The aim of this study is to test experimentally the validity of the Stacey and Anderson (2001) and Stacey and Loper (2007) postulates. More broadly however, we embark on a new approach that has potential to contribute indirectly toward the resolution of the “new core paradox” (Olson, 2013) by investigating experimentally the electrical resistivity of solid and liquid Ni in the range of 3 to 9 GPa. The “new core paradox” refers to the energy deficit for the generation and maintenance of magneto-hydrodynamic convection necessary to sustain the geodynamo prior to the nucleation of the IC (Olson, 2013).

Ni has an electronic structure of  $[\text{Ar}] 4s^2 3d^8$  and was selected as a lower melting temperature analogue to Fe ( $[\text{Ar}] 4s^2 3d^6$ ) and for its similarities of ferromagnetic and paramagnetic states. Furthermore, Ni is integral to both the inner and the outer core (Poirier, 1994; McDonough and Sun, 1995) and its alloying with Fe increases the stability field of the high pressure phase relative to pure iron (Lin et al., 2002). The presence of 5.5% of Ni in the core does not affect the hcp structure of the Fe alloy (Tateno et al., 2012). Moreover, because of the similarities between Fe and Ni, ab-initio calculations demonstrate that at high  $T$ , the seismic properties of Fe-Ni alloys are almost indistinguishable from those of pure Fe (Martorell et al., 2013; Davies et al., 2015). In addition, both Ni and Fe have similar behaviour of their melting curves (Japel et al.,

2005) that can be attributed to their d-electrons. Ross et al. (2007) predicted that partially filled d-shells lower the energy of the liquid state at the onset of melting leading to a loss of d-band structural periodicity compared to filled d-band metals (Japel et al., 2005). This lowers the melting slope and may be characteristic of a select group of late transition metals with partially filled d-bands. The partially filled d-band also has an impact on compressibility and internal pressure anomalies, as observed in liquid Fe and Ni (Steinemann and Keita, 1988). In contrast, the density of states (DOS) of Cu, with a filled d-band, changes only slightly upon melting (Williams and Norris, 1974). The melting line of Cu is much steeper than the melting lines of Ni and Fe.

The electronic structure of Ni (e.g., Busch et al., 1974; Waseda and Tamaki, 1975) and its transport properties (Evans and Jain, 1972; Laubitz et al., 1976) have been the subject of numerous theoretical and, to a lesser degree, experimental studies. The Ni melting curve has also been investigated theoretically (some recent studies include Luo et al. (2010) and Pozzo and Alfe (2013)) and experimentally (some recent studies include Japel et al. (2005) and Ross et al. (2007)) although they are not always in complete agreement. The 1 atm electrical resistivity of liquid Ni has been investigated both theoretically (Fujiwara, 1979) and experimentally (e.g., Güntherodt et al., 1975). However, theoretical treatments of the transport properties of liquid Ni were unable to replicate the experimental values with any appreciable degree of success. In terms of experimental investigation of Ni resistivity at high  $P$ , there has been very little reported since Bridgman (1952). The more recent high  $P$  studies (Yousuf et al., 1986; Sundqvist, 1988; Decker and Chen, 1992) were focused on the lower  $T$  regime around the Curie temperature,  $T_C$ , and relatively low  $P$  of up to 5 GPa. We are not aware of any experimental study of electrical resistivity of liquid Ni at high  $P$ , and so were motivated to measure this transport behavior along its melting boundary in the context of the Stacey and Anderson (2001) and SL 2007 predictions as well as thermal conductivity of terrestrial planetary cores.



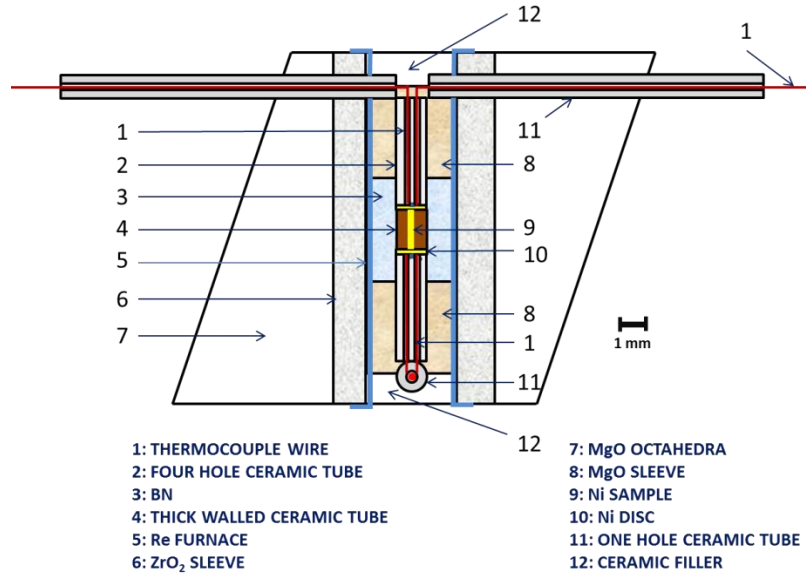
## 2.2. Methods

The experiments were carried out using a 3000-ton multi-anvil large volume press with the capability of fully automated pressure control and adjustable rates of heating. The technical details of the press and its pressure calibration at room and high  $T$  have been described elsewhere (Secco and Yong, 2012; 2016; Secco and Sukara, 2016). Detailed expositions on the multi-anvil pressure cell design, materials, properties and applications have been given by others (Frost et al., 2004; Leinenweber et al., 2012; Shatskiy et al., 2011). For the specific experimental  $P$  and  $T$  conditions of this study, three important experimental challenges had to be considered: i) control over the molten metal sample containment and geometry; ii) reactivity with, and diffusion of, molten metal into its container; iii) thermocouple/electrode - molten sample contamination. Each of these problems was overcome as described below.

The main pressure medium was a semi-sintered MgO octahedron doped with 5%  $\text{Cr}_2\text{O}_3$  with an edge length of 18 mm as shown in Figure 2.1. A hole was drilled between two parallel faces of the octahedron to accommodate a  $\text{ZrO}_2$  sleeve which acted as thermal insulation. Inside the  $\text{ZrO}_2$  sleeve were three stacked sleeves, each of 4 mm length. The two outer sleeves (Figure 2.1) were MgO and the inner sleeve was hexagonal boron nitride (hBN). Prior to cell assembly, hBN and two MgO sleeves, along with the  $\text{ZrO}_2$  hosting sleeve, were baked separately in a high temperature oven at 1073 K for approximately 12 hours to remove any volatile phases including organic, hydrous or other contaminants.

To maintain the geometry of the sample during the melt phase, a thick walled  $\text{Al}_2\text{O}_3$  tube, was used as the Ni sample container. A sample of 0.19 mm in radius and 1.50 mm in length was cut from high purity Ni wire (Alfa Aesar, 99.99%). The sample length was cut longer than the sample container by 0.05 mm on each end. The purpose was to ensure good electrical contact with electrodes made of thermocouple (TC) wire. Before emplacement into the ceramic tube, the Ni sample was lightly polished and cleaned with alcohol to remove any oxidation and surface contaminants. The sample container and thick walled ceramic tube was also carefully cleaned. The same procedure was repeated

on two Ni discs, having the same purity as the sample wire and with a diameter of 1.25 mm and thickness of 0.25 mm, placed between the sample end and the thermocouple junction. The discs were used to ensure good electrical contact between the sample and a geometrically imperfect TC junction of overlapping W5%Re and W26%Re wires.



**Figure 2.1: Cross-section of the experimental pressure cell.**

The discs also provided an initial barrier for inter-diffusion of Ni and TC in the melted sample phase without affecting the initial voltage drop across the sample, and consequently the measurement of electrical resistivity. The overall total resistivity contribution of the discs was calculated to be  $\sim 1\%$ . This is because the area of the disc is much larger than that of the sample, and its thickness is very small relative to the length of sample. When the total resistivity is calculated (adding  $\rho$  of discs and  $\rho$  of the sample), the contribution of the discs to the total  $\rho$  is negligible. In the first 2 – 3 seconds following melting, the contribution to the voltage drop across the sample by W and Re contamination was negligible because of the relative size of the contact disc area compared to the sample. Thus, the resistivity obtained in the initial stage of melting comes almost entirely from the contribution of the cylindrical Ni sample. The diffusion of W and Re from the TC into the liquid sample progressed with time; however, this

approach enabled the acquisition of accurate resistivity data on Ni at the moment of melting which was the focus of this study.

W26%Re / W5%Re wires of 0.20 mm diameter were used as both thermocouples and electrodes in the 4-wire resistivity measurement method employed in this study. Thermocouple wires were threaded through 4-hole  $\text{Al}_2\text{O}_3$  tubes which were symmetrically emplaced within the MgO sleeves. Using a microscope and purpose-built tool, a small indent was drilled in the bottom of each  $\text{Al}_2\text{O}_3$  tube on the side oriented toward the Ni disc and the sample, which hosted the TC junction. This prevented an excess of TC wire from protruding from the 4-hole ceramic tube and altering the sample geometry. Melt containment was achieved between the 4-hole  $\text{Al}_2\text{O}_3$  tube hosting the TC and the thick walled  $\text{Al}_2\text{O}_3$  tube hosting the sample by minimizing the internal free volume on cell assembly.

Resistive heating was achieved by using a Re cylindrical furnace that was emplaced within the  $\text{ZrO}_2$  cylinder. In initial test runs, the maximum temperature difference between the two TC's located at each end of the 1.50 mm long sample was observed to be  $\pm 50$  K at temperatures up to 2000 K. The assembled octahedral pressure cell was placed in a vacuum furnace at  $\sim 420$  K for 12 – 24 hours to remove volatile phases and other contaminants.

Following slow pressurization to the desired level, a fast rate of heating of up to 300 K/min was employed, during which data were collected in the voltage drop mode across the sample and in TC mode to record the temperature. The reason for the rapid heating and data collection was to minimize diffusive processes between the thermocouples and the sample. A manual switch was used to alternate between the two modes. In the TC mode, the thermal EMF corresponding to temperature was recorded and later converted to the actual temperature using an in-house algorithm for type C thermocouples. Pressure correction was not applied for type C thermocouples.

In the voltage drop mode, a constant DC current of 0.5 A was passed through one leg of the TC, through the sample and out through the same wire type leg of the other TC. The DC power source was a Keysight B2961A and DC voltages were recorded using a

Keysight 34470A digital multimeter and associated BenchVue software. Voltage drop data were acquired in the solid state only when the temperature during heating was stabilized. Temperatures in the melt were held for 20 – 40 s and the data were acquired rapidly using the high data acquisition rate (up to 20 Hz) of the Keysight 34470A meter. A manual polarity switch was used to mitigate any possible voltage contribution due to the temperature differences between two thermocouple junctions and any other parasitic voltages. The positive and negative polarity voltage drop data were averaged before calculating resistance. Following excursion into the liquid phase, the  $T$  was quenched by shutting off the furnace power.

The recovered samples were ground to obtain a section parallel to the long axis of the cylindrical sample so that the sample could be optically and chemically analyzed. The dimensions of the recovered sample were compared with the initial pre-experiment values and while no appreciable changes in dimension were observed under the optical microscope, the effects of thermal expansion and compressibility were included in the overall error calculation discussed in the next section. The recovered samples were investigated by wavelength dispersive X-ray spectroscopy using a JEOL JXA-8530F field-emission electron microprobe (EMP). An accelerating voltage of 20 kV, and a probe current of 50 nA, were used for all composition analyses.

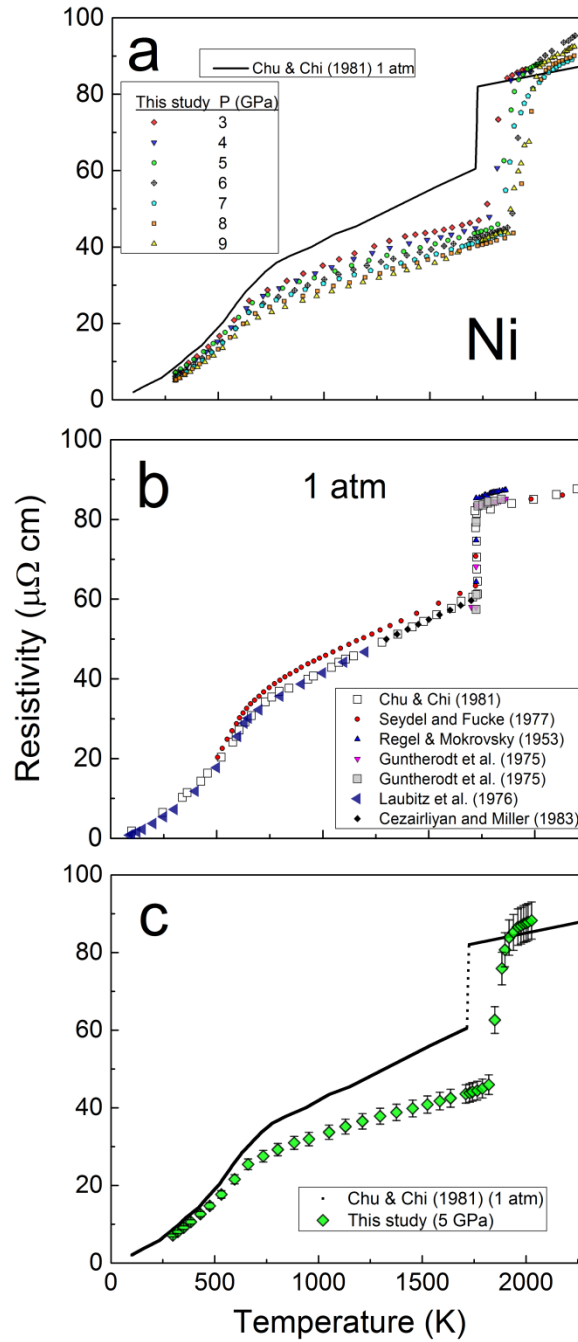
The electrical resistance was calculated from Ohm's law. After comparison of the initial and recovered sample dimensions, the electrical resistivity of both solid and liquid states of Ni was determined. The resistivity was calculated from Pouillet's law,  $\rho = \frac{RA}{D}$ , where  $\rho$  is the resistivity of the sample,  $R$  is the sample resistance, and  $A$  and  $D$  are the area and length of the cylindrical wire sample, respectively. The uncertainty in the sample dimensions corresponds in part to uncertainties in caliper and microscope measurements. The most significant error in sample length however, came from the difficulty in distinguishing the shape of the boundary between the thermocouple and recovered melted sample. That error was negligible in the solid, and estimated to be up to a factor of five times that of the standard length uncertainty in the liquid state (in the extreme case). The significantly larger error bars in the liquid state data reflect that. In principle, thermal

expansion at high  $T$  and compressibility at high  $P$  are antagonistic effects but they are not cancelling and cannot be neglected. The errors due to thermal expansion and compressibility were less than the uncertainties in length measurement and were included in the final error calculations.

The standard temperature uncertainty in a type C thermocouple is  $\pm 4.4$  K at 698 K and about 1% at high temperatures. The primary contribution to  $T$  uncertainty in this study comes from the related uncertainty in TC wires at high  $P$  and  $T$ . The error due to thermal gradients was negligible in the lower temperature range and taken into account in the higher temperature range. The maximum error contribution of the diffusion buffer Ni discs to the measured electrical resistivity of the sample was evaluated to be 1.2%. The thermal pressure effect to the overall pressure uncertainty, while very small, was included in the overall error estimates. A standard error calculation and propagation was carried out according to the formalism of Bevington and Robinson (2003). The contribution of the diffused W and Re in the Ni sample following the initial melting is addressed in the next section. The actual effect of alloying on the observed electrical resistivity, deeper in the temperature range of the melt, is addressed via its effect on the  $T$ -coefficient of resistivity.

### 2.3. Results

The  $T$ -dependence of electrical resistivity of both solid and liquid Ni at pressures in the range 3 – 9 GPa are shown in Figure 2.2a. The high  $P, T$  data are shown in comparison to the 1 atm data recommended by Chu and Chi (1981) and other studies at atmospheric pressure are shown in Figure 2.2b. Throughout the pressure range discussed here, and in the solid state temperature regime, our measured electrical resistivity data of Ni are self-consistent and exhibit the expected  $T^2$  dependence (Calandra and Gunnarsson, 2002) in the ferromagnetic state prior to the linear trend observed above the Curie temperature ( $T_C$ ). The electrical resistivity of solid Ni decreases with increasing pressure which is characteristic of most metals (Bridgman, 1952).



**Figure 2.2:** (a) The  $T$ -dependence of electrical resistivity of solid and liquid Ni at pressures in the range 3 – 9 GPa compared with the resistivity at 1 atm. (b) The  $T$ -dependence of electrical resistivity of solid and liquid Ni at atmospheric pressure from various studies [Chu and Chi, 1981; Seydel and Fucke, 1977; Güntherodt et al., 1975; Laubitz et al., 1976; Cezairliyan and Müller, 1983. Güntherodt et al. (1975) provides two datasets. The data from Regel and Mokrovsky (1953) are as

**cited in Seydel and Fücke (1977). (c) Representative error bars for 5 GPa run (error in  $T$  is within the symbol size).**

We note, however, that the slope of electrical resistivity at high pressure between the Curie temperature and melting is lower than that determined at atmospheric pressure. The most likely reason is that above the Curie temperature, the long-range order of spin magnetic moments is lost by the effects of temperature, and electron scattering by magnons becomes greatly reduced. With higher temperature, magnetic moments are increasingly destroyed, and consequently the compressibility is increased (as one of the primary static properties controlled by d-electrons). This allows pressure to reduce the amplitude of phonon vibrations more effectively in a way that temperature cannot compensate, but also allows for pressure-induced modifications of the Fermi surface. Furthermore, pressure acts in such way, that it reduces the density of states through band splitting. Together, these factors account for the lower slope of electrical resistivity above the Curie temperature in the high pressure datasets compared to the 1 atm dataset.

At the onset of the liquid region, there is a significant jump in resistivity. The electrical resistivity curves of liquid Ni are also well-behaved with linear trends as shown in Figure 2.2a, clearly indicating the melt was contained. Earlier cell designs that showed post-recovery evidence of liquid Ni leakage and sample geometry disruption had irregular resistivity behaviour in the liquid region that was a revealing sign of liquid sample breach of its container boundaries. Remarkably, at the moment of complete melting, the electrical resistivity is constant at different pressures within the experimental uncertainties. This means the electrical resistivity of liquid Ni is invariant along the melting curve up to 9 GPa, which is the main result of this study.

The pressure effects on the resistivity observed in this study are consistent with the pressure effects on the resistance of Ni observed by Sundqvist (1988) and Decker and Chen (1992), despite different experimental methodologies and relatively narrow  $P$ - $T$  ranges adopted in their studies. In general, the decrease of electrical resistivity in the solid state in the  $P$ -range of 3-9 GPa is linear and it is consistent with the observed behaviour in resistance reported by Pu (1991). Figure 2.2c displays the representative calculated

error bars from different sources as discussed in the previous section. The error bars due to the uncertainty in temperature are small and are within the symbol size.

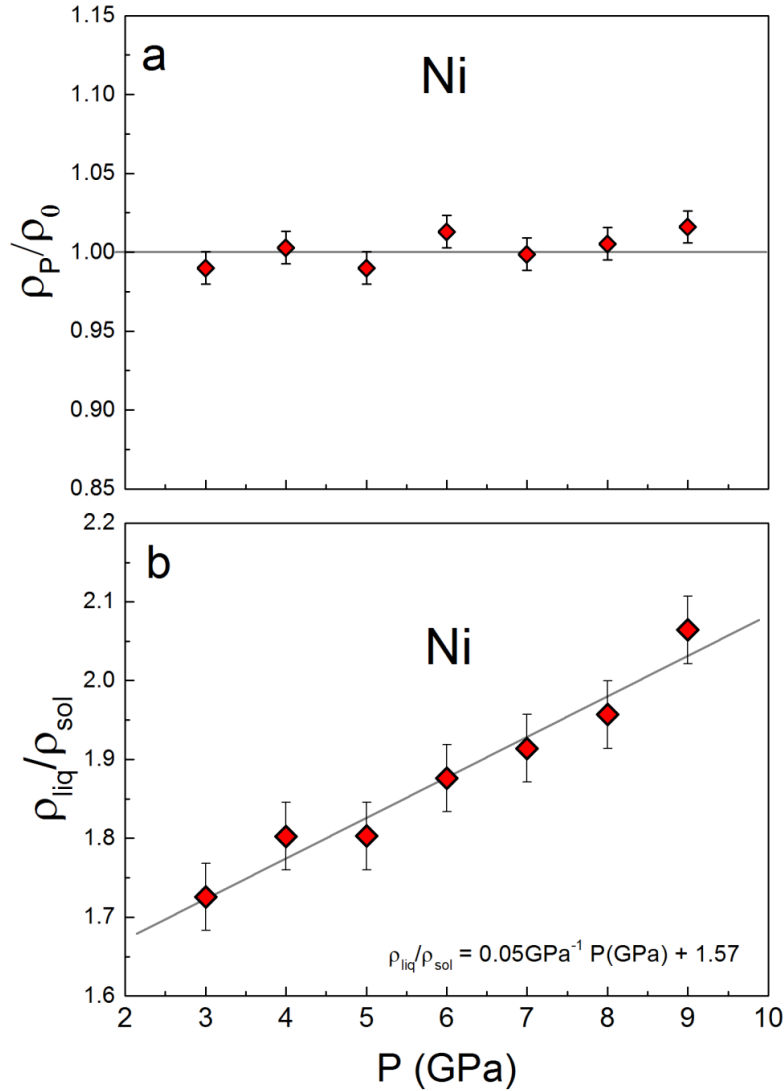
At the onset of the melting, the resistivity behavior is characterized by a rapid increase in resistivity of a magnitude consistent with the jump observed at 1 atm. The continuous increase in resistivity on increasing temperature during melting in our data, in contrast to the apparent near vertical jump in the 1 atm data, can be interpreted as likely indication of the presence of  $T$ -gradients in the cell which are exacerbated by a rapid rate of heating through melting. The resistivity continues to rise as the sample progressively melts over a narrow range of temperature and then assumes a different, that is, linear  $T$ -dependence in the completely molten phase. The ratios of the electrical resistivity of the molten Ni on the melting boundary at pressures in the range 3 – 9 GPa to the 1 atm value (Chu and Chi, 1981) hover around unity (Figure 2.3a) which demonstrate the invariance of resistivity along the melting boundary.

Our initial resistivity values in the liquid are in good agreement with those of Seydel and Fücke (1977) and Güntherodt et al. (1975). Another relevant finding in this study is illustrated in Figure 2.3b, where the ratio of the liquid to solid electrical resistivity at the melting temperature increases linearly and rapidly as plotted as a function of pressure. This is discussed later in connection with the effects of  $P$  on the DOS at the melting point.

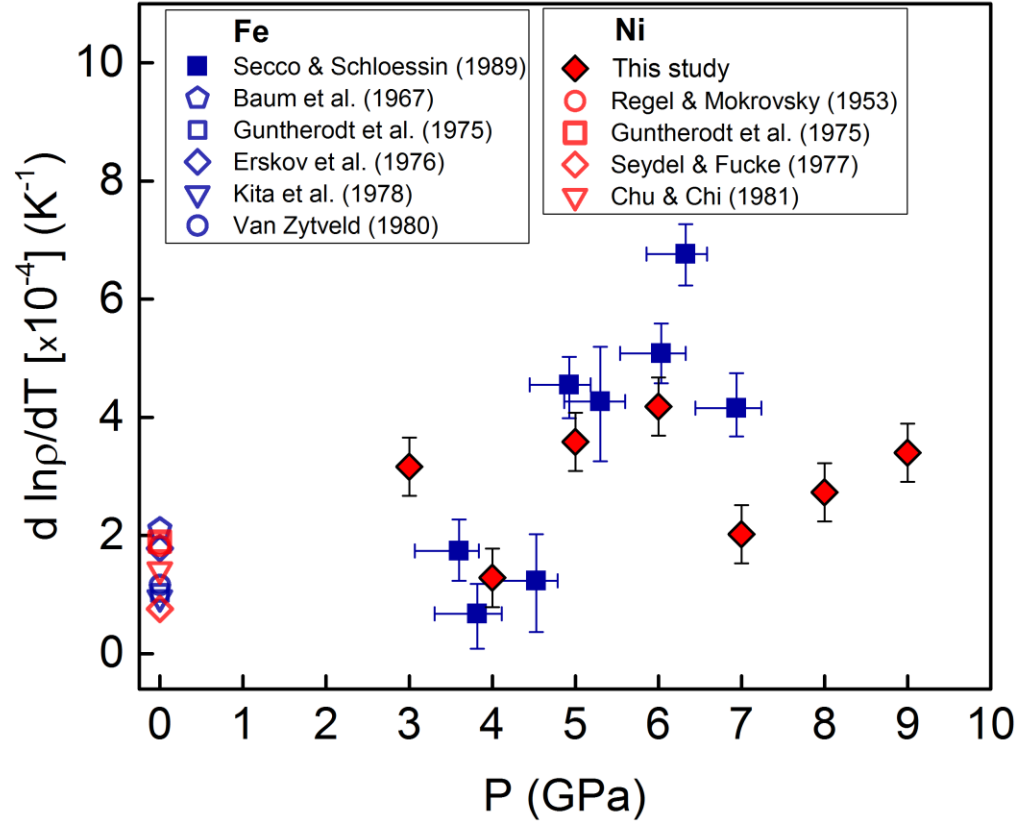
The  $T$ -coefficients of resistivity in the liquid state,  $(d\ln\rho/dT)_P$  obtained in this study are plotted in Figure 2.4 and are compared with 1 atm studies. Although there is some variation in values in the high pressure range, our values are in general agreement with 1 atm values. Our data for Ni are also compared with similar data for Fe at high pressure in Figure 2.4. Both transition metals have generally similar values of  $(d\ln\rho/dT)_P$  in the liquid state providing further evidence of the similarity of charge transport behavior in liquid Ni and Fe. The jump in values for Fe at ~5 GPa was interpreted to result from the changes in short range atomic structural order in the liquid at the triple point in the  $P$ ,  $T$  phase diagram caused by different parent solid structures (Secco and Schloessin, 1989) and later supported by measurements of other physical property changes in the liquid at 5 GPa



(Sanloup et al., 2000; Terasaki et al., 2002), but Ni does not show any solid state polymorphism in the range of pressures investigated here. The variability of  $(d\ln\rho/dT)_P$  for molten Ni may be an indication of the effects of diffusion of TC metals into the liquid sample.



**Figure 2.3:** (a) The ratio of the electrical resistivity of molten Ni on the melting boundary at pressures 3 – 9 GPa ( $\rho_P$ ) and at ambient pressure ( $\rho_0$ ) (Chu and Chi, 1981). (b) The ratio of electrical resistivity of liquid Ni to that of solid Ni before melting as a function of pressure.



**Figure 2.4:** The temperature coefficient of electrical resistivity,  $(d \ln \rho / dT)P$ , plotted for liquid Ni for pressures from 3 GPa to 9 GPa. Error bars in pressure are within the symbol size. The  $d \ln \rho / dT$  values for Ni are compared to values for liquid Fe in a similar pressure range [Secco and Schloessin, 1989]. Additional comparison is made with the  $d \ln \rho / dT$  at atmospheric pressure for both liquid Ni and Fe, derived in earlier experimental work (Baum et al., 1967; Güntherodt et al., 1975; Kita et al., 1978; Seydel and Fucke, 1977; van Zytveld, 1980; Chu and Chi, 1981). The data point from Erskov et al. ([1976] is as cited in van Zytveld (1980), and the data point from Regel and Mokrovsky (1953) is as cited in Seydel and Fucke (1977).

On the other hand, assuming that Matthiessen's Rule is valid in liquid Ni (e.g., Matthiessen and Vogt, 1864; Zinov'ev et al., 1972; Stacey and Anderson, 2001), and comparing the  $T$ -coefficient of electrical resistivity of Re and W in the high  $T$  solid state

(Powell et al., 1963; Desai et al., 1984) with that of liquid Ni at high pressures, there is a notable similarity. It is possible that the contribution for the higher value of slope of electrical resistivity of liquid Ni comes from the diffusion of W and Re into molten Ni. While we make a note of this behavior, further study is needed to quantify it. Obviously, the diffusion and dissolution of TC metals in liquid Ni (Natanzon et al., 1992) is a problem if one wants to determine electrical resistivity of pure Ni at higher temperatures in the melt. However, during initial test runs, Ni sample was rapidly heated to the melting point at pressure and quenched immediately. The subsequent EMP analysis showed only limited surface/grain boundary diffusion, but neither W nor Re was dissolved in the sample. This demonstrates that, in the presence of a Ni disc and rapid heating with rapid data acquisition, the initial few electrical resistivity points in liquid Ni (Figure 2.2a) come only from the Ni sample contribution and are not affected by any diffused W and Re. Indeed, the self-consistency of the data presented here seems to confirm that. This also confirms that there is no appreciable W or Re diffusion in the Ni sample in the solid state at high pressure which is consistent with the results of an earlier study that pressure has a retarding effect on diffusion of Re in solid Ni (Watson et al., 2008). This highlights the important role of the Ni disc in mitigating any potential diffusion from the relatively small area of the TC tip.

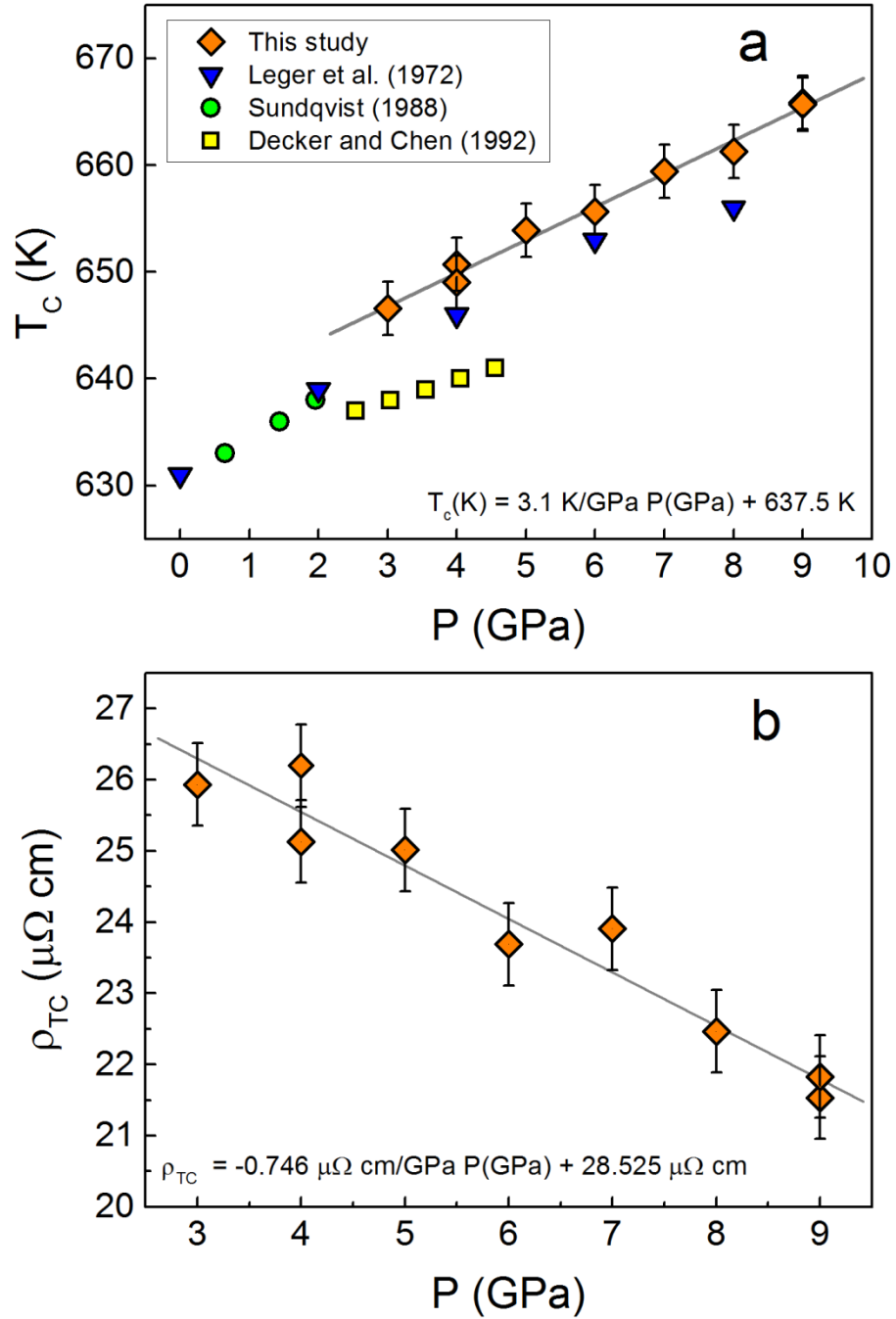
It should be noted however, that in the recovered samples of the initial test runs (data from which are not reported here) which were kept in the melt between 200 to 300 s, the maximum combined content of W and Re in the recovered Ni sample never exceeded 50 wt% (~25 at.%). During that prolonged time in the melt, the content of W and Re stabilized to a value close to the saturation limit of W in molten Ni (Natanzon et al., 1992). However, the EMP results obtained from sectioned samples recovered from test runs, heated up to 2173 K and held for up to 300 s in the melted sample phase, showed no appreciable  $\text{Al}_2\text{O}_3$  contamination in the sample.

The variation of the Curie temperature of Ni is plotted against pressure in Figure 2.5a. The Curie temperature was obtained by resistivity curve fitting and then taking the second derivative in the region between 500 K and 800 K. The Curie temperature of Ni increases with increasing pressure as also reported by Decker and Chen (1992) and

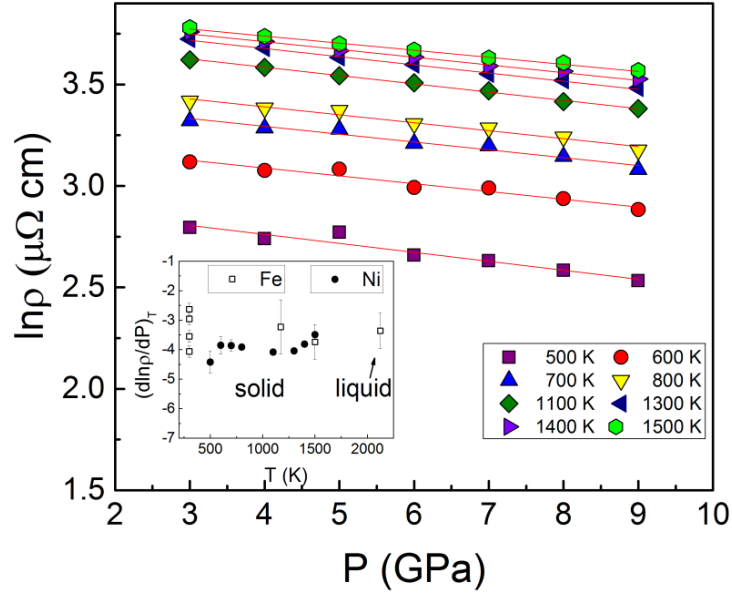
Sundqvist (1988). The overall trend agrees reasonably well with the literature values, within the uncertainty reported in this study demonstrating the well-known positive pressure effect on the Curie temperature (Bloch and Pauthenet, 1965; Leger et al., 1972; Sundqvist, 1988; Decker and Chen, 1992). Figure 2.5b shows the resistivity at  $T_C$  with increasing pressure. The overall decrease of the resistivity at  $T_C$  with respect to pressure is consistent with the earlier observations (Sundqvist, 1988; Decker and Chen, 1992).

Pressure coefficients of electrical resistivity,  $(d\ln\rho/dP)_T$ , were determined from the  $\ln\rho$  vs.  $P$  slopes for temperatures between 500 and 1500 K and are shown in Figure 2.6. Above the Curie temperature, the value of pressure coefficients of electrical resistivity remains relatively constant. In the inset of Figure 2.6, values of  $(d\ln\rho/dP)_T$  for Ni are compared with values for Fe (Secco and Schloessin, 1989) and the agreement between the two metals provides consistent and further evidence of the parallel behavior of Ni and Fe.

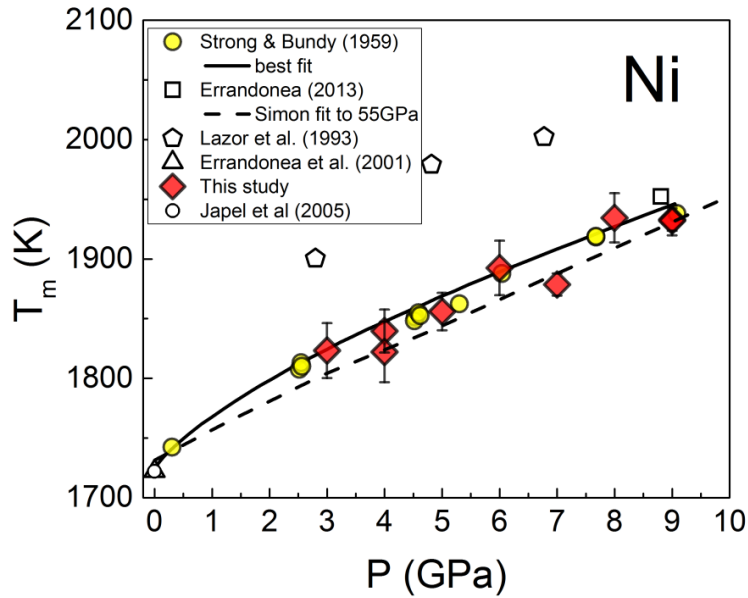
The melting temperature of Ni is plotted as a function of pressure in Figure 2.7 and is compared to the experimental data from Strong and Bundy (1959). There is good overall agreement between the two datasets. A small amount of contamination of Re or W would elevate the melting point of the Ni alloy (e.g., Okamoto, 2012) which additionally confirms the absence of any appreciable contamination prior to onset of Ni melting. The error bars correspond to the uncertainty associated with picking the melting point of a sample that has progressively melted over a narrow  $T$ -range.



**Figure 2.5:** (a) The dependence of the Curie temperature on pressure compared with the values from earlier studies (Leger et al., 1972; Sundqvist, 1988; Decker and Chen, 1992). (b) Resistivity at Curie temperature as a function of pressure.

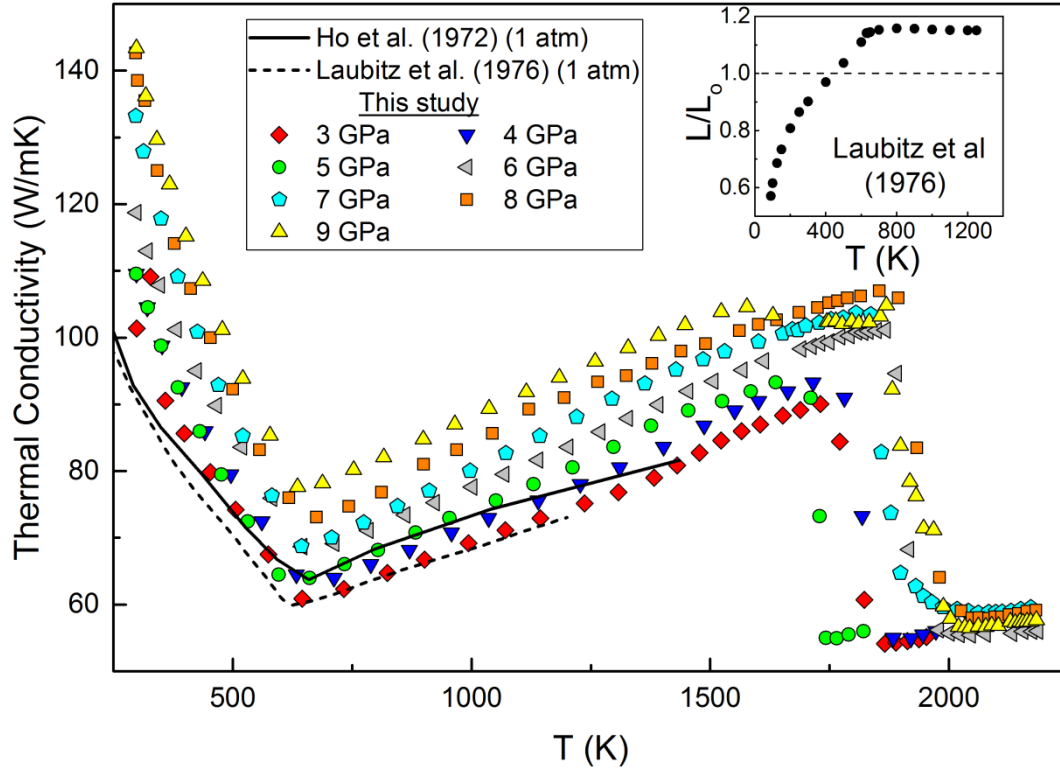


**Figure 2.6: Logarithmic electrical resistivity of solid Ni along isotherms as a function of pressure. The slopes of pressure coefficient of resistivity,  $(d\ln\rho/dP)_T$ , are plotted in the inset in units of  $\text{GPa}^{-1}$ .**



**Figure 2.7: A comparison of the melting temperatures of Ni obtained by resistivity jump on melting in this study with earlier studies using other methods in large volume press (yellow circles) and diamond anvil cells (other symbols) (Strong and Bundy, 1959; Lazor et al., 1993; Errandonea et al., 2001; Japel et al., 2005; Errandonea, 2013).**

Finally, the electronic component of the thermal conductivity,  $k_e$ , of Ni was calculated using our electrical resistivity data and the constant Sommerfeld value of the Lorenz number ( $L_0 = 2.44 \times 10^{-8} \text{ W}\Omega/\text{K}^2$ ). This is compared with the atmospheric pressure data of the total experimentally measured thermal conductivity,  $k_{total}$ , from Laubitz et al. (1976) and Ho et al. (1972), as shown in Figure 2.8. The total experimentally measured thermal conductivity includes both electronic and phonon components ( $k_p$ ) and is therefore expected to be higher than our calculated electronic thermal conductivity values. This is apparent in Figure 2.8, taking into account the observed trend of increasing electronic thermal conductivity with pressure in the solid state. The inset figure shows the temperature dependence of the Lorenz number,  $L(T)$ , normalized to  $L_0$ . The function  $L(T)$  was determined from separate experimental measurements of electrical resistivity and thermal conductivity of Ni (Laubitz et al., 1976). Values of  $L(T)/L_0$  are less than unity in the low temperature range, indicating that if  $L(T)$  was used in our calculation, the thermal conductivity values calculated with our experimental resistivity values would be even lower than those plotted in the low temperature range. However, in the higher  $T$  range,  $L(T)/L_0 > 1$  for Ni and this is also consistent with Fe as recently discussed (Secco, 2017). The values of the electronic thermal conductivity of Ni display the same general trend as the experimentally obtained total thermal conductivity at atmospheric pressure (Laubitz et al., 1976; Ho et al., 1972). Moreover, while the thermal conductivity of Ni has a positive  $P$ -dependence in the solid state, our results demonstrate that thermal conductivity is effectively invariant in the liquid in the range of  $P$  and  $T$  investigated in this work.



**Figure 2.8:** Calculated electronic thermal conductivity,  $\kappa_e$ , for solid and liquid Ni at pressures 3 - 9 GPa using the Wiedeman Franz law and the Sommerfeld value of the Lorenz number ( $2.44 \cdot 10^{-8} \text{ W}\Omega\text{K}^{-2}$ ). The electronic thermal conductivity of Ni is compared with total thermal conductivity,  $\kappa_{total}$ , at atmospheric pressure obtained by Laubitz et al. (1976) and Ho et al. (1972). The inset is the ratio of the experimentally derived temperature dependent Lorenz number for Ni, as measured by Laubitz et al. (1976), and the Sommerfeld value given above.

## 2.4. Discussion

The results obtained in this study demonstrate, within experimental uncertainties, that the electrical resistivity of liquid Ni is invariant along the melting curve up to 9 GPa. This diverges from the anticipated behaviour of electrical resistivity of liquid metals at high pressure arising from the thermodynamic argument presented by Stacey and Anderson (2001) and Stacey and Loper (2007). According to their prediction, the electrical resistivity of Ni is expected to be non-constant along the melting curve because Ni is an archetypical 3d transition metal and a very close electronic analogue of Fe. Recent measurements however of the electrical resistivity of Co ( $[\text{Ar}] 4s^2 3d^7$ ) along its melting



boundary show invariant behavior (I.E. Ezenwa, personal communication) similar to what is found in the current study on Ni. Therefore, in an attempt to reconcile the predictions by Stacey and Anderson (2001) and Stacey and Loper (2007) and recent theoretical (e.g., Pozzo et al., 2012; 2013) and experimental results (Gomi et al., 2013) on liquid Fe with the results obtained in this work, we seek a physical mechanism that explains such behaviour of Ni. Moreover, considering the electronic similarity of Ni and Fe, we seek to understand if the behaviour observed in liquid Ni under high pressures could potentially be extended Fe with important implications for the transport properties of the Earth's core. To make such a connection, it is important to discuss comparatively a simple metal such as Cu since it bridges the gap between the transition and noble metals. Additionally, Stacey and Anderson (2001) and Stacey and Loper (2007) suggested that Cu should show invariant resistivity behavior along its melt boundary.

This chapter presents a qualitative discussion on the possibility of a *P*-invariant Fermi surface and a constant electron mean free path at the onset of melting, as the physical mechanisms responsible for the invariant electrical resistivity of liquid Ni along its melting curve. Both phenomena are expected to manifest simultaneously. This chapter is organized as follows: in Section 2.4.1, the possibility of a constant spherical Fermi surface along the melting curve is examined; in Section 2.4.2, the role of d-band electrons, the local structures in the early melt and their potential influence on the electron mean free path is considered. Additionally, the correlation between the transition metals that obey the Kadowaki-Woods (K-W) ratio (Kadowaki and Woods, 1986) and those metals exhibiting anomalously shallow melting curves is also discussed in Section 2.4.2.

### **2.4.1 Fermi Surface and the Hall Coefficient in Liquid Transition Metals**

The main factors that affect the electrical resistivity of liquid metals are the magnitude and frequency of oscillatory motion of the ions, electron-electron scattering, and scattering of electrons by disordered magnetic moments (e.g., Mott, 1964, 1972). Both temperature and pressure affect the magnitude of these scattering mechanisms, where pressure increase suppresses the amplitude of atomic vibrations, thereby decreasing

electron scattering, while temperature has the opposite effect in both solid and liquid metals.

From Mott's formula for electrical conductivity (e.g., Mott, 1972, 1980; Shimoji, 1977) which is the basis for the Kubo-Greenwood expression used to calculate resistivity of transition metals (e.g., de Koker et al., 2012; Pozzo et al., 2012, 2013, 2014), the electrical resistivity of liquid metals is inversely proportional to the Fermi surface size and the mean free path of conduction electrons. Notably, in its unmodified form, the expression below is best applicable to simple liquid metals; however, it can also be applied to complex liquids (i.e., molten transition metals) (Mott, 1980):

$$\sigma_e = S_F |e|^2 l / 12\pi^3 \hbar \quad (2.1)$$

Here,  $\sigma_e$  is electrical conductivity,  $S_F$  is the area of the Fermi surface, and  $|e|^2$  is the electron mean free path which is defined as the product of the Fermi velocity,  $v_F$ , and the conduction electron relaxation time,  $\tau$ , where  $\lambda = v_F \tau$ , and  $\hbar$  is the modified Planck constant. The relaxation time varies with the DOS at the Fermi level (Shimoji, 1977) and the combined scattering mechanisms operating at a specific  $P$  and  $T$ .

If the electrical resistivity of a liquid metal at high pressures is invariant at the melting point, then it is reasonable to examine if there is a fundamental physical reason that would cause the Fermi surface and the mean free path of electrons in liquid transition metals to remain invariant along the melting boundary (e.g., Gapotchenko et al., 1988). To address those questions, a brief preamble needs to be given about the Hall coefficient in liquid metals since it can yield information about the shape of the Fermi surface and correspondingly, electronic transport (Chien and Westgate, 1980). In contrast to most solid metals, where the Hall coefficient,  $R_H$ , is a subtle indicator of the geometry of the Fermi surface, liquid simple metals (treated as simple liquids) are generally characterized by  $R_H = -\left(\frac{1}{ne}\right)$ , where  $n$  and  $e$  are the charge carrier number density and electron charge, respectively. This provides evidence that the Fermi surface can be treated as spherical (Faber, 1972; Evans, 1978). Generally, this can be extended to liquid transition metals

(treated as complex metal liquids (Iida and Guthrie, 2015)), although in some liquids with unfilled d-orbitals, a more complex behaviour is observed (Dupuy and Dianoux, 1978).

In solids, the Hall coefficient depends strongly on pressure (Boye et al., 2005) and temperature (Künzi and Güntherodt, 1980), indicating adjustment in electronic structure caused by these parameters. More directly, the Hall coefficient depends on the Fermi velocity, the electron effective mass,  $m^*$ , and on the first and second derivatives of electron energy  $E(k)$  (Busch and Güntherodt, 1974). Consequently, the Hall coefficient depends on the area of the Fermi surface through the expression (Ziman, 1961; Busch and Güntherodt, 1974):

$$R_H = -12\pi^3\hbar/em^*v_F S_F \quad (2.2)$$

A constant value of the Hall coefficient as shown in equation (2.2) suggests that either the effective mass, Fermi velocity and Fermi surface area all conspire to change in such a way that their product is constant, or that each of these parameters remains constant. As mentioned above, the Fermi surface has spherical shape in liquid metals since the energy shells in  $k$  space are spheres (see Busch and Güntherodt, 1974) and the Brillouin zone concept ceases to be relevant in the liquid state (Barnard, 1972). Assuming the spherical Fermi surface in the liquid state at atmospheric pressure can be reasonably extended to the high-pressure regime, albeit with a larger radius, equation (2.2) is expected to apply. This simplifies the conceptual inquiry into the problem of electrical conductivity, and by extension resistivity of compressed liquid, as an electron-ion elastic scattering event takes an electron from a given point on the Fermi surface to another point, on the Fermi surface (Blatt et al., 1976). This is especially relevant in conjunction with the presence of pressure independent local structures and coordination number at the onset of melting (Shen et al., 2004) as will be discussed later in this section.

The effects of pressure and temperature on the modification of the Fermi surface in solids and liquids are well known (Gaidukov and Itskevich, 1964; Jan, 1968; Evans and Jain, 1972; Venttsel et al., 1973; Vinokurova et al., 1979; Springford, 1980; Gapotchenko et al., 1988; Degtyareva, 2006). While pressure decreases the volume, in inverse space it increases Fermi wave vector ( $k_F$ ) and consequently the size of the Fermi sphere (Venttsel

et al., 1973). Temperature has an opposite effect, as it causes dilation of the electron shells (Kreutz et al., 1998; Sanloup et al., 2002). To gain some insight into relative magnitudes of these opposing effects on the Fermi surface a comparison is made of the isothermal compressibility and thermal expansion of liquid Ni and Cu (Nix and MacNair, 1941; Crawley, 1974; Drotning, 1981; Yokoyama et al., 1983; Ivanov et al., 1984; Hixson et al., 1990; Anderson and Ahrens, 1994; Nasch and Steinemann, 1995; Itami, 1995; Iida and Guthrie, 2015). While liquid Cu has a higher thermal expansion coefficient than liquid Ni by ~14%, the compressibility of liquid Cu is about ~40% larger than that of liquid Ni. High pressure brings atoms closer together and increases their exchange-interaction energy, thus causing broadening and overlap of the electron energy levels (Al'tshuler et al., 1968). Furthermore, pressure-induced broadening decreases the 3d DOS, which corresponds to volume reduction. It is the d-band density of states in both solid and liquid Ni that contributes the most to overall density of states at the Fermi level (Jank et al., 1991) and to the dominant *s-d* scattering mechanisms.

The implication of the above is that Cu will have significantly larger increase in its Fermi surface under compression, at melting, compared to the relatively more stable Fermi surface of Ni. Cu exhibits such behaviour, primarily because of the absence of an anomalous unfilled d band contribution, and its resistivity would be expected to decrease in the melt as a function of pressure in the absence of *s-d* electron scattering. This is contrary to what Stacey and Anderson (2001) and Stacey and Loper (2007) predicted but what has been shown by a recent experimental study on Cu up to 5 GPa (Ezenwa et al., 2017). Consequently, it would not be surprising if other transition metals with unfilled 3d shell might have a similar behaviour to Ni, as recently shown by a very recent experimental study on the resistivity of Co along its melting boundary (Ezenwa and Secco, 2017), although some exceptions to this are possible. That similarity is primarily due to their electronic structure and unfilled d-bands; the transition metals exhibit anomalous compressibility relative to simple and noble metals (Steinemann and Keita, 1988). However, in reality, complexities arise as the pressure derivative of the Fermi surface is generally highly nonlinear (Gapotchenko et al., 1988) in different transition metals. Moreover, in some solid metals, such as Co, the Fermi surface pressure derivative

is negative (Gapotchenko et al., 1988). For comparison, the Fermi surface pressure derivative for solid and liquid Ni is positive.

Based on the experimental results presented in this study, and the controlling effect of electronic properties of unfilled d-band transition metals on the size of the Fermi surface discussed above, it is reasonable to expect the possibility that under the opposite effects of pressure and temperature, the Fermi surface will remain invariant along the melting boundary. We note that experimental evidence of constant Fermi surface along the pressure dependent melting curve could be obtained by measuring the Hall coefficient of the compressed liquid metal.

The qualitative argument is extended to other physical properties of Ni in order to understand the possible role of the local short range structures in the liquid Ni and reasons for possible constant electron mean free path at melting points. Additionally, other similar 3d metals are briefly considered.

#### **2.4.2 The Role of d-electrons in Liquid Structure and the Electron Mean Free Path**

The structure and electronic properties of liquid transition metals have been studied extensively (Ziman, 1961; Evans and Jain, 1972; Mott, 1972; Busch et al., 1974; Busch and Güntherodt, 1974; Waseda and Tamaki, 1975; Meyer et al., 1976; Evans, 1978; Khanna and Cyrot-Lackmann, 1978; Fujiwara, 1979; Shvets, 1982; Dose et al., 1986; Jank et al., 1991; Jakse et al., 1996; Baria, 2004; Thakor et al., 2009). As a transition metal, Ni has vacant 3-d-states. The 3d-band of Ni, which is narrow in the solid state at 1 atm and broadens at higher pressure, has a high DOS relative to the s-band (Meyer et al., 1976; Khanna and Cyrot-Lackmann, 1978; Dose et al., 1986). However, the specific feature of a d-band is that it consists of five sub-d-bands, formed from wave functions of different symmetries (Blatt et al., 1976). The structure of a Ni d-band is complex due to the presence of preferential spin states and the DOS varies strongly with energy within the band.

In transition metals, both d-band and s-band electrons reside above the Fermi energy and have a contribution in electrical conductivity. The d-electrons have higher effective mass

and have lower velocity while lower effective mass and more mobile s-electrons are mainly responsible for transport of charge (Mott, 1972, 1980). The *s-d* scattering mechanism, favoured by Mott (1964, 1972, 1980), can be described in terms of hybridization of *s-d* orbitals, where s-electron makes a transition to the d-like part of the Fermi surface and this mechanism will be present in the high-pressure environment. The electron scattering is confined in an energy range within  $kT$  of the Fermi energy, where  $k$  is the Boltzmann's constant. In the solid, the number of scattering events is smaller than in the liquid.

The effective electron scattering cross sections in transition metals can be expressed as:  $\sum_{sc} (kT)^2 / (\varepsilon_d - \varepsilon_F)^2$  where  $\varepsilon_d$  is the energy of the d-band electrons within  $kT$  of the Fermi level that could contribute to *s-d* scattering (e.g., see Mott Mott, 1964, 1972; Blatt et al., 1976) and  $\varepsilon_F$  is Fermi energy. As temperature increases, the scattering cross section increases and hence the contribution of the electron-electron scattering to the resistivity as highly mobile s-electrons get scattered into much less mobile d-states. However, the exact magnitude of such contribution to electrical resistivity of liquid transition metal remains unclear.

In the liquid state, the 3d band of Ni is wider and 3d DOS is lower than that in solid Ni at 1 atm because of the reduction in the number of nearest neighbours (Khanna and Cyrot-Lackmann, 1978). The experimentally obtained results for DOS of solid and liquid Ni show that the d-band width increases by factor of 1.4 between solid and liquid (Dose et al., 1986). Theory predicts that this ratio scales almost linearly to the jump in electrical resistivity between solid and liquid Ni, which is about 1.3 at atmospheric pressure, but increases with pressure (Dose et al., 1986). Indeed, the results in this work demonstrate that the jump in electrical resistivity between solid and liquid is progressively higher with increasing pressure, and the trend is linear as shown in Figure 2.3b.

When McLachlan and Ehlers (1971) studied the effects of pressure on the melting temperature of metals, they noticed that Ni and a few select transition metals diverge from the trend theoretically predicted (see Japel et al., 2005 and references therein). Consequently, one of the unusual features of Fe, Ni, Co, Mo and Pt is their shallow

melting curves (Japel et al., 2005). These authors experimentally studied the melting curves of Ni and Cu and compared the results with the available model. According to the model discussed by Japel et al. (2005), partially filled d-electron bands lose structural periodicity associated with melting, which in turn changes the DOS in the liquid and lowers the liquid energy relative to the solid. Furthermore, at high pressure, s-d electron transfer lowers the slope of the melting curve of unfilled 3d-band metals. On the other hand, because of the filled d-band in Cu, its melting curve does not diverge from the theoretical model (Japel et al., 2005). This indeed has important ramifications for the discussion here, as it relates characteristics of the filled and unfilled 3d-band atomic structure to melting boundary behaviour. Ross et al. (2007) discussed the Peierls/Jahn-Teller distortion and the possibility that pressure-induced s-d electron “promotion” provides a mechanism for creating and enhancing the stability of local structures by enabling energetically preferred local ordering for liquids of metals with partially filled d-bands (e.g., Ni and Fe). The partially filled d-shell has the capacity to form locally preferred structures, which lowers the free energy of the liquid and hence lowers the melting temperature (Luo et al., 2010). Supporting such an argument is the well established presence of local ordering in liquid Ni where there are clusters with icosahedral short range order (ISRO) (Schenk et al., 2002; Lee et al., 2004; Ross et al., 2007). ISRO clusters incorporate 12 atoms exhibiting 5-fold symmetry surrounding a central atom (Lee et al., 2004). These clusters interact via a Lennard-Jones potential, which has energy that is 8.4% lower than a close packed arrangement in the solid (Schenk et al., 2002).

Could the presence of local structures in the melt discussed above mean that the electron mean free path is controlled by the length scale of ISRO clusters such that it remains invariant at the onset of melting and independent of  $P$ ? The experimentally observed local structural invariance of Fe, at the onset of melting and up to 58 GPa (Shen et al., 2004) may be used as an indicator of what can be expected for Ni. Shen et al. (2004) used x-ray scattering in a laser heated diamond anvil cell to demonstrate that liquid Fe remains a closed packed hard sphere liquid with the same shape of the structure factor up to 58 GPa. They concluded that *for liquid metals with close-packed structures and isotropic*

*metallic bonding, changes of local atomic configuration are generally not seen with pressure.* The experimental results presented in this study seem to support the argument that the overall arrangement of local structures and preferred ordering in Ni upon the onset of melting, remains relatively constant with increasing pressure (as manifested on the melting boundary) and consequently maintains a constant electron mean free path. That argument is additionally supported, at least in part, by theoretical work on the structure of liquid Ni along the melting curve (Cao et al., 2015). These authors found that the pair distribution function remains stable at pressures in the range of 20 - 100 GPa, while the coordination number decreases slightly from about 14.5 at atmospheric pressure to about 14 at 100 GPa.

Now, the correlation among unfilled 3d-band transition metals that obey the K-W ratio (Kadowaki and Woods, 1986; Jacko et al., 2009) is considered. The K-W ratio compares the temperature dependence of the resistivity of a metal to that of its heat capacity. When plotted on the standard K-W plot, select transition metals (Fe, Ni, Co, Pt, Pd, Re, and Os) have the same trend with a slope of  $\frac{A_r}{\gamma^2} \approx 0.4 \mu\Omega \text{cm mol}^2 \text{K}^{-2} \text{J}^{-2}$  (Jacko et al., 2009), where  $\gamma$  is the linear factor of temperature dependent electronic contribution to the heat capacity, and  $A_r$  is the proportionality factor to the quadratic term of  $T^2$  in resistivity at low temperature. Considering that the K-W ratio is a reflection of electron-electron scattering in strongly correlated systems (Rice, 1968), such as heavy fermions, we expect that the K-W ratio reveals similar information about electron-electron scattering in 3d transition metals (Jacko et al., 2009). The common thread between Ni and the select group of transition metals that follow the K-W ratio is the relation between the temperature dependent electronic contribution to the heat capacity and electron-electron scattering. We expect that the similarity in K-W behaviour extends to transport properties and that the invariant electrical resistivity behaviour observed in compressed liquid Ni, will be potentially present in those 3d transition liquid metals that also have unfilled d-shells.

Finally, the metals that have a shallow melting curve also exhibit a common trend on a K-W plot (e.g., Fe, Ni, Pt). Considering that both phenomena are caused by the



contribution of unfilled d-band electrons, we can reasonably predict that the transition metals to which both phenomena apply, will have invariant electrical resistivity along the melting curve. The recent experimental work by McWilliams et al. (2015) demonstrated that electrical resistivity and thermal conductivity of liquid Pt remain relatively invariant along its melting boundary, up to Earth's core pressures. Experimental verification of constant resistivity of Fe along its melting boundary has not yet been obtained.

## 2.5. Conclusion

High pressure electrical resistivity of Ni is constant along the melting curve. The electrical resistivity behaviour of Ni at melting (as a close analogue to Fe) disagrees with Stacey and Loper (2007) conclusion that such behaviour can only be applicable to simple liquid metals. Furthermore, the results presented here are consistent with conclusions of the recent experimental studies on Pt (McWilliams et al., 2015). The nature of such electrical resistivity behaviour in liquid Ni is attributed to the possibility of a constant Fermi surface and an invariant electron mean free path in the initial Ni melt. This may be associated with local symmetry structures observed in molten transition metals with unfilled d-band which has been shown to be responsible for the shallow melting curves. Based on the arguments presented and supportive evidence in the literature, it is proposed that the same electrical resistivity behaviour as observed in liquid Ni will be observed in other liquid transition metals that follow the Kadowaki-Woods ratio. The same argument predicts that Stacey and Anderson's (2001) theoretical interpretation will not be applicable to some liquid simple metals with a filled d-band, such as Cu. With respect to our results on Ni and their implications for the behaviour of electrical resistivity of Fe and its alloys in Earth's outer core, it is premature to make any predictions other than to highlight the similarity between Ni and Fe electronic structure and behaviour. Experimental resistivity data of the major core component, Fe, and its alloys along the melting boundary are needed and if shown to be constant, this could have important implications for heat flow in Earth's core.

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## Chapter 3

### 3. Electrical resistivity of liquid Fe to 12 GPa: Implications for heat flow in cores of terrestrial bodies

*Today's scientists have substituted mathematics for experiments, and they wander off through equation after equation, and eventually build a structure which has no relation to reality.*

- Nikola Tesla

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Silber, R. E., Secco, R. A., Yong, W. and Littleton, J. (2018) Electrical resistivity of liquid Fe to 12 GPa: Implications for heat flow in cores of terrestrial bodies, *Nature Scientific Reports*, 8, 10758, doi: 10.1038/s41598-018-28921-w

#### 3.1. Introduction

Electrical and thermal transport properties of liquid iron (Fe) control the amount of heat conducted through the outer core (OC) to the core-mantle boundary (CMB) (de Koker et al., 2012; Gomi et al., 2013; Goncharov et al., 2015; Konôpková et al., 2016; Ohta et al., 2016; Pozzo et al., 2012; Stacey and Loper, 2007) in terrestrial planetary bodies. Experimental evaluation of electrical resistivity ( $\rho$ ) and thermal conductivity ( $\kappa$ ) of liquid Fe under high pressures ( $P$ ) is very challenging (Ohta et al., 2016; Shen et al., 2004), and remains one of the key aspects in rigorously constraining the thermal, spatial and temporal evolution of terrestrial cores and dynamos Gubbins et al., 2015. Despite recent advances in high pressure experimental techniques, thus far only two experimental investigations of  $\rho$  of liquid Fe in the lower  $P$  region below 7 GPa are reported in literature (Deng et al., 2013; Secco and Schloessin, 1989).

Recent theoretical (de Koker et al., 2012; Pozzo et al., 2012) and experimental (Gomi et al., 2013; Ohta et al., 2016) studies present a revised set of low  $\rho$  values and

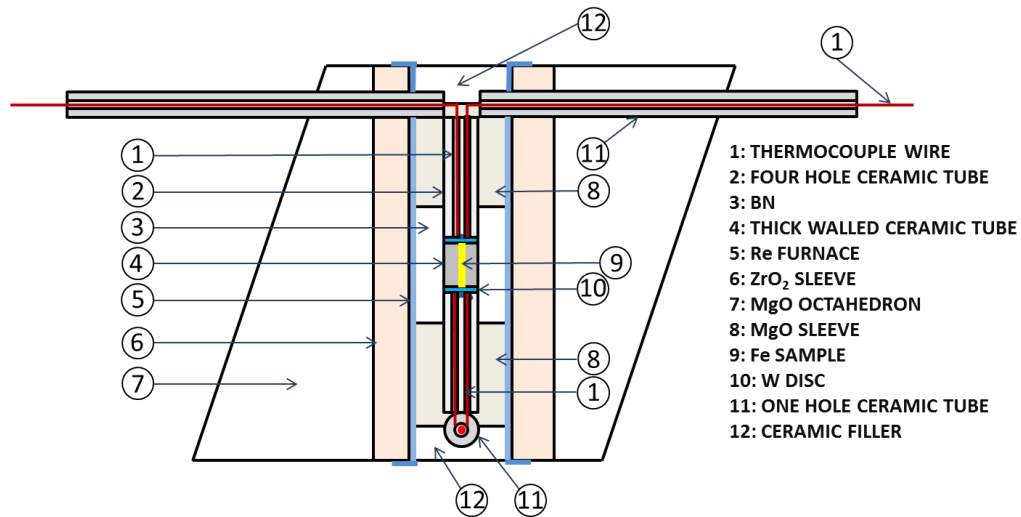
corresponding  $\kappa$  values for the Earth's liquid outer core that are up to 4 times higher than previously accepted (Stacey and Loper, 2007). Such high values of  $\kappa$  for the outer core, in the range  $90 - 130 \text{ Wm}^{-1}\text{K}^{-1}$ , directly affect estimates of the age of the inner core (Gubbins et al., 2015), as well as the energy budget available to power and maintain the geodynamo (Gubbins et al., 2015) for the past 4.2 Ga (Tarduno et al., 2015). However, in contrast to the low values of  $\rho$  and high values of  $\kappa$  in the Earth's liquid core, the first direct experimental measurements (Konôpková et al., 2016) of  $\kappa$  of Fe showed  $\kappa$  to be in line with previously accepted values (Stacey and Loper, 2007). New diamond anvil cell (DAC) experimental data (Goncharov et al., 2015; Hsieh et al., 2017; Ohta et al., 2017; Okuda et al., 2017) place constraints on the  $\kappa$  of lower mantle minerals, which subsequently limits the magnitude of heat flux through the CMB. These experimental results are complemented by numerical studies (Drchal et al., 2017; Pourovskii et al., 2017) of Fe at core conditions which demonstrate the important role of electron-electron scattering and spin disorder. The absence of a consensus on  $\kappa$  and uncertainty in ohmic losses in the core necessitate a consideration of alternative sources of energy required to generate the Earth's magnetic field throughout history (O'Rourke and Stevenson, 2016).

It was recently postulated on the basis of theoretical reasoning that  $\rho$  may be invariant for pure simple liquid metals, but not for liquid transition metals, along their respective melting curves (Stacey and Loper, 2007). However, new experimental work demonstrated that transition metals, Ni and Co have invariant  $\rho$  along the melting boundary (Silber et al., 2017; Ezenwa and Secco, 2017). This study is motivated by the possibility that liquid Fe may exhibit the same melting boundary behavior of  $\rho$  as Ni and Co, and enable better insight into the thermal state and dynamics of experimentally reachable conditions of cores, particularly at the boundary between the solid inner and liquid outer cores, particularly at the boundary between the solid inner and liquid outer cores, of the small terrestrial bodies Mercury, Mars, Moon and Ganymede.

## 3.2. Methods

### 3.2.1. Instrumentation

We used a large volume 3000 ton multi-anvil press and a 4-wire method, along with polarity switching to measure electrical resistivity ( $\rho$ ). The cell design (Figure 3.1) and the experimental methods are described in detail elsewhere (Silber et al., 2017). The radial geometry of the liquid Fe sample is preserved by using the high density ceramic tube in which a highly polished Fe wire is tightly fitted with tolerances less than 0.001 mm. The only notable difference in this work is the use of a W-foil to contain the Fe melt and preserve the axial geometry of the liquid sample. The advantages of this method (Silber et al., 2017) are: (i) liquid containment; (ii) preservation of sample geometry through the full range of  $P$ - $T$  experimental conditions; and (iii) delaying the onset of diffusion and sample contamination, such that the  $\rho$  values collected through rapid data acquisition at the melting temperature are predominantly from the Fe-sample contribution. The experimental approach to evaluate the effects of W diffusion in liquid Fe, and detailed compositional analyses by Electron Microprobe (EMP) data and images, are reported in this section.



**Figure 3.1: The high pressure experimental cell design (after Silber et al., 2017).**

### 3.2.2. Use of Tungsten (W) Disc

The most optimal way to measure electrical resistivity of molten materials is to maintain direct contact between the electrodes and the sample. However, such an approach is not possible in the case of liquid transition metals (Ezenwa and Secco, 2017; Silber et al., 2017) Ni and Co, and even more so in the case of liquid Fe since most electrode materials will easily diffuse into these transition metals. In this work we used type C thermocouples (TC) and diffusion of W and Re from a TC wire junction in direct contact with the molten Fe sample is unavoidable and would inevitably skew readings of both voltage drop and temperature. A modified approach (Silber et al., 2017) can be adopted to postpone the effect of diffusion, data are acquired rapidly. This method relies on use of W as an intermediary highly conductive material, located between 4-wire electrode/thermocouple junctions and the sample, enclosed in a high density ceramic tube (CT) (Figure 3.1). A W-disc emplaced at these positions is also instrumental in containing molten Fe and maintaining axial geometry. The thickness of W disc is 0.1 mm and a radius of approximately 3 times that of the sample. Considering that electrical resistivity of W is half that of the solid Fe sample at 300 K, the overall contribution to measured  $\rho$  is less than 1% with the thickness and length utilized in this work). Therefore, the measurement of electrical resistivity of the liquid Fe is minimally affected. Moreover, the choice of W as an intermediary material is influenced by the requirement that its melting temperature is much higher than the melting temperature of the measured Fe sample. By using W disc as a contact/containment medium, we preserve the chemical (and thermoelectric) integrity of the TC/electrode during the initial rapid set of electrical resistivity measurements that are mainly due to the contribution of the liquid Fe sample. However, such an approach can only be effective if it can be demonstrated that there is little or no immediate diffusion of W throughout the sample, at the onset of melting. To confirm this, we performed electron microprobe (EMP) analyses on our post-experimental recovered samples that were compressed and heated to temperatures below melting, to the melting temperature, and to temperatures of 50 K and 188 K above melting. The heated experimental cell was immediately quenched after reaching the



target temperature. Additionally, we used high density, thick walled, ceramic tubes ( $\text{Al}_2\text{O}_3$ ) to maintain the lateral geometry of the liquid sample.

### 3.2.3. Electron Microprobe Data

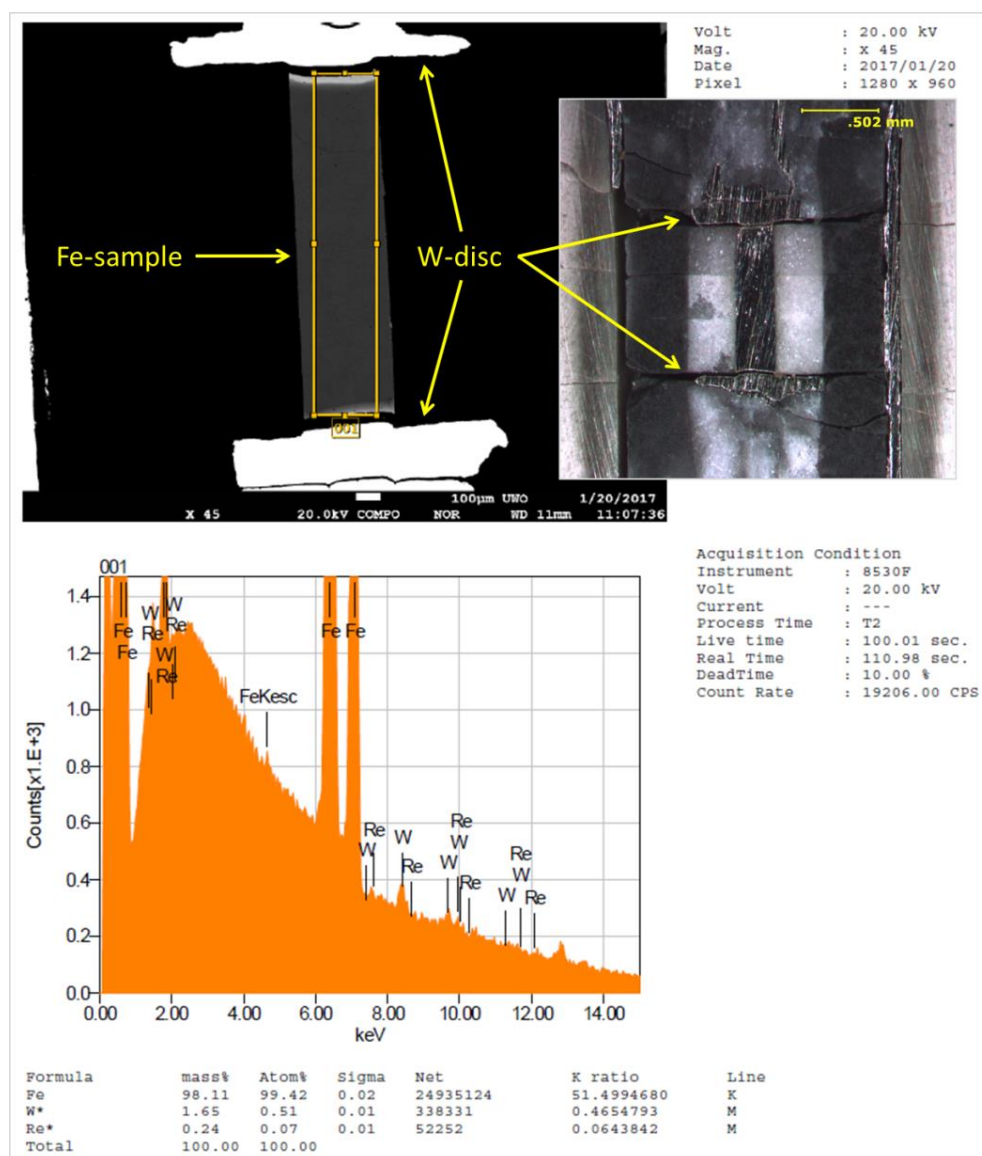
EMP data was collected using a JEOL JXA-8530F field-emission electron microprobe at the Centre of Planetary Science & Exploration, Western University, London, Ontario, Canada. For all the analyses in this work, an accelerating voltage of 20 kV, a probe current of 50 nA, and a spot size ( $\sim 100$  nm) beam were used. In terms of compositional analyses, our samples were compared against the pure metal standards (Fe, Ni, W, Re) and silicate phase references (Si).

EMP results for samples recovered from heating to high temperatures but not melted showed negligible ( $<0.4\text{wt}\%$ ) W diffusion into solid Fe. The EMP results for samples heated to melting and above are given in Figures 3.2 – 3.7. Figure 3.2 shows sample compressed to 3 GPa and heated to the melting point. In the energy dispersive X-ray spectroscopy (EDS) data sets and images shown in Figure 3.2 and 3.3, it can be seen that at the onset of melting, diffusion of W into the cylindrical ends of the Fe sample takes place. However, the initial set of voltage drop measurements across the liquid sample is primarily due to Fe. The corresponding recovered and sectioned sample is shown in the inset.

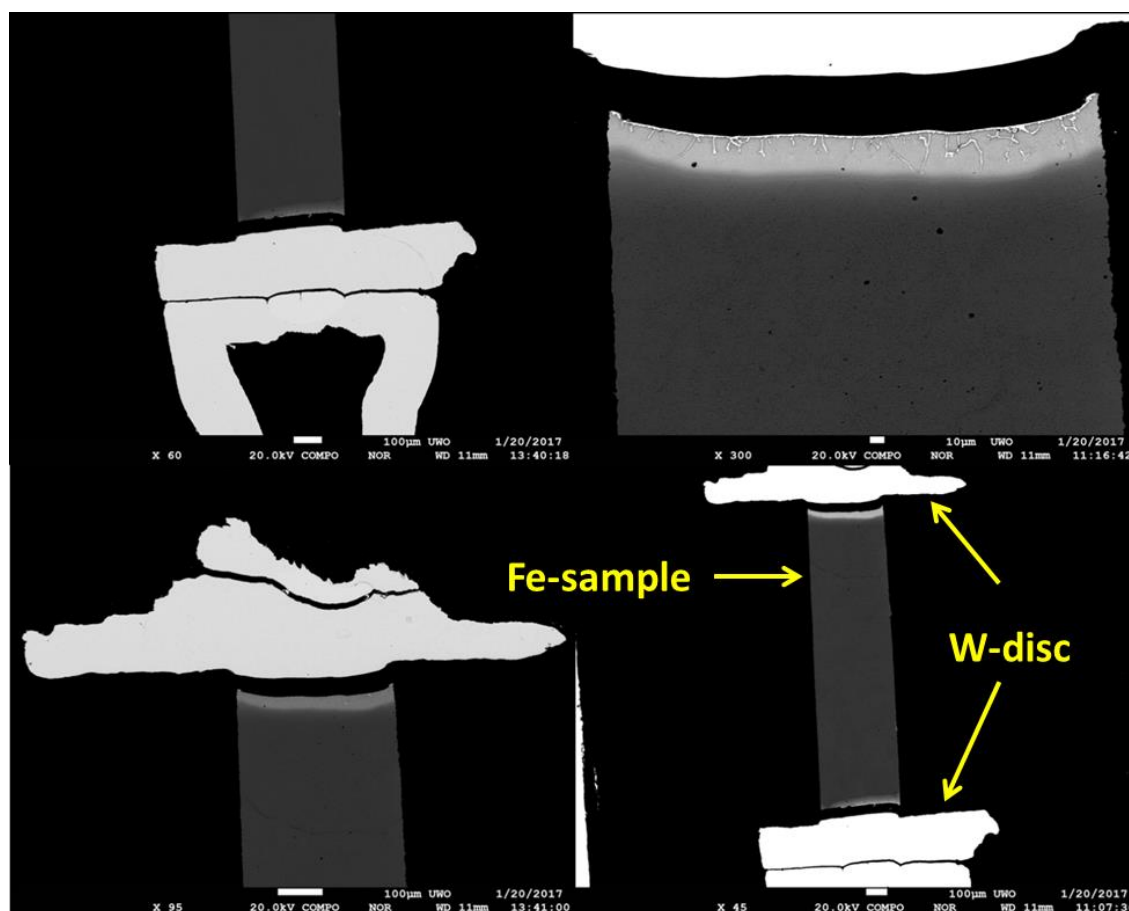
In the sample compressed to 7 GPa and heated to 50 K above the melting point (Figures 3.4), the evidence of W diffusion into the Fe sample is clearly visible. However, Fe is still dominant at 97.16 at%. Figure 3.5 shows wavelength dispersive X-ray spectroscopy (WDS) analyses (the annotated values of point analyses correspond to the table values) and the progression of diffusion can be seen. The corresponding optical image of the same recovered sample is shown in the inset of Figure 3.4.

In a sample heated to a temperature of 188 K above the melting  $T$ , W diffusion in liquid Fe is clearly evident (Figures 3.6 and 3.7). However, it must be emphasized that diffusion is also sensitive to the amount of time spent in melt. After careful observation, it can be seen in plots of  $\rho$  (see the results section) that the linear positive slope of  $\rho$  in liquid Fe

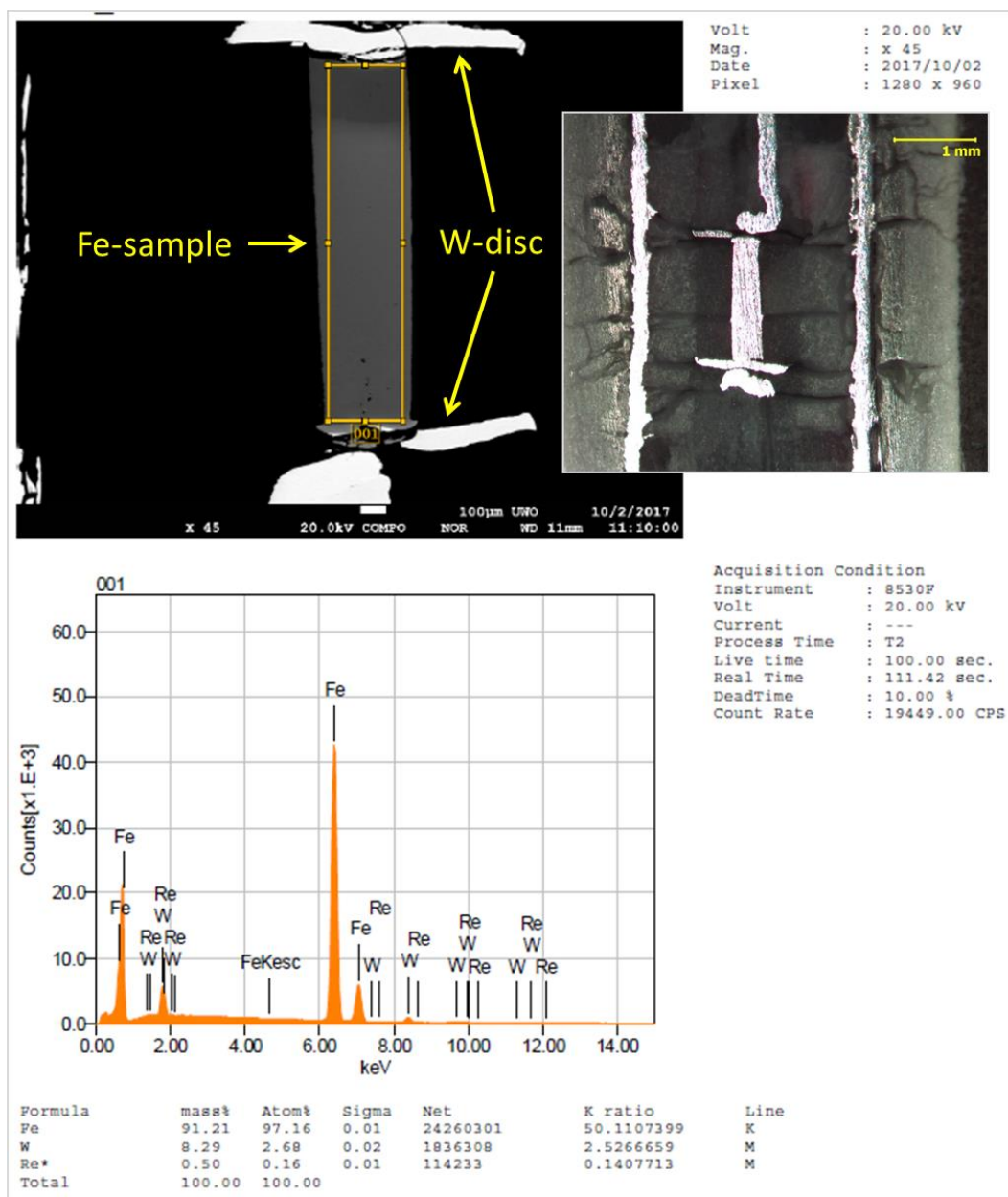
starts decreasing after the first 3 – 6 data points in the complete melt. This is interpreted to be caused by the progression of W diffusion in liquid Fe, which starts to lower  $\rho$ . For all experimental pressures in this work, we observed that the trend line of  $\rho$  in the liquid changes sharply to a negative slope at about the 16 second mark in melt. We note a rapid decrease in  $\rho$  after a duration of 16 seconds in the melt, but these data are not shown here. A reasonable interpretation is that after approximately 16 seconds (following the onset of melt), the effect of W in the liquid Fe starts to dominate in the measured electrical resistivity. This leads to rapid decrease of  $\rho$ , observed in liquid at all pressures in this study. Therefore, in determination of  $\rho$  along the melting boundary, we only consider those first few  $\rho$  points in the liquid Fe that exhibit a distinct linear trend.



**Figure 3.2:** A representative example of EMP-EDS of a sample compressed to 3 GPa and heated to the melting point used in determination of diffusion of W into Fe at the melting point. The heated experimental cell was immediately quenched after reaching the target temperature. Surface diffusion along the grain boundaries is visible; however overall Fe is 99.42 at%. The yellow outlined rectangular are is the region probed by EDS. Inset: Corresponding image of post-experiment recovered and sectioned sample.



**Figure 3.3:** Close-up of the region with surface diffusion of W into liquid Fe. The sample was compressed to 3 GPa and heated to the melting point. The heated experimental cell was immediately quenched after reaching the target temperature. The regions are W (or W/Re TCs) and the dark gray metal in the middle is the Fe sample. The light grey regions at the ends of the sample contain some W.



**Figure 3.4: Representative EMP-EDS of a sample compressed to 7 GPa and heated to 50 K over the melting point, and then quenched. The diffusion of W can be seen throughout the sample which is still dominated on average by Fe (97.16 at%). The upper part of the sample is less contaminated due to the fact that it was on the bottom during the experiment, and diffusion is likely uneven because of the influence of gravity. The rectangular area outlined in yellow is the region probed by EDS. Inset: The corresponding post-experimentally recovered and sectioned sample. The image in the inset is rotated 180° relative to the EMP image.**

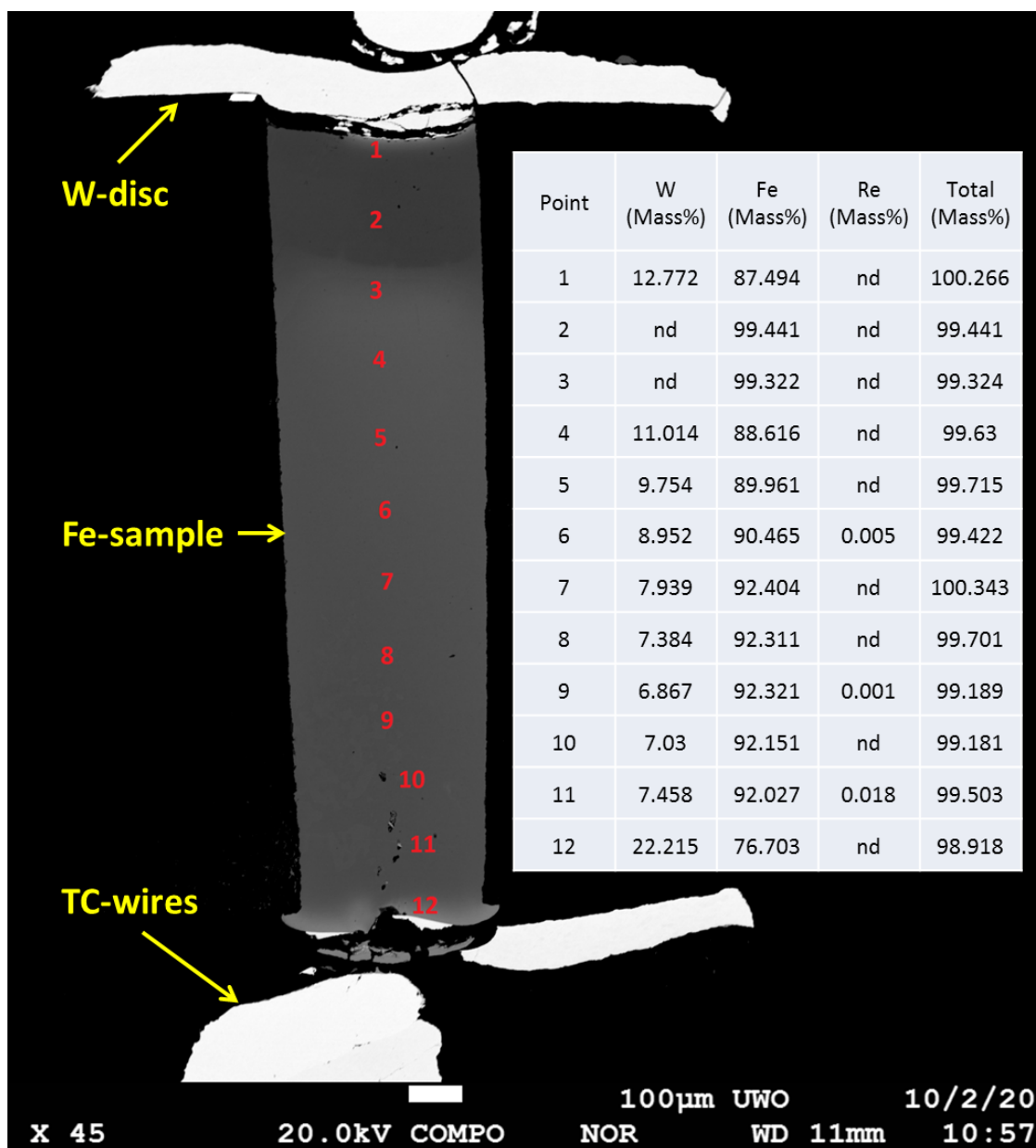
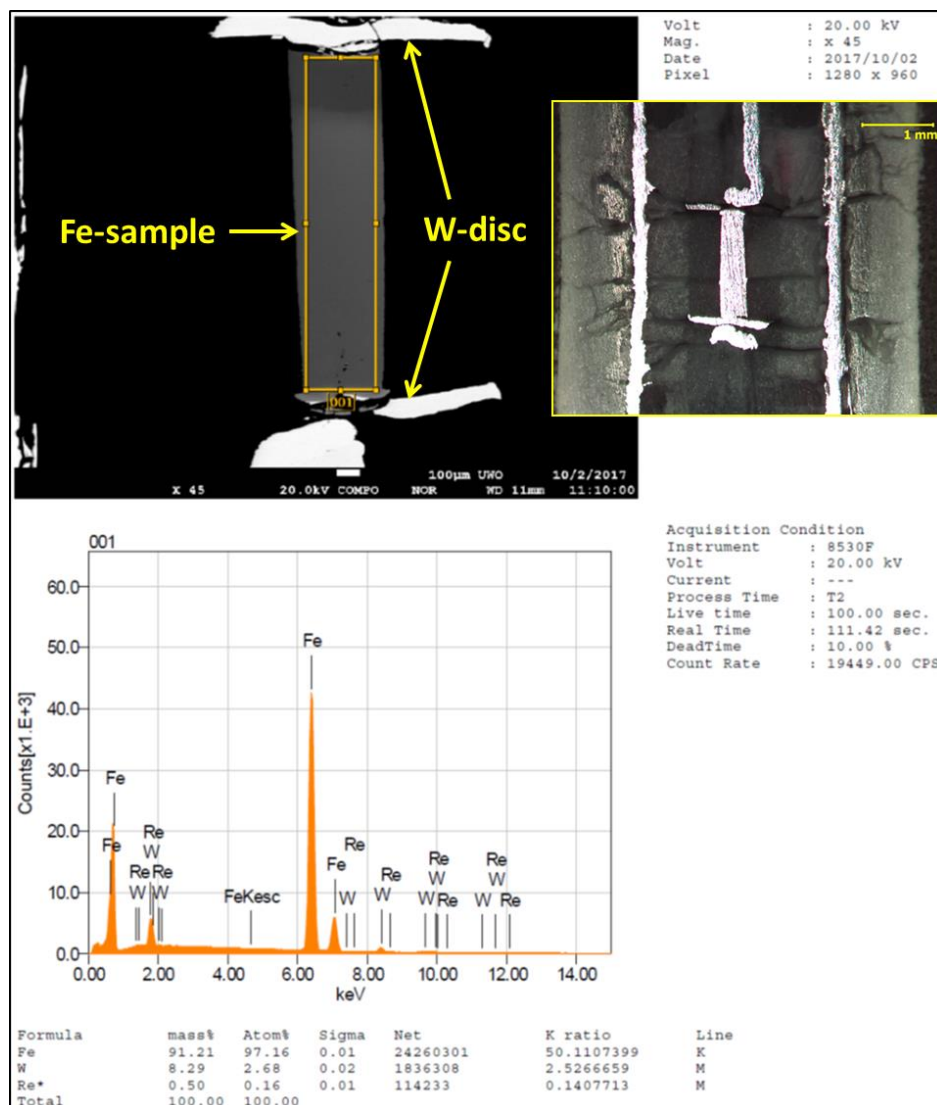
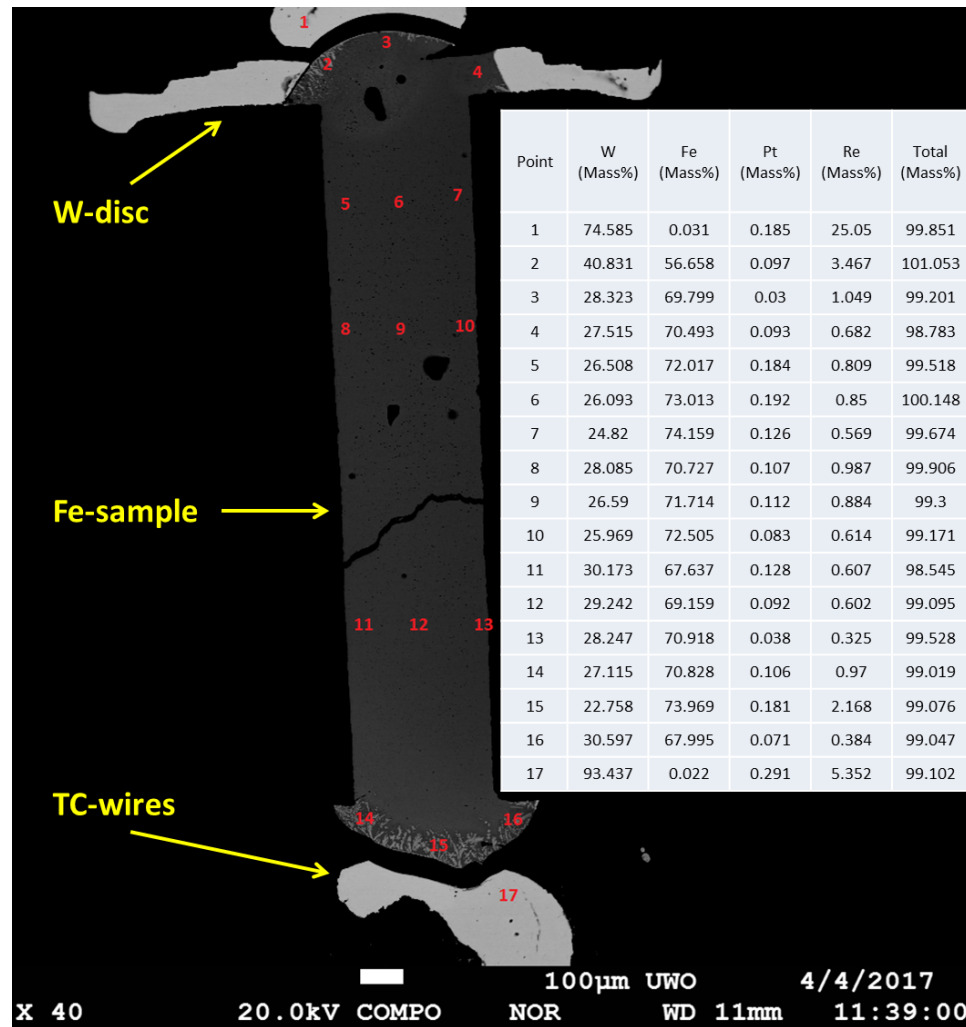


Figure 3.5: EMP-WDS of the sample in Figure 3.4. The annotated points on the sample correspond to the point numbers in the table. The notation “nd” means not at detectable levels.



**Figure 3.6: EMP-EDS of the sample compressed to 3 GPa and heated to 188 K above the melting point. It is possible to see the formation of dendritic structures at the ends of the sample because the TC wires penetrated the disc and were in touch with the liquid Fe sample, which enabled diffusion of both W and Re into liquid Fe. The rectangular area outlined in yellow is the region probed by EDS. Inset: Magnified dendritic structures in the lower part of the sample.**



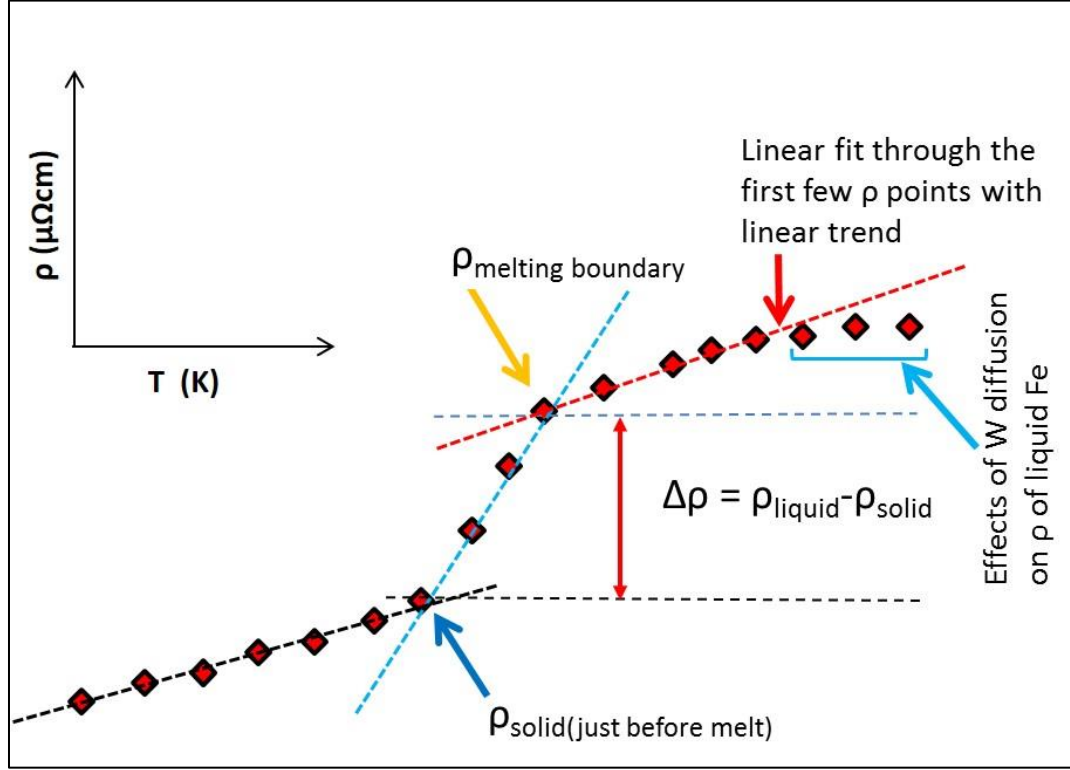
**Figure 3.7:** The EMP-WDS scan of individual points on the sample in Figure 3.6. The points and values in the table correspond to the annotated points throughout the sample.

### 3.2.4. Determination of Electrical Resistivity Along the Melting Boundary

Figure 3.8 illustrates the procedure of determining  $\rho$  of Fe along its melting boundary. The procedure consists of fitting a linear trend through data points of  $\rho$  in the solid and connecting the last  $\rho$  point in the solid with the points in the liquid using a linear trend through intermediate points between the two phases. The intersection between the linear fit through the first few  $\rho$  points in liquid (with a clear linear trend) and the line through intermediate points, connecting the solid and liquid phase, is taken to be  $\rho$  along the



melting boundary. It is interpreted that Fe is fully melted at that point so that the measured  $\rho$  is the resistivity of only the liquid.

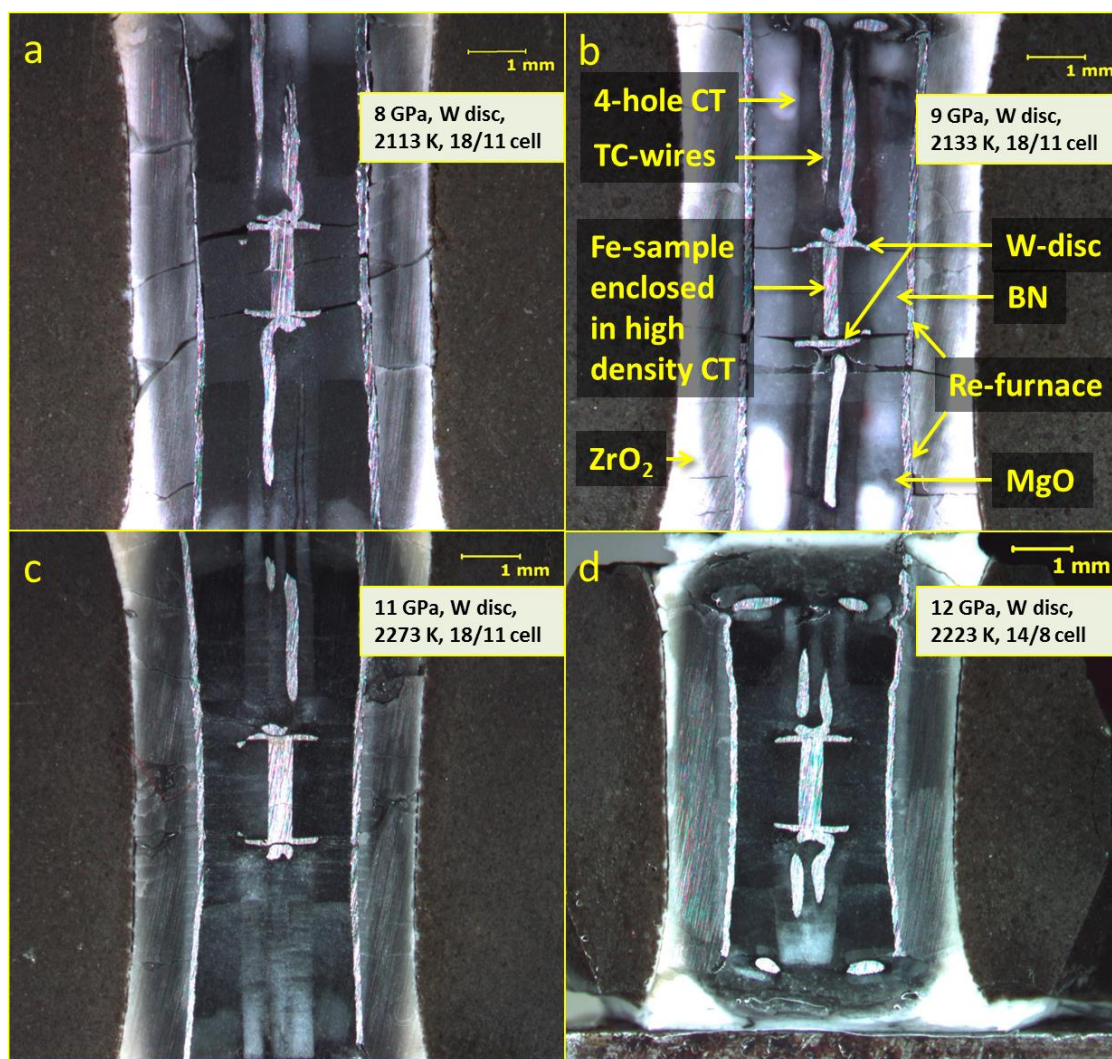


**Figure 3.8: Illustration showing how the  $\rho$  along the melting boundary of Fe and  $\Delta\rho$  ( $\rho_{\text{liquid}} - \rho_{\text{solid}}$ ) were determined.**

### 3.2.5. Uncertainties and Sectioned Samples Geometry

The errors calculated in this study reflect the standard deviation between the absolute value of positive and negative polarity voltage readings during data collection, as well as the uncertainty in length of the sample that arises from volumetric changes at high  $P$  and  $T$  including melting, and slight changes in shape of the recovered sample. The uncertainty in length in the solid phase is 0.01 mm and in the liquid phase 0.05 mm. Overall, the same methodology in error determination as discussed in detail by Silber et al. (2017) is followed in this work.

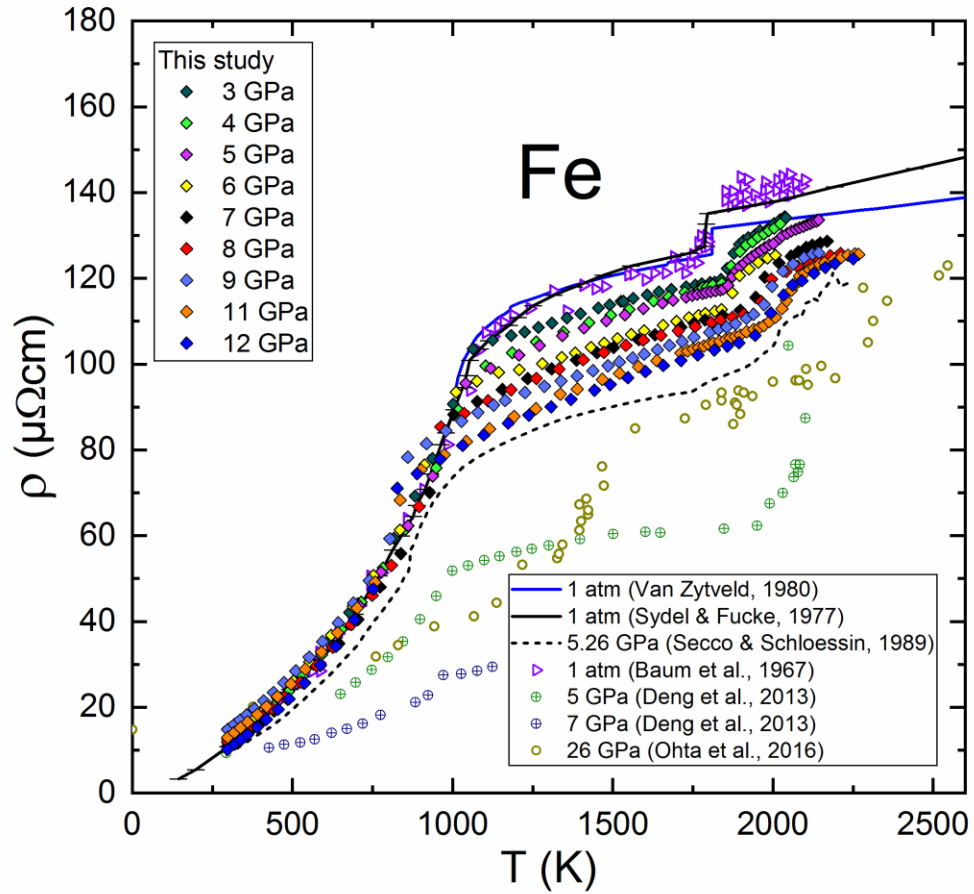
For illustrative purposes, Figure 3.9 shows images of representative post-experiment samples recovered from a range of pressures that were heated deep into liquid to illustrate the preserved geometry in quenched samples.



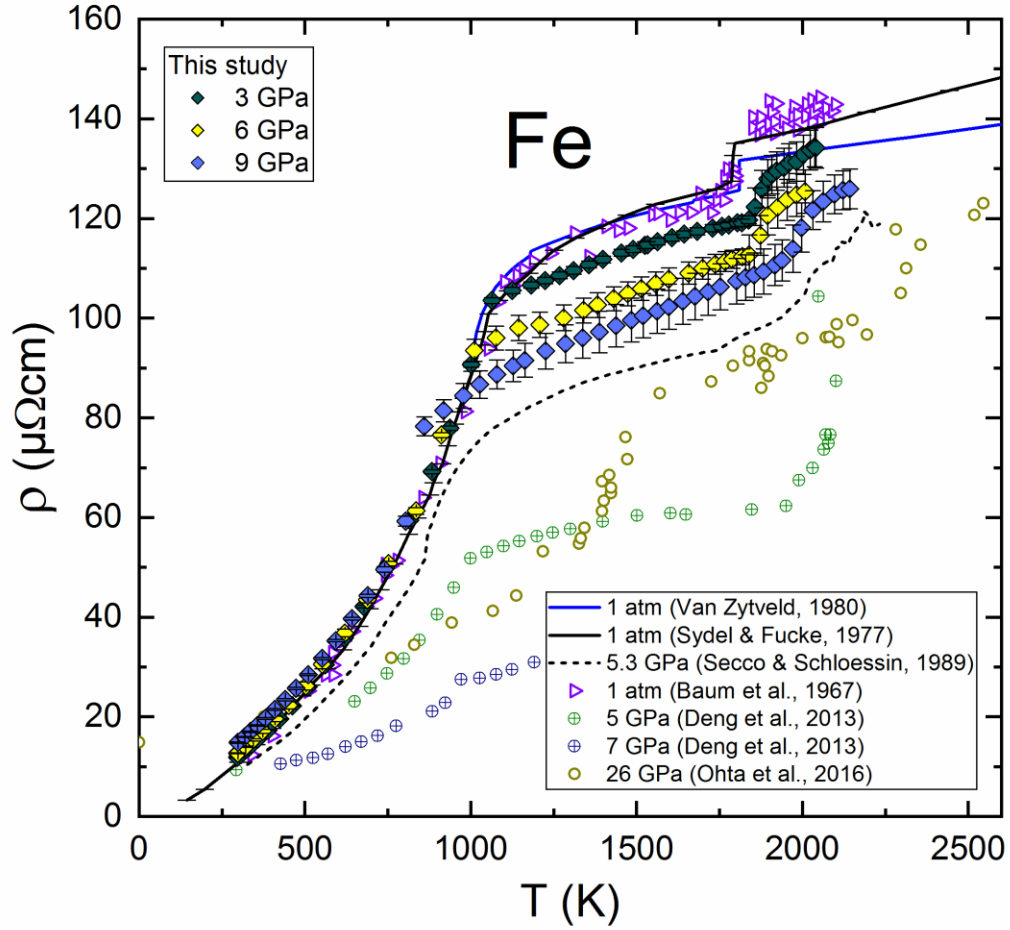
**Figure 3.9:** Representative examples of recovered and sectioned sample cells heated and compressed to (a) 8 GPa, (b) 9 GPa, (c) 11 GPa and (d) 12 GPa. The maximum temperatures are stated in the figures. Panels (a) – (c) show 18/11 cell and panel (d) shows 14/8 cell. A W-disc was employed throughout.

### 3.3. Results

Here, the results of measurements of  $\rho$  of solid and liquid Fe (99.99% purity), between 3 and 12 GPa (Figure 3.10) are reported. Representative error bars are shown in Figure 3.11 for 3, 6 and 9 GPa of this study. The measured  $\rho(P,T)$  for all experiments are compared to data from atmospheric and other high pressure studies. Overall, the values of  $\rho$  obtained for solid Fe follow the similar trend observed in measurements at 1 atm and in earlier measurements (Secco and Schloessin, 1989) up to 7 GPa, but diverge significantly from recent work (Deng et al., 2013) for 5 and 7 GPa (Figure 3.10).



**Figure 3.10:** Electrical resistivity of solid and liquid Fe at 3 – 12 GPa. Our data compared with  $\rho$  from the earlier results (as shown in the legend), obtained at 1 atm., 5, 5.3, 7 and 26 GPa.



**Figure 3.11: Electrical resistivity curves at 3, 6 and 9 GPa with representative error bars and combined with available literature values of  $\rho$  obtained at atmospheric pressure and at 5, 5.3, 7 and 26 GPa. The simultaneous increase in  $\rho$  and  $T$  in the melting interval are likely the result of the presence of  $T$ -gradients in the cell which are exacerbated by the rapid rate of heating through melting.**

We have not observed the effects of the  $\epsilon$ -phase on  $\rho$  at 12 GPa, nor did we see any deviation from the standard  $\alpha$ -phase scattering before the Curie  $T(T_c)$ , suggesting that the sample did not enter the  $\epsilon$ -phase. The electrical resistivity of  $\alpha$ -Fe remains invariant as a function of  $P$  up to  $T_c$  because of strong magnon scattering and a large Fe magnetic moment ( $2.2\mu_B$ ) (Landrum and Dronskowski, 2000). Notably, while  $T_c$  (1040 K at 1 atm) remains constant up to 1.75 GPa (Leger et al., 1972), continuous pressure dependent decrease in  $T_c$  that approximately follows the  $\alpha$ - $\gamma$  boundary was observed. The electrical resistivity decreases almost linearly above  $T_c$  as a function of  $P$  in the  $\gamma$ -phase, primarily

because the long-range order of spin magnetic moments is lost by the effects of temperature, and the electron scattering by magnons becomes reduced compared to temperature-induced phonon scattering, which itself is suppressed by the effects of pressure. Our results demonstrate, within experimental uncertainties, that  $\rho$  of liquid Fe, along its melting boundary, decreases from 3 to 5 GPa and remains invariant from 6 to 12 GPa. For all experimental  $P$  above the  $\delta$ - $\gamma$ -liquid triple point at 5.2 GPa, the  $\rho$  values of liquid Fe at melting remain remarkably constant at  $\sim 120 \mu\Omega\text{cm}$  up to 12 GPa (Figure 3.12a). This value is consistent with recent DAC data (Ohta et al., 2016) for  $\rho$  of liquid Fe at 26 GPa.

In comparison with Ni and Co, the interpretation of  $\rho$  of liquid Fe is more complex due to the polymorphism in solid state before and after the  $\delta$ - $\gamma$ -liquid triple point pressure. Such behavior requires additional consideration. Although not previously reported by experimental studies to-date, the abrupt and distinct change in  $\rho$  of liquid Fe at the  $\delta$ - $\gamma$ -liquid triple point is not unexpected. There is also a significant change observed in other properties of liquid Fe at this triple point, such as the temperature coefficient of resistivity (Secco and Schloessin, 1989), structure factor, compressibility, and density (Sanloup et al., 2000) and viscosity (Terasaki et al., 2002).

### 3.4. Discussion and Conclusions

#### 3.4.1. Liquid Structure, Liquid Properties and Melting Boundary

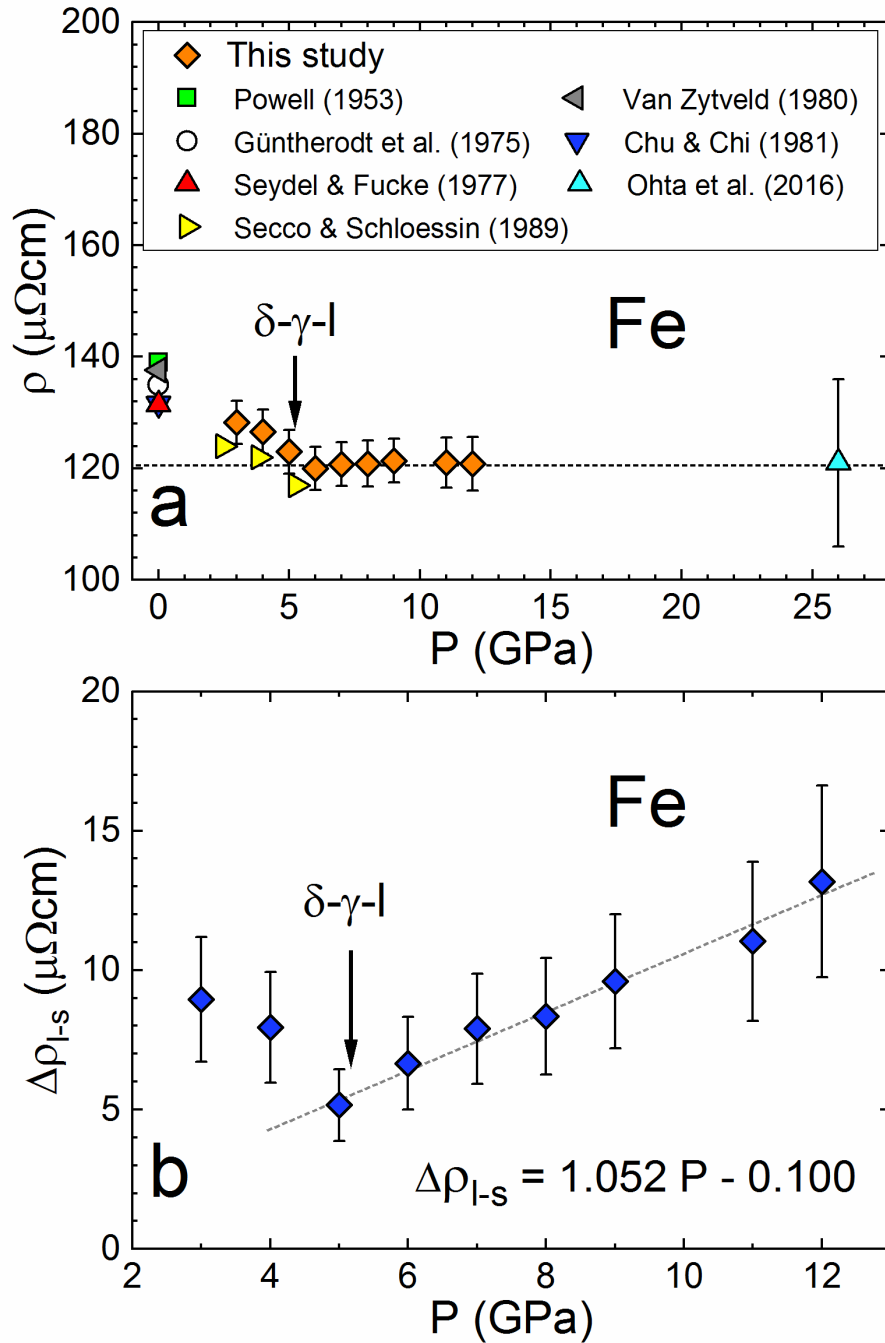
Liquid-liquid phase transitions under high pressure are not uncommon in transition metals (Lee and Lee, 2016). The existence of such a phase transition in liquid Fe around 5 GPa just above the melting boundary, influencing structural changes and many of its properties, has been considered recently (Sanloup et al., 2000). However, we cannot interpret the change in our observed  $\rho$  of liquid Fe around 5.2 GPa as an equilibrium liquid-liquid phase transition, as such a transition is thermodynamically not plausible at the existing triple point. This leads us to support the premise (Secco and Schloessin,

1989) that the solid Fe-parent phase has a direct influence on the structure and properties of the liquid in short and medium range order at temperatures very close to the melting boundary. The existence of spin scattering similarities between the liquid and solid Fe-phase (Waseda and Suzuki, 1970) seems to support that. Correspondingly, in-situ high pressure X-ray scattering study shows that liquid Fe originating from the  $\gamma$ -parent solid phase remains structurally stable along its melting boundary from 27 to 58 GPa (Shen et al., 2004). The aforementioned results impose significant constraints on the thermodynamic and transport properties of liquid Fe (Shen et al., 2004). The conclusions of that study imply possible  $P$ -independent electron mean free (Silber et al., 2017) path along the Fe melting boundary and may corroborate why our observed constant value of  $\rho$  above 5 GPa for liquid Fe is in line with  $\rho_{liquid}$  at 26 GPa (Ohta et al., 2016) as shown in Figure 3.12a. This suggests that such a trend may extend to the  $\epsilon$ - $\gamma$ -liquid triple point.

The structural invariance (Shen et al., 2004) of liquid Fe at high  $P$  is consistent with report that the product of thermal expansivity and isothermal bulk modulus ( $\alpha K_T$ ) for Fe remains nearly constant at high pressures and temperatures (Wasserman et al., 1996). In the liquid late transition metals under pressure, Peierls/Jahn-Teller distortion (symmetry-breaking rearrangements of atomic structures) and  $s$ - $d$  electron promotion (Ross et al., 2007) leads to the existence of highly concentrated stable local structures that maximize packing density while lowering electronic binding energy. Although this phenomenon is considered to lower the melting slopes of Fe, Ni and Co, it may also be responsible for maintaining the constant electron mean free path in the liquid at the onset of melt (Silber et al., 2017). Indeed, it was found that the packing fraction along the melting curve of Fe remains nearly constant (Shen et al., 2004). For Ni, electron-electron scattering was discussed in the context of the Kadowaki-Woods ratio (Silber et al., 2017), which compares the temperature dependence of  $\rho$  to that of heat capacity of a particular metal (Kadowaki and Woods, 1986). The Kadowaki-Woods ratio indicates the presence of strong electron-electron scattering in heavy fermions and weaker scattering in a select group of transition metals (Jacko et al., 2009), including Fe and Ni. This suggests that the contribution of such scattering to overall  $\rho$  is not negligible, especially for liquid Fe at high pressure (Drchal et al., 2017; Pourovskii et al., 2017).

The jump in  $\rho$  between the last solid and first liquid ( $\Delta\rho_{l-s}$ ) decreases linearly from 3 to 5 GPa, and then increases at pressures above the 5 GPa  $\delta$ - $\gamma$ -liquid triple point (Figure 3.12b). We have not measured  $\rho$  of the  $\epsilon$ -phase nor the subsequent  $\Delta\rho_{l-s}$  at corresponding melting points. However, it can be reasonably expected, based on recent results (Gomi et al., 2013), that  $\rho$  of the  $\epsilon$ -phase saturates at high pressures (above 60 GPa). That would imply that  $\Delta\rho_{l-s}$  from the  $\epsilon$ -phase does not increase linearly at high pressures and it likely tapers off. Consequently, given the apparent effects of the  $\delta$ - $\gamma$ -liquid triple point on the  $P$ -dependence of  $\Delta\rho_{l-s}$ , in the absence of experimental results in the liquid above the  $\epsilon$ - $\gamma$ -liquid triple point  $P$ , it is not reasonable to speculate on the precise value of  $\rho$  in Earth's OC and at the ICB. However, we do not expect that  $\rho$  of liquid Fe, originating from a parent  $\epsilon$ -phase, would be considerably different from the value of approximately 120  $\mu\Omega\text{cm}$ , obtained for liquid Fe between 6 and 12 GPa in this study and corroborated by a similar value measured (Ohta et al., 2016) at 26 GPa. Nevertheless, the increasing magnitude of  $\Delta\rho_{l-s}$  (Figure 3.12b) implies that caution needs to be exercised in terms of estimating  $\rho$  of liquid Fe obtained from solid phase measurement and extrapolated to core conditions.

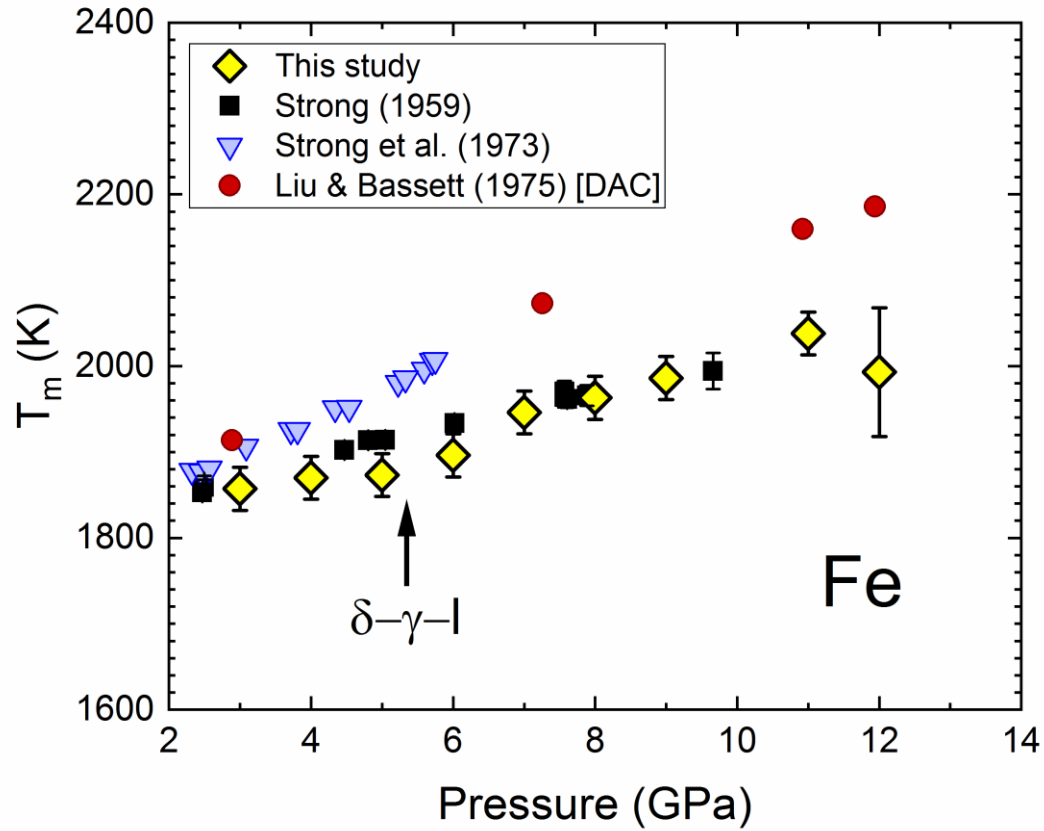




**Figure 3.12: Electrical resistivity of Fe along the melting boundary and the change in resistivity from solid to liquid. (a)  $\rho$  at the first melt for pressures 3 – 12 GPa, compared to the earlier results (as shown in the legend) obtained at 1 atm, 2.5, 3.8, 5.3 and 26 GPa. (b) The change in  $\rho$  on melting demonstrating an abrupt change at 5 GPa. The triple point (Strong et al., 1973) pressure is indicated by the arrow.**



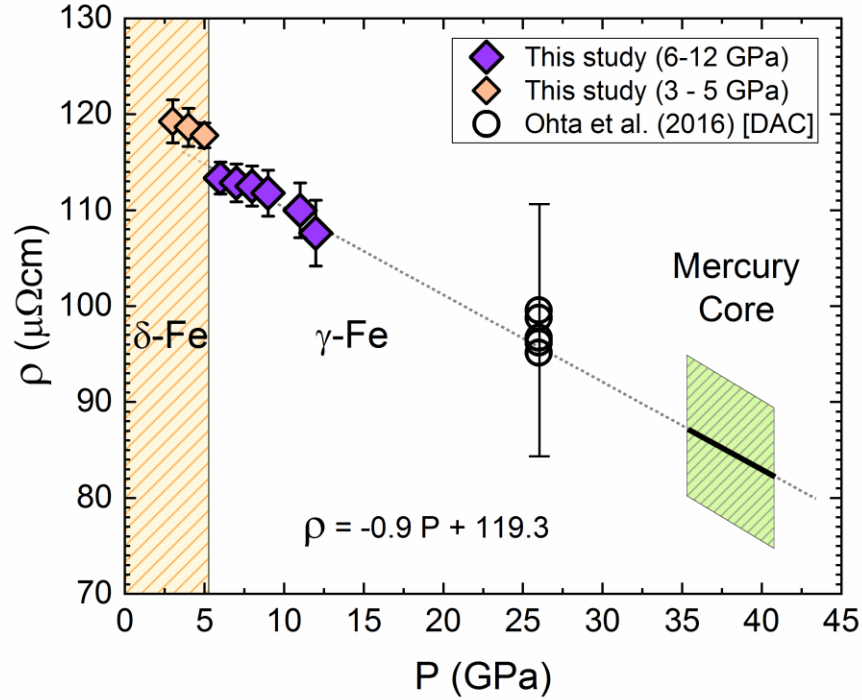
The melting curve ( $T_m$ ) determined by the jump in  $\rho$  during the solid-liquid phase transition is compared to available values in the literature (Figure 3.13). The  $T_m$  values obtained in this work agree well with one study (Strong, 1959) and are below the values compared to the other two (Strong et al., 1973; Liu and Bassett, 1975). However, there are no other literature data available for the low  $P$  melting curve of Fe, thus making the extent of uncertainties due to the choice of experimental set up in previous studies (Strong et al., 1973; Liu and Bassett, 1975) unclear, when compared with our values. It is important to note that the sensitivity of our measurements had sufficiently high resolution to detect the change in slope of the  $\delta$ -liquid and  $\gamma$ -liquid parts of the melting curve at the  $\delta$ - $\gamma$ -liquid triple point, as thermodynamics requires.



**Figure 3.13:** Melting curve of Fe from 3 to 12 GPa. The melting results, as inferred from  $\rho$  measurement, are compared with other studies. The triple point (Strong et al., 1973) pressure is indicated by the arrow.

### 3.4.2. Thermal Conductivity and Heat Flow in the Cores of Terrestrial Bodies

The findings have direct implications for constraining electrical and thermal transport properties in the cores of terrestrial bodies made of Fe. Mercury has both a solid inner and liquid outer core which generates a weak dynamo (Dumberry and Rivoldini, 2015). Pressure in the center of Mercury's solid  $\gamma$ -Fe inner core is about 36 GPa and the temperature is in the range (Dumberry and Rivoldini, 2015) 2200 – 2500 K. The pressures at the top of its liquid outer core, near the CMB range from approximately 5 to 8 GPa and temperature estimates (Hauck et al., 2013) are between 1850 – 2200 K. If we assume a linear decrease of  $\rho$  of solid  $\gamma$ -Fe phase just before melting (Figure 3.14), we obtain a value for  $\rho$  of  $87 \pm 10 \mu\Omega\text{cm}$  for an Fe core at the center of the planet. The electronic component of thermal conductivity ( $k_e$ ) is inversely proportional to  $\rho$  and can be calculated from the Wiedemann-Franz law,  $k_e = \frac{LT}{\rho}$ , using for the Lorenz number,  $L$ , the Sommerfeld value of Lorenz number,  $L_0 = 2.44 \times 10^{-8} \text{ W}\Omega/\text{K}^2$ , which has been shown to be a reasonably valid approximation (Secco, 2017) for Fe at Mercury's core, as well as to much higher (de Koker et al., 2012; Pozzo et al., 2013),  $P$  and  $T$ . For Mercury's solid core temperatures, the values of thermal conductivity of  $62 - 70 \text{ Wm}^{-1}\text{K}^{-1}$  are obtained. At the top of a pure liquid Fe outer core, the value of  $\kappa_e$  is calculated to be  $41 \pm 4 \text{ Wm}^{-1}\text{K}^{-1}$ . The range of thermal conductivity calculated in this study stems from the range of values used for temperatures of Mercury's CMB. The calculated value of thermal conductivity of  $41 \pm 4 \text{ Wm}^{-1}\text{K}^{-1}$ , using the measured value of electrical resistivity of liquid Fe at 5 GPa, is in very good agreement with a recently obtained value (Secco, 2017) of  $42.6 \text{ Wm}^{-1}\text{K}^{-1}$  based on measured thermal conductivity of for liquid Fe at 1atm along with added pressure-dependence of thermal conductivity, as well as a value of  $55 \pm 8 \text{ Wm}^{-1}\text{K}^{-1}$  obtained by first principles calculations (de Koker et al., 2012) at similar  $P, T$ .

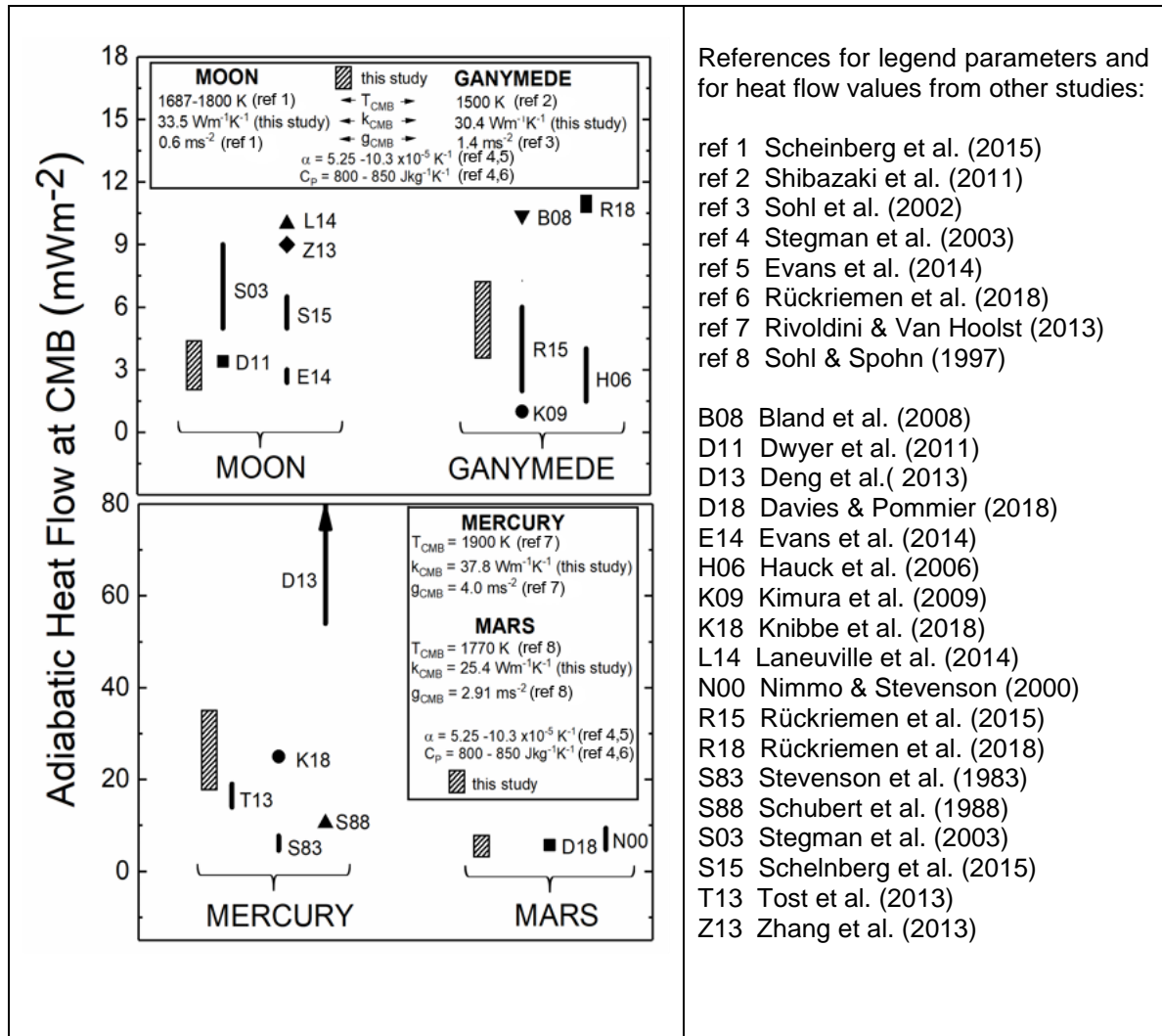


**Figure 3.14:** Values of electrical resistivity of  $\gamma$ -Fe just before melting.  $\rho$  of  $\gamma$ -Fe (6 – 12 GPa), just before melting, extrapolated to the Mercury core pressure, and compared to  $\rho$  (with error bars) of  $\gamma$ -Fe before melting at 26 GPa. Also, we show  $\rho$  of  $\delta$ -Fe (3 – 5 GPa) just before melt (the yellow shaded area on the left). The change in the trend between  $\delta$ -Fe and  $\gamma$ -Fe as a function of pressure is clearly visible. The green shaded polygonal area on the right represents the uncertainty in  $\rho$  and  $P$  at the center of Mercury’s core.

Similar calculations for the top of the liquid Fe cores of Moon, Ganymede, and Mars were carried out. Thermal conductivity values derived from the electrical resistivity measurements obtained in this work were used with values for thermal expansion ( $\alpha$ ), gravitational acceleration ( $g$ ), and heat capacity at constant pressure ( $C_P$ ) to calculate the adiabatic heat flow ( $q_{cond}$ ) on the core side of the CMB of these terrestrial bodies using the following equation:

$$q_{cond} = k_e \left( \frac{dT}{dr} \right)_{ad} = k_e \frac{\alpha g T}{C_P} \quad (3.1)$$

The ranges of adiabatic heat flow values are compared with several other studies (Figure 3.15). The parameter values used in our study are given in the figure legends.



**Figure 3.15: Comparison of values of adiabatic core heat flow at the CMB of Moon, Ganymede, Mercury and Mars. Values obtained in this study (hatched rectangles) were calculated using the parameter values given in the legends. The CMB pressures at which the heat flow values were calculated are: Moon - 4.9 GPa (Steinberger et al., 2015); Ganymede - 5.9 GPa (Hussmann et al., 2007); Mercury - 5.0 GPa (Rivoldini and Van Hoolst, 2013); Mars – 23 GPa (Sohl and Spohn, 1997).**

The range of values of heat flux conducted along the adiabat is usually attributed to poorly constrained values for thermal conductivity and thermal expansion (Davies and Pommier, 2018; Knibbe and van Westrenen, 2018; Rückriemen et al., 2015; Scheinberg

et al., 2015). Our experimentally measured values of electrical resistivity of liquid Fe at high pressures lead to robust thermal conductivity values and this focuses the source of the range of values of adiabatic heat flux on uncertainties in thermal expansion. All other parameters at the CMB of these bodies ( $g$ ,  $T$ ,  $C_p$ ) are known with sufficient accuracy to be responsible for only a few percent variation in the calculated conducted heat flux. The values of conducted heat flux for Ganymede and Mars are similar in range used in thermal evolution studies. The two high value ranges of conducted heat flux for Ganymede (Bland et al., 2008; Rückriemen et al., 2018) and the three highest values for the Moon (Laneuville et al., 2014; Stegman et al., 2003; Zhang et al., 2013) are caused almost entirely by the high values of thermal expansion ( $0.9\text{-}1.0 \times 10^{-4} \text{ K}^{-1}$ ) used in those studies. However, the range of values for the Moon, which also includes high thermal expansion, is lower than most previous studies of lunar thermal evolution. In part, this is due to the lower thermal conductivity value that we have determined in this study. The comparison for Mercury highlights that the values of conducted heat flow found in our study generally are higher than three previous studies (except for one study (Deng et al., 2013), wherein specific details on parameters used in their calculation of conducted heat flow were not provided). Two thermal evolution models (Knibbe and van Westrenen, 2018; Tosi et al., 2013) used adiabatic heat flux values that fall within our range of values. Most thermal evolution models show the heat flux through Mercury's CMB to be only a few  $\text{mW/m}^2$  and this is achieved within the first 1 Gyr (Grott et al., 2011; Hauck et al., 2004; Tosi et al., 2013) or even within the first few million years (Knibbe and van Westrenen, 2018). This means that the heat flow through the CMB is sub-adiabatic which suggests that the outer parts of Mercury's liquid core are thermally stratified (Dumbrery and Rivoldini, 2015). The highest values of adiabatic heat flux for Mercury, using the highest values of thermal expansion, would provide a stabilizing effect to the thermally stratified layer owing to the greater departure of the sub-adiabatic temperature profile from the adiabat. This would require greater secular cooling (over longer time period) for the sub-adiabat to intersect the core liquidus. In addition to a stabilizing effect, the high values of core adiabatic heat flux would lead to an increase in thickness of the thermally stratified layer. Both of these effects would slow the growth rate and increase the depth, respectively, of the core region in which Fe snow could develop.

The cores of small planetary bodies are often postulated to include some amount of light alloying elements (Collins and Johnson, 2014; Murchie et al., 2014; Sohl and Schubert, 2015; Van Hoolst and Rivoldini, 2014; Weber et al., 2011) such as S, Si, O or C. While it has been shown that S, Si, and C in Fe increases  $\rho$  for the solid phase at high pressures (Gomi et al., 2016; Kiarasi and Secco, 2015; Suehiro et al., 2017; Zhang et al., 2018), their effects on  $\rho$  of the liquid phase, and therefore on  $\kappa$ , has not been reported. Experimental measurements at 1 atm on Fe-Si compositions with 14-75 wt%Si show that at high Si concentrations,  $\rho$  in the liquid state is lower than for pure Fe and the temperature dependence of  $\rho$  in the liquid is negative (Baum et al., 1967). This unusual behavior needs to be investigated at high pressure before speculating on the effects on core thermophysical properties and dynamics. Since the results demonstrate an important effect of solid structure on the electrical resistivity of liquid Fe, a direct evaluation of  $k_e$  in the Earth's outer core awaits measurement of  $\rho$  (or more difficult  $\kappa$ ) for liquid Fe melting from the parent  $\varepsilon$ -phase.

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## Chapter 4

### 4. Heat Flow in Terrestrial Cores from Invariant Electrical Resistivity of Fe-Si on the Melting Boundary to 9 GPa

*Let the future tell the truth, and evaluate each one according to his work and accomplishments.*

*The present is theirs; the future, for which I have really worked, is mine.*

- Nikola Tesla

*A version of this chapter is being adapted for submission to a peer-reviewed journal:*

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#### 4.1. Introduction

Much of what makes life sustainable on Earth, from the strong magnetic field (e.g., Nimmo, 2015a; b), to mantle convection and subsequent plate tectonics (e.g., Olson et al., 2015; Olson, 2016), depends critically on the thermal conductivity and rate of heat transport in the Earth's core and across the core-mantle boundary (CMB) (Vocadlo, 2015). However, thermal conductivity ( $\kappa$ ) and related electrical resistivity ( $\rho$ ) of Earth's outer core (OC), composed of liquid iron (Fe) alloyed with lighter elements, still remain two of least constrained geophysical parameters (Williams, 2018). Thermal conductivity is inversely proportional to electrical resistivity via the Wiedemann–Franz law (e.g., Secco, 2017), and it controls the energy budget of the core (Gubbins et al., 2015; Davies, 2015). Therefore, better characterization of both of these parameters in the Earth's liquid OC is of great importance. For example, thermal conductivity modulates thermal convection in the OC, which is very sensitive to the rate of electron dominated heat conduction from the inner core boundary (ICB) to the CMB and the rate at which heat is

extracted by the mantle (Davies, 2015; Gubbins et al., 2015). Thus, the stability and a type of convection (thermal vs. compositional) depend closely on thermal conductivity (and related electrical resistivity), as well as viscosity of liquid Fe alloyed with yet unresolved combination of light elements (Davies et al., 2015). Additionally, the energy budget of the core and the rate at which that energy is extracted across the CMB imposes constraints on the nature of the geomagnetic field (Olson et al., 2015; Olson, 2016). The magnetic field is generated through the conversion of kinetic energy produced by the convecting molten alloy flows (e.g., Labrosse, 2015; Davies, 2015; Gubbins et al., 2015) into electrical energy. Moreover, the interpretation of the nature of the geomagnetic field which has existed for 3.5 - 4.2 Gyr (Tarduno et al., 2010; Biggin et al., 2015; Biggin et al., 2009; Tarduno et al., 2015), and the age of the solid inner core (IC) closely depend on the transport properties of the liquid Fe alloy (e.g., Gomi et al., 2013). This is because the thermal conductivity of the core controls the amount of heat conducted down the adiabat, and the higher its value, the faster is the growth rate of the IC (Davies et al., 2015).

However, the challenge of better constraining the transport properties of the liquid Fe alloy in the core is multi-faceted. The uncertainty in precise evaluation of both thermal conductivity and electrical resistivity of the Fe alloy in the OC is caused by and has effects on: i) The unresolved compositional makeup and proportions of light elements in the liquid OC (e.g., Litasov and Shatskiy, 2016); ii) The exact effects of light element alloying on the transport properties of the liquid Fe (e.g., Zhang et al., 2016a; Shibazaki and Kono, 2018); iii) The amount of heat flow across the CMB (e.g., Ammann et al., 2014; Nimmo, 2015a); iv) A large spread of estimated temperatures at the CMB and ICB (e.g., Andrault et al., 2011; Anzellini et al., 2013; Sakairi et al., 2017; Zhang et al., 2018a). Lastly, from the experimental perspective, reaching and maintaining the core temperatures ( $T$ ) and pressures ( $P$ ) for sufficiently long time, while maintaining liquid sample geometry and purity to collect resistivity data, are still not experimentally achievable (e.g., Williams, 2018).

Here I present results of electrical resistivity measurements on solid and liquid Fe-4.5 wt%Si (henceforth referred to as Fe-4.5Si) from 3 GPa to 9 GPa, and up to  $\sim 2200$  K, to evaluate the effect of low Si content on the resistivity and thermal conductivity of the

liquid Fe-alloy. Toward that end, it is important to first probe the behavior of liquid binary alloys such as Fe-Si to characterize their behavior and determine what conclusions can be made before attempting studies on ternary Fe alloys or even more complex liquid Fe systems at similar or even much higher pressures. This work is also a sensible step toward direct experimental efforts to resolve and understand the properties of liquid Fe-alloys at the core conditions.

This study is motivated by recent reports which show that the electrical resistivity of transition metals Co and Ni is invariant along the melting boundary (Ezenwa and Secco, 2017; Silber et al., 2017). The same trend is observed in Fe beyond the triple point of  $\sim 5.2$  GPa (Silber et al., 2018). Thus, it is sensible to ask if the liquid Fe-alloys (with low content of light elements) could exhibit the same behavior as the pure Fe liquid, and whether Matthiessen's rule holds along the melting boundary. Matthiessen's rule states that the  $\rho$  is additive, such that the total electrical resistivity is the sum of  $\rho$  resulting from imperfections in the crystal and  $\rho$  due to thermal motion of the metal ions in the lattice. Despite the fact that this study is conducted at low pressures relative to Earth's core, the results are crucial in identifying the nature of the phenomenon that exerts much stronger controls on the electrical resistivity of pure 3d transition metals and their alloys at much higher pressures. Based on the experimental results and the supporting evidence from recent developments in understanding of dynamics of liquid metals, I demonstrate that pressure dependent icosahedral short range order (ISRO) controls the mean free path of electrons in liquid Fe-alloys and governs the electrical resistivity in the outer core. To my knowledge, the effect of ISRO on electrical resistivity has not been considered before. Consequently, I postulate that this phenomenon enables prediction of electrical resistivity of liquid Fe-alloy at the ICB as the critical anchor solid-liquid point, which in turn enables a significantly better constrained interpretation of thermal conductivity at ICB and CMB and eliminates some of the uncertainties noted above.

However, it is necessary to first give a condensed background of the relevant aspects which introduce the uncertainty in the determination of electrical resistivity and thermal conductivity of the Earth's OC.

This chapter is organized as follows: in Section 4.2, I discuss the uncertainties imposed by incomplete understanding of compositional and alloying effects on thermal conductivity of the OC. The uncertainty in temperature profiles at the CMB is also discussed along with a brief review of electrical resistivity measurements. Sections 4.3 and 4.4 are dedicated to methods and results, respectively. The detailed interpretation and implications of the findings in the context of the results and the postulated phenomenon for the determination of thermal conductivity in the OC are discussed in Section 4.5. The conclusions are presented in Section 4.6.

## **4.2. Additional Challenges and Uncertainties in Constraining the Transport Properties of the Liquid Fe Alloys**

### **4.2.1 The Composition of the Outer Core**

In terms of composition, while it is well understood that the OC is composed of liquid Fe and ~5-10% Ni (almost indistinguishable from pure Fe), alloyed with a small fraction of lighter elements (Poirier, 1994), the exact combination and overall proportion of lighter elements remains unresolved (e.g., Vocado, 2015). The knowledge of the makeup and exact fraction of light elements in the OC, are required to satisfy the seismological (e.g., Badro et al., 2014; Zhang et al., 2016a), cosmochemical (e.g., McDonough and Sun, 1995) and geophysical (e.g., McDonough, 2003; Morard et al., 2013) constraints. Consequently, there is only a limited number of light elements whose combination (or even a singular presence) may satisfy those constraints: silicon (Si), sulfur (S), carbon (C), hydrogen (H), oxygen (O) and recently proposed magnesium (Mg). Numerous earlier studies aiming to characterize the light-element composition in the core presented a wide range of compositional estimates (e.g., Allègre et al., 1995; McDonough and Sun, 1995; Alfè et al., 2002; Badro et al., 2007; Sakai et al., 2006; Takafuji et al., 2005; Alfè et al., 1999; Huang et al., 2011; Badro et al., 2014; Zhang et al., 2016a).

Evidently, the debate on the core composition is still ongoing (e.g., Litasov and Shatskiy, 2016; Tateno et al., 2018). However, the consensus tilts toward Si as the major light element in the OC (e.g., Zhang et al., 2016a; Suer et al., 2017). This, of course, adds the geophysical interest in Fe-Si alloys in addition to and beyond traditional industrial applications (e.g., Numakura et al., 1972; Narita and Enokizono, 1979; Kita et al., 1994; Waseda et al., 1995; Gu et al., 2004; Qin et al., 2004; Shin et al., 2005; Cui and Jung, 2017). Cosmochemical abundance of Si in meteorites (Poirier, 1994; McDonough and Sun, 1995; Karato and Murthy, 1997; Murthy and Karato, 1997; Georg et al., 2007), mantle abundance and isotopic ratio in terrestrial rocks (e.g., Fitoussi et al., 2009; Georg et al., 2007; Shahar et al., 2009), higher sound velocity and higher bulk modulus in the core (Lin et al., 2003; Sanloup et al., 2004; Antonangeli et al., 2010; Mao et al., 2012; Badro et al., 2007; Tsuchiya and Fujibuchi, 2009), chemical affinity with the metallic phase and solubility in Fe at high pressures (e.g., Kuwayama and Hirose, 2004; Takafuji et al., 2005; Tateno et al., 2015), along with reduced density of the liquid Fe-Si alloy comparing to pure Fe (~8% in OC) (e.g., Zhang et al., 2016a), all make Si the likely dominant light element in the core (Hirose et al., 2013; Fischer et al., 2014; Litasov and Shatskiy, 2016; Zhang et al., 2016a). The estimates of the core Si content range from ~4 – 12% (Litasov and Shatskiy, 2016; Zhang et al., 2016a). However, plausible arguments presented to the contrary (e.g., Williams et al., 2015) show that the consensus on which minor element is dominant in the core has not been reached yet.

Si can stabilize the body centered cubic (bcc) phase of Fe (Cote et al., 2008). Si also has a stabilizing effect on the face centered cubic (fcc) and hexagonal close packed (hcp) phases of an Fe-Si alloy (Asanuma et al., 2008; Kuwayama et al., 2008; 2009; Tateno et al., 2010; Tateno et al., 2015) and its presence in amounts likely to be in the core does not significantly modify the melting curve of pure Fe (Asanuma et al., 2010; Fischer et al., 2013; Zhang et al., 2016a, 2018a). In addition, the solubility of Si in liquid Fe increases with pressure (Tateno et al., 2015).

On the other hand, the singular presence of Si in the Fe-Ni alloy in the OC is not plausible due to the same cosmochemical, geophysical and seismologic considerations discussed above that dictate the presence, albeit limited, of other light elements (Tateno



et al., 2018). For example, S is expected to play a dominant light element role in the cores of small planetary bodies such as Mercury, Mars, Ganymede and the Moon (see Sanloup et al., 2002; Pommier, 2018). Conversely, the experimental evidence shows that S cannot be a single light element in the core (Sata et al., 2010; Huang et al., 2013; Badro et al., 2014; Umemoto et al., 2014). Moreover, S is not expected to be present beyond 2 wt% in the Earth's core (McDonough, 2003; Suer et al., 2017). Similarly, C is suggested to be below 1wt% (Zhang and Yin, 2012; Dasgupta et al., 2013; Morard et al., 2014) because higher content of C in the core would, for example, require unrealistic C content in the Earth's mantle. However, the simplistic picture of the OC composition cannot address some most recent results (e.g., Deng et al., 2013; Tateno et al., 2018). Using the results from melting experiments in the Fe–S–C ternary and Fe–S–Si–C quaternary systems up to 20 GPa which show that S preferentially partitions into a molten core, Deng et al. (2013) concluded that the liquid OC will be S rich and Si poor, with only a moderate amount of C in both OC and IC. High pressure experimental results on Fe–C liquid alloys (Morard et al., 2017) further demonstrate that C is only a very minor constituent of the OC.

On the other hand, the results obtained by Mori et al. (2017) show that while the crystallization from the eutectic liquid with ~6 wt% S at 254 GPa can account for the core density deficit. These studies are in a reasonable agreement with the study by Suer et al. (2017), who conducted metal-silicate partitioning experiments at pressures 46-91 GPa and temperatures 3100 - 4100 K. The authors showed that S partition coefficients are an order of magnitude less than that from earlier studies and demonstrate that S is not a highly siderophile element at high pressures and temperatures. Additionally, oxygen may be present in the OC in quantities below ~2 wt%, while H, due to its volatility, is expected to be only a very minor component in the liquid Fe-alloy (Zhang et al., 2016a).

Further uncertainties of Si content within the makeup of the core light elements were recently introduced by Tateno et al. (2018), who considered the eutectic behaviour of ternary Fe-alloys near ICB. Their experimental melting study on Fe–Si–S (2.2-2.7wt% Si and 2.0-2.1wt%S) at OC pressures indicated that the liquid evolves toward a Si poor and S rich composition upon crystallization (Tateno et al., 2018). This suggests that the solid

alloy, crystallized from the liquid with such composition at the ICB, is more enriched in Si/S and consequently cannot satisfy the seismically required jump in density which is observed at the ICB (Tateno et al., 2018). Tsuno et al. (2018) showed that the C solubility in a molten alloy decreases with increasing presence of S. Similarly, it was demonstrated that recently proposed Mg (O'Rourke and Stevenson, 2016; O'Rourke et al., 2017) is present in the OC in likely negligible quantities (Du et al., 2017).

Clearly the debate is not settled yet over the exact light element composition in the outer core. This is indeed one of the factors responsible for the significant uncertainty in the evaluation of  $\rho$  and  $\kappa$  of potential liquid alloys in the OC. More fundamentally, the individual or combined effect of light elements on the transport properties of liquid Fe at low to moderate pressures and temperatures is not resolved. The major factor is the general absence of electrical resistivity measurements on liquid Fe-alloys (binary, ternary or higher order) at high pressures, which is primarily attributed to the associated experimental challenges (Williams, 2018).

#### **4.2.2. Electrical Resistivity and Thermal Conductivity of Fe and its Alloys**

The first reliable experimental  $\rho$  results on the effect of Si content in a solid Fe-alloy were reported by Yensen (1915). These results are still the benchmark for most of the studies at ambient pressure and temperature. Baum et al. (1967) measured electrical resistivity of Fe alloys at the ambient pressure and in the temperature range 800-1700° C. While some reported results on electrical resistivity at melting of Fe-Si are inconsistent with increasing Si content (e.g., Baum et al., 1967), the same authors also observed a negative temperature coefficient of electrical resistivity before melting. An anomalous temperature dependence of the electrical resistivity in Fe-7wt%Si was also reported by Nishino et al. (1993).

In contrast to the number of studies of  $\rho$  of Fe-Si alloys at ambient pressure, only a very limited number of high pressure experimental measurements of  $\rho$  and  $\kappa$  of liquid Fe and its alloys are reported in literature to date (e.g., Secco and Schloessin, 1989; Ohta et al., 2016; Silber et al., 2018), although a recent study using a multi-anvil press, following the

experimental design of Silber et al. (2017), is a step in the right direction (Pommier and Leinenweber, 2018).

The electrical resistivity on solid samples at pressures approaching that of the IC can be measured in a diamond anvil cell (DAC). Currently, a common approach of measuring  $\rho$  in DAC involves measuring the voltage drop on decompression and using the van der Pauw method to evaluate  $\rho$  at ambient temperature (Gomi et al., 2013,2016; Seagle et al., 2013; Zhang et al., 2018b). Such Values of  $\rho$  are then used in the Bloch-Grüneisen relation to account for the temperature effect on electrical resistivity (e.g., Seagle et al., 2013). In principle, while those authors measured  $\rho$  generally up to  $\sim 100$  GPa, the flattening of the resistivity curve allows extrapolation to much higher pressures. Most recently, the electrical resistivity of Fe alloy with 3 wt% S and 3 wt% Si was measured using the DAC method and the results indicate smaller contribution of S to  $\rho$  relative to Si (Suehiro et al., 2017). The contribution of C to electrical resistivity of Fe-alloy was reported to be stronger than S or Si (Zhang et al., 2018b). The overall results among different DAC-based experimental investigations are in a reasonable agreement for both pure Fe and Fe-alloys (e.g., Zhang et al., 2018b).

The values of  $\rho$  and  $\kappa$  estimated for pure Fe at the CMB range from  $\sim 60 - 130 \mu\Omega\text{cm}$  and  $\sim 67 - 145 \text{ W/mK}$ , respectively, while the addition of 9 wt% Si reduces thermal conductivity to  $\sim 41 - 60 \text{ W/mK}$  at the same pressure (Seagle et al., 2013). Gomi et al. (2013) reported the values of  $\kappa$  of Fe-4wt%Si to be  $90 \text{ W/mK}$  and  $148 \text{ W/mK}$  at CMB and ICB, respectively. The same authors also found the heat flow across CMB to be  $\sim 11 \text{ TW}$ . Moreover, Gomi et al. (2013) were the first to consider the contribution of the resistivity saturation at high pressure which suggests that the  $\rho$  at high pressure cannot exceed  $\sim 150 \mu\Omega\text{cm}$  (Gomi et al., 2016). An extensive review of the phenomena of saturation resistivity in metals at atmospheric pressure is given by Gunnarsson et al. (2003). Similar results were obtained from experiments on Fe-Si and Fe-Ni, where  $\rho$  and  $\kappa$  at the top of the core were evaluated at  $112 \mu\Omega\cdot\text{cm}$  and  $87 \text{ W/mK}$ , respectively, taking into account the chemically-induced resistivity saturation in the Earth's core (Gomi et al., 2016). Recently, resistivity saturation was modeled numerically for Fe-Si, Fe-S and Fe-O

alloys (Wagle et al., 2018) and shown that the Ioffe-Regel criterion of electron mean free path equal to the interatomic distance was reached at very high temperatures.

A common thread among all these experimental studies is that  $\rho$  of pure Fe and its alloys (at room temperature) increases significantly at  $P \geq 12$  GPa (corresponding to the bcc-hcp transition) and starts to decrease after about 20 GPa, generally tapering off toward a more stable value after 60 GPa. Furthermore, for most alloys, Matthiessen's rule is obeyed at high pressures and an ambient temperature. However, the validity of Matthiessen's rule at high temperatures is not well defined, although when the electrical resistivity approaches the saturation value, Matthiessen's rule breaks down (Gomi et al., 2016).

The corresponding theoretical studies have been somewhat more consistent with each other in estimating the  $\rho$  and  $\kappa$  of the OC. In ground-breaking work, Elsasser (1946) theoretically estimated electrical resistivity of the OC at  $100 \mu\Omega\text{cm}$ . Ever since then, the values of electrical resistivity of the OC have been continuously revised upward and downward (see Gomi and Hirose, 2015 for a review). Relatively recent high values of the resistivity at the CMB for Fe alloyed with Ni and Si ( $212 \mu\Omega\text{cm}$ ), were initially calculated by Stacey and Anderson (2001) on the basis of shock wave experiments (Matassov, 1977) and developed from the theoretical foundation formulated by Gilvarry (1956). These values for the electrical resistivity of the OC have been dramatically revised to about  $90 - 100 \mu\Omega\text{cm}$  as a result of the density-functional-theory-based molecular dynamics (DFT-MD) simulations (de Koker et al., 2012; Pozzo et al., 2012, 2013) for the considered Fe-alloy at the CMB. An even lower value of  $73.5 \mu\Omega\text{cm}$  was calculated for the pure Fe liquid at the CMB conditions (Pozzo et al., 2012). Similarly low values for  $\rho$  of liquid Fe at the CMB conditions were computed recently by Wagle and Steinle-Neumann (2018).

These recently revised theoretical and experimental values of  $\rho$  and derived  $\kappa$  are up to five times greater than the earlier values (e.g., Stacey and Anderson, 2001; Stacey and Loper, 2007) and impose much greater uncertainty in the type of convection in the OC needed to power the geodynamo (e.g., Gomi et al., 2013; Nimmo, 2015b; Davies, 2015;

Gubbins et al., 2015). The reason for the greater uncertainty is straightforward. Increasing the thermal conductivity means increasing the conductive heat loss from the core through the CMB, which in turn reduces the available energy to power the geodynamo (Davies et al., 2015). Moreover, higher thermal conductivity predicates a much younger inner core as it implies much faster growth (e.g., Gomi et al., 2013, 2016) relative to earlier estimates. This also has the effect of reducing the power available to the geodynamo throughout its existence via chemical convection as a result of IC growth over a limited lifespan.

However, a recent experimental study (Konôpková et al., 2016) reported convincing results that are contrary to the recent theoretical and experimental estimates of thermal conductivity of Fe (e.g., Pozzo et al., 2012; de Koker et al., 2012; Ohta et al., 2016; Gomi et al., 2013; Seagle et al., 2013). In direct measurement of  $\kappa$ , Konôpková et al. (2016) employed a heat pulse propagation through a solid Fe sample after heating with a nanosecond laser pulse and demonstrated that the  $\kappa$  for pure Fe at the CMB conditions ( $33 \pm 7$  W/mK) is closer to the values discussed by Stacey and Anderson (2001) (46 W/mK) than to the recently revised and theoretically calculated values. In another study, Silber et al. (2018) demonstrated that the electrical resistivity of liquid Fe is likely to remain constant along the melting boundary up to the  $\gamma$ - $\epsilon$ -liquid transition at about 80 GPa. These results indeed show a renewed need for a rigorous evaluation of the electrical and thermal transport properties of liquid Fe-alloys at high pressure.

Finally, I address the uncertainties in a wide range of the values of the heat flow across the CMB imposed by estimates of thermal conductivity (Ammann et al., 2014; Olson et al., 2015) and the melting temperature of Fe-alloy in the same region (e.g., Andrault et al., 2011; Anzellini et al., 2013; Davies et al., 2015; Olson, 2016). An upper and lower limit on the melting temperature of Fe-alloys in the OC may be inferred with respect to the lower mantle solidus. However, the estimates of the lower mantle solidus range from  $3570 \pm 200$  K (Nomura et al., 2014) to  $\sim 4150 \pm 150$  K (Fiquet et al., 2010; Andrault et al., 2011). The presence of light elements in Fe is expected to depress the melting curve relative to pure Fe as illustrated by Zhang et al. (2018a). On the other hand, some

experimental results at high pressure suggest that addition of 9wt%Si causes the melting of Fe-Si alloy at higher temperatures relative to pure Fe (e.g., Fischer et al., 2013).

The rate at which the top of the OC releases thermal energy into the overlying base of the mantle is controlled by the temperature difference between the core and the interior of the mantle and depends on the thermal conductivity of the mantle mineral phases, perovskite post-perovskite and ferro-periclase (Ammann et al., 2014). As noted earlier, the rate of such cooling affects the type of convection in the core and potential stratification at the top of the core (e.g., Gubbins et al., 2015). In the lower mantle, perovskite has relatively low thermal conductivity in comparison to the post-perovskite phase, which is found in the D'' region (Hirose et al., 2015). The heat flux across the CMB is thought to be enhanced across the D'' region. However, there are still appreciable uncertainties in the values of thermal conductivity of the lower mantle minerals (Ammann et al., 2014; Ohta et al., 2017; Hsieh et al., 2017). Additionally, thermal conductivity of ferropericlase in the lower mantle can be reduced by Fe substitution and spin crossover (Ohta et al., 2017; Hsieh et al., 2017).

Thus, an indirect reliance on these parameters, because of the inherent uncertainties, may skew the estimated values of thermal conductivity of liquid Fe-alloy in the core, and illustrates the need for direct experimental measurements of  $\rho$  and  $\kappa$  of liquid Fe-alloys at high pressures.

## 4.3. Methods

### 4.3.1. Experiments

A 0.1 m length of high purity Fe-Si wire with  $4.5 \pm 0.1\text{wt}\%\text{Si}$  (or 8.6 at% Si) was supplied by special order from ChemPur Corporation (<https://chempur.de>). The starting sample wire exhibited a high degree of brittleness and hardness as is common in an alloy with similar Si content (Mohri et al., 2017). The detailed description of the experimental

procedure of the high pressure-temperature runs is given elsewhere (Silber et al., 2017, 2018), therefore only a brief discussion is given here.

Prior to emplacing the Fe-Si cylindrical sample into a high density, thick walled ceramic tube, the sample was carefully polished in such way that the diameter matched the inner diameter of the ceramic tube. Separately, the samples and the hosting ceramic tubes were also meticulously cleaned in ethyl alcohol ultrasonic bath to remove any contaminants. The ceramic tube was used to constrain the radial geometry of the molten sample, while W-discs on each end were used to contain the melt, preserve axial geometry and ensure contact with thermocouple wires/current leads during the experiments. Prior to being loaded into the 3000 ton large volume multi-anvil press, the assembled octahedra cells were heated in a vacuum furnace at about 420 K for 12 hours. The description of the octahedron cell, internal component details and setup are given in Silber et al. (2017, 2018). The average sample length was  $1.5 \cdot 10^{-3}$  m. Upon compression, a 4-wire method of recording the temperature and voltage decrease separately across the sample was used, while maintaining a constant current of 0.5 A. The DC power source was a Keysight B2961A, and DC voltages were recorded using a Keysight 34470A digital multimeter, and the associated BenchVue software. A manual polarity switch was used in all experiments to account for any contribution to the voltage due to potential temperature differences between the two thermocouple junctions. Before conducting resistivity measurements, each sample was preheated at the run pressure to 1000 K and cooled slowly to ensure full contact between the W26%Re/W5%Re thermocouple wires, W-disc and a sample situated in the middle. Preheating to higher or lower temperatures did not affect the starting value of  $\rho$ . The electrical resistivity values were obtained through Ohm's and Pouillet's laws. The melting curve boundary was identified based on the onset of the discontinuity in the resistivity curve typically associated with melting. Multiple runs at each pressure were conducted to ensure repeatability of the phenomena and overall repeatability of data, especially for pressures 3-5 GPa, where the electrical resistivity does not exhibit any significant jump at the melt.

The uncertainties were calculated using the well-established method (Bevington and Robinson, 2003), as described in detail in Silber et al. (2017, 2018). The uncertainties

reflect the standard deviation between the absolute value of positive and negative polarity voltage readings and account for the length changes during the compression and heating. Pressure- and temperature-related uncertainties, while very small, were also included in calculation.

### 4.3.2 EMP Analyses

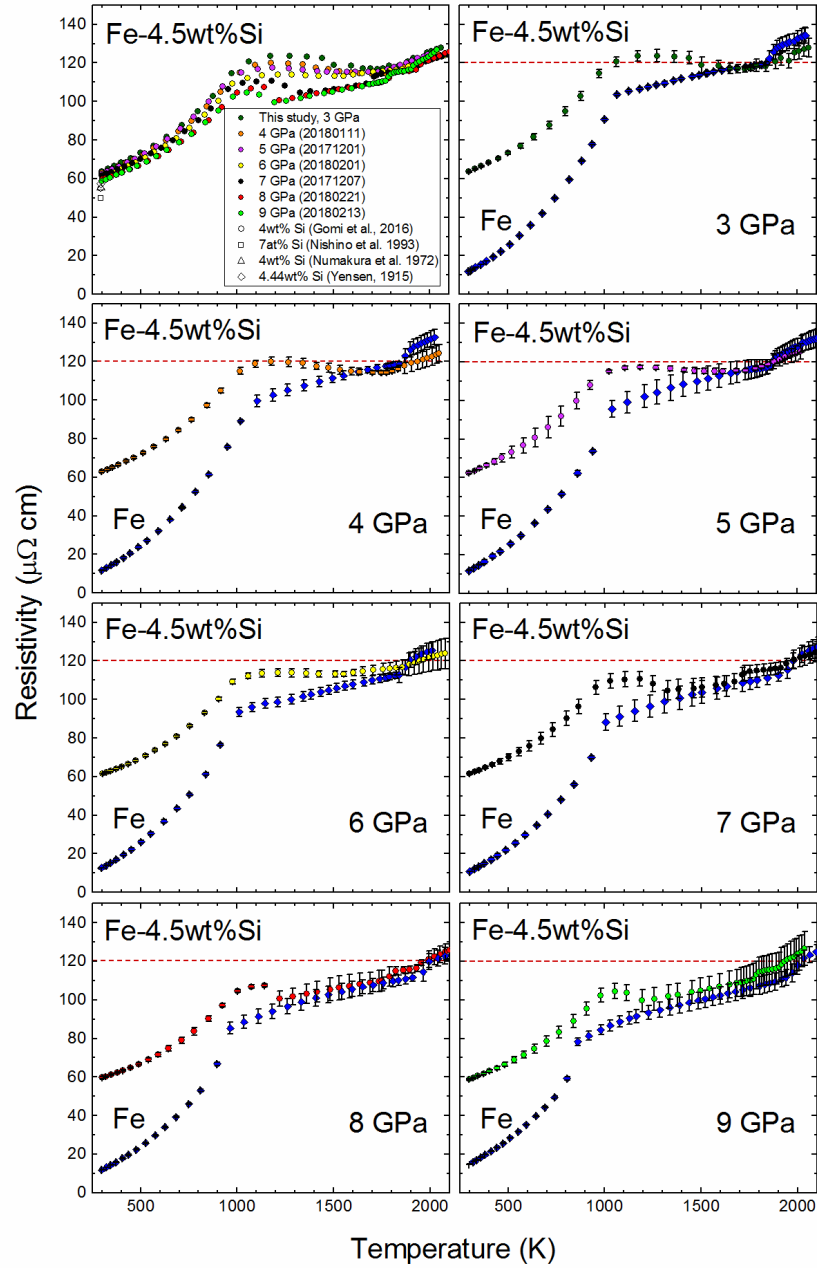
The EMP analysis was done at the Centre of Planetary Science & Exploration, Western University, London, Ontario, Canada. A starting sample wire was probed by JEOL JXA-8530F Electron Microprobe (EMP) to evaluate the purity and homogeneity. For all the analyses, an accelerating voltage of 20 kV, a probe current of 50 nA, and a spot size ( $\sim 100$  nm) beam were used. To test for diffusion and contamination from a W-disc, the post-experimentally recovered samples, initially compressed to the same pressure and heated to the melting point and significantly above the melting point (1950 K and 2100 K), were subsequently probed by EMP. In any measurement of  $\rho$ , it is important to mitigate the contamination. Thus, the main concern in this study was potential contamination from W disc and from the sample container. However, one of the simple ways to mitigate the contamination of the liquid sample due to diffusion is to conduct rapid data collection in the liquid. In principle, throughout this study, the duration of a sample in the liquid state was generally on the order of seconds.

## 4.4. Results

### 4.4.1. Electrical Resistivity of Solid Fe-4.5Si Alloy

The electrical resistivity of Fe-4.5Si in the pressure range 3 – 9 GPa is shown in Figure 4.1. The initial starting values of  $\rho$  at room temperature closely agree with Yensen (1915), Baum et al. (1967), Numakura et al. (1972) and Nishino et al. (1993) for the similar Si content, and are in line with values for 4 wt% Si (Gomi et al., 2013) all at 1 atm. The comparison with Fe shows that the starting resistivity of Fe-4.5Si alloy at 3-9 GPa is by a factor of  $\sim 6$  greater than that of pure Fe.





**Figure 4.1:** Electrical resistivity of solid and liquid Fe-4.5Si from 3 to 9 GPa, and compared with pure Fe at each  $P$ . The dashed line indicates the  $\rho$  of  $120 \mu\Omega\text{cm}$  which corresponds to the  $\rho$  of Fe-4.5Si at melting boundary for all  $P$ . For comparison purposes, the values of  $\rho$  at room temperature and 1 atm by other authors are also included (Yensen, 1915; Numakura et al., 1972; Nishino et al., 1993; Gomi et al., 2016).

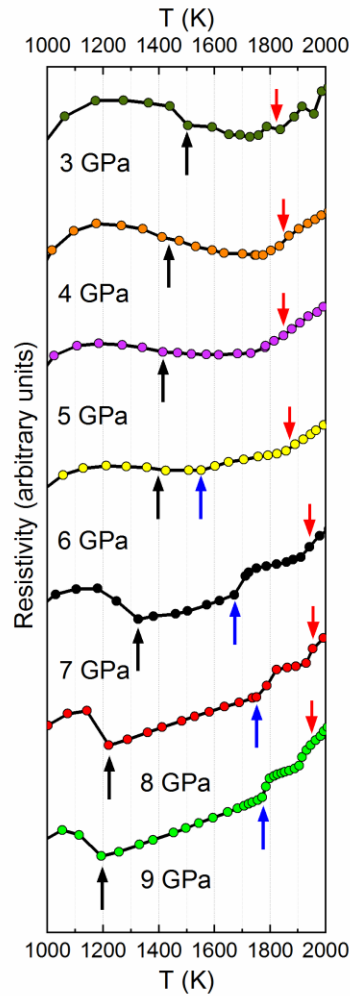
From the Fe-Si phase diagram (Kubaschewski, 1982; Cui and Jung, 2017), Fe-4.5Si has body centered cubic structure (bcc) which is generally referred to as the A2 phase. At ambient temperature,  $\rho$  of the Fe-4.5Si A2 phase exhibits a small and steady decrease between 3 – 9 GPa which is consistent with early studies (e.g., Balchan and Drickamer, 1961), but diverges from the recent trend observed in DAC measurements (e.g., Seagle et al., 2013; Gomi et al., 2013).

Fe-4.5Si is a ferromagnetic alloy prior to reaching the Curie temperature ( $T_C$ ), where magnetism, like in other transition metal alloys, originates from a partially filled spin polarized 3d band. Before the onset of the Curie temperature,  $\rho$  of the A2 phase in the experimental pressure range 3-9 GPa exhibits the influence of strong spin scattering of conduction electrons similar to the behavior of pure Fe, Ni and Co (Secco and Schloessin, 1989; Silber et al., 2017, 2018; Ezenwa and Secco, 2017) (Figure 4.1).  $T_C$  marks the temperature at which the Fe-alloy loses its long range magnetic spin moments. This transition is generally associated with the marked change in resistivity as evidenced in this study and earlier studies (e.g., Secco and Schloessin, 1989; Silber et al., 2017, 2018).

Consequently, the effects of pressure on  $\rho$  are more pronounced in the region of  $T_C$  (Figure 4.1) where the peak in the resistivity curve is significantly depressed by pressure. The value of  $T_C$  evidently decreases with increasing pressure. However, above  $T_C$ , electrical resistivity of the paramagnetic A2 phase of Fe-4.5Si starts to strongly diverge from the typical resistivity trend of Fe. Instead of tapering off and continuing a slow but steady increase following the peak value just above  $T_C$ , the electrical resistivity of Fe-4.5Si starts to decrease, exhibiting a negative temperature coefficient of  $\rho$ . The decrease in  $\rho$  is both  $T$  and  $P$  dependent (Figure 4.1). This agrees well with earlier studies which reported the same anomalous behaviour of electrical resistivity of Fe-Si alloys (Baum et al., 1967; Nishino et al., 1993).

The negative slope of  $\rho$  in the paramagnetic A2 phase changes at the temperature point which exhibits a strong pressure dependence. The temperature, which corresponds to the change of resistivity slope, decreases steadily with  $P$  as shown by the black arrows in Figure 4.2. Remarkably, that temperature coincides with the melting temperature of Si

(e.g., Kubo et al., 2008), which would imply a structural change in the solid Fe-Si alloy at corresponding temperature and pressure. It is relevant to note that upon melting, the coordination number in pure Si increases from 4 (diamond structure) to 6 in the liquid state. While this does not imply partial melting of Si within the alloy but rather implies an important structural change associated with the Si component that can be interpreted based on its pure form which assumes metallic character upon melting.



**Figure 4.2:**  $P$  and  $T$  dependent behaviour of  $\rho$  which changes at the onset of different phases. The transition from disordered bcc to the mixed phase (3-5 GPa), and to the fcc phase (6-9 GPa), is marked by the black arrows pointing up. This transition closely matches the melting of pure Si which is characterized by the coordination number change from 4 to 6. A change from the fcc phase to another mixed phase is marked by the blue arrow pointing up. The melting points are marked by down-pointing red arrows.

An interesting feature of the electrical resistivity of Fe-4.5Si is observed following the transition to a positive slope. In that temperature region (Figure 4.1 and 4.2), the electrical resistivity of Fe-4.5Si almost lines up with  $\rho$  of pure fcc-Fe at the same pressure. It should be noted that in the pressure range 3 - 5 GPa, the slope of resistivity changes gradually, while at pressures 6-9 GPa, the change is discontinuous. At pressures 3-5 GPa, the temperature range where the resistivity of Fe-Si matches that of pure Fe is relatively small and matches  $\rho$  of pure Fe almost perfectly. On the other hand, at higher pressures, that transitional region starts to broaden significantly and is sharply delineated by the discontinuous trends in the resistivity curve (Figure 4.2). Additionally, at pressures 6 - 9 GPa in the aforementioned temperature range, the resistivity of Fe-4.5Si mirrors the trend of pure Fe almost perfectly, although it exhibits a slightly increased value relative to pure Fe.

It is widely accepted that the scattering of an electron wave from a lattice irregularity impacts the electrical resistivity. Consequently,  $\rho$  strongly reflects the level of ordering in the solid (e.g., Numakura et al., 1972; Narita and Enokizono, 1979). It should be noted that the  $P$ - and  $T$ -dependent region where  $\rho$  of Fe-4.5Si matches the behaviour of Fe corresponds to the Fe fcc phase. Thus, it is reasonable to conclude that the Fe-4.5Si sample also has the fcc structure. This is especially true above 5 GPa. For the pressure range 3-5 GPa, such interpretation is slightly more difficult and cannot be made with certainty.

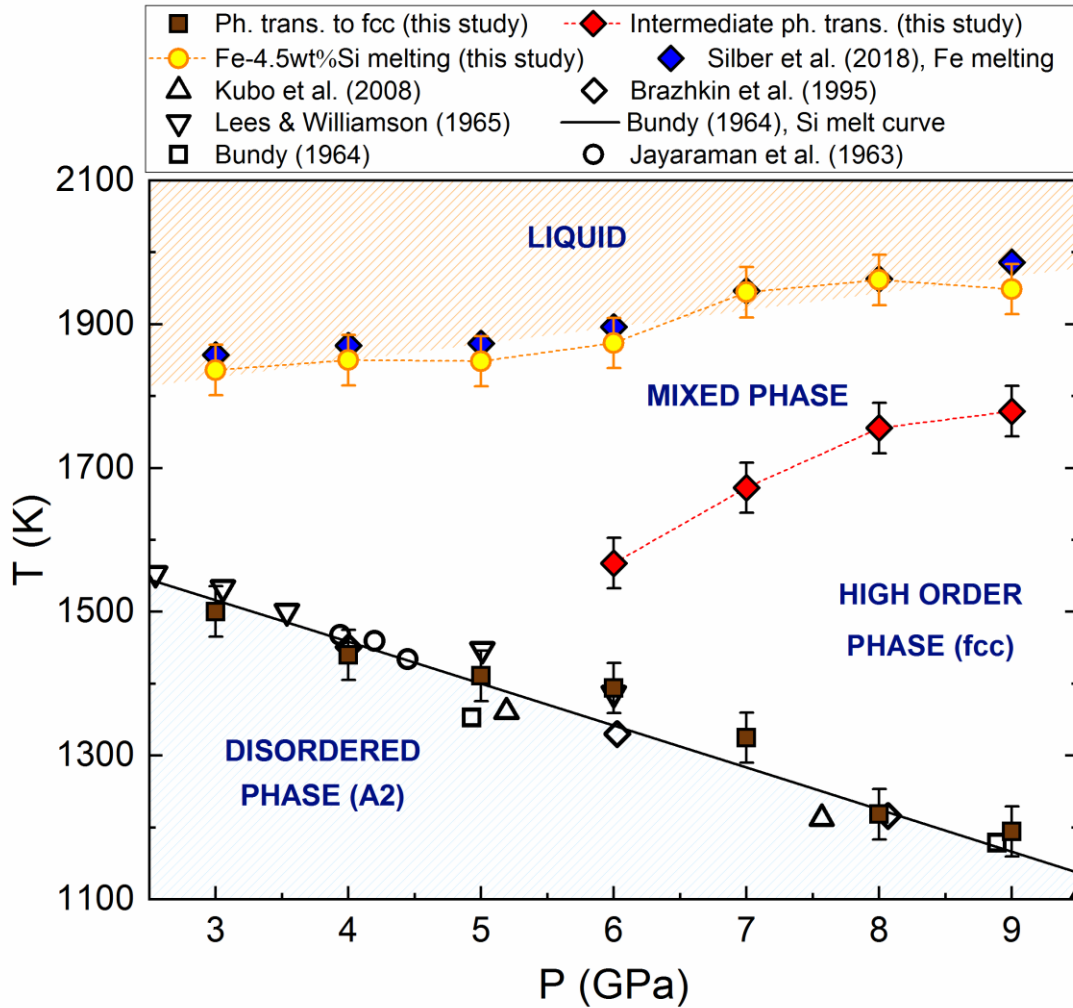
On the other hand, the appearance of the fcc phase at  $P > 5$  GPa is not surprising, as it has been observed in an Fe-alloy with a much higher Si content and at pressures beyond 80 GPa (Fischer et al., 2013). This implies that at high pressures, the fcc A1 phase of an Fe-Si alloy which is generally present only up to ~3.8wt% Si at 1 atm (Cui and Jung, 2017), starts to broaden and becomes prominent in the region below the melting curve and at high  $P$ . However, it should be emphasized that the  $P$ - $T$  phase space for the considered Fe-Si alloy is still poorly defined and there is no adequate analogue in literature, especially below 20 GPa.

#### 4.4.2. Melting Points and Phase Diagram of Fe-4.5Si for Pressures 3-9 GPa

Based on the behaviour of the electrical resistivity of Fe-4.5Si (Figures 4.1 and 4.2), a rather simplistic  $P$ - $T$  phase diagram of Fe-4.5Si (Figure 4.3) has been constructed. The transition from the disordered bcc paramagnetic phase into the mixed phase (below 5 GPa) and the fcc phase (6-9 GPa) is clearly observed. However, in the pressure range 3-5 GPa, the exact structural nature of the region above the transition from the disordered A2 phase (which coincides with the Si melting curve) cannot be resolved further in this study. From the analysis of the Fe-Si phase diagram (Cui and Jung, 2017), it can be reasonably expected that this region below 5 GPa is a mixture of the bcc and fcc phases. The same can be said for the region above the fcc phase that can be clearly identified (Figure 4.2) at pressure range 6 - 9 GPa.

At  $P > 6$  GPa, electrical resistivity jumps again at the end of interpreted fcc phase and starts again to exhibit a trend similar to that of pure Fe (Figure 4.1), where the mixed phase at  $T > 1700$  K resumes the same slope of the electrical resistivity. This jump in resistivity is identified as melting. In this pressure range, the melting is characterized by the presence of an initially small jump in  $\rho$ , which eventually approaches the magnitude of the jump of a pure Fe at 9 GPa. The subsequent slope of  $\rho$  in the liquid matches that of pure Fe.

However, at pressures 3-5 GPa, determination of the melting point is not as trivial. While the resistivity of Fe-4.5Si at 3 GPa exhibits a very small decrease (Figure 4.2), after which it resumes the same slope as pure Fe, at pressures of 4 and 5 GPa the transition to liquid is almost indistinguishable. The behaviour of  $\rho$  at melting at 4 GPa is detected by a small, yet distinct discontinuity in the slope. That change in slope is barely detectable at 5 GPa, where the trend in  $\rho$  is almost linear during melting. It is important to emphasize that this anomalous behaviour has been validated in multiple experiments for each pressure point, and the same trend was replicated in all runs.

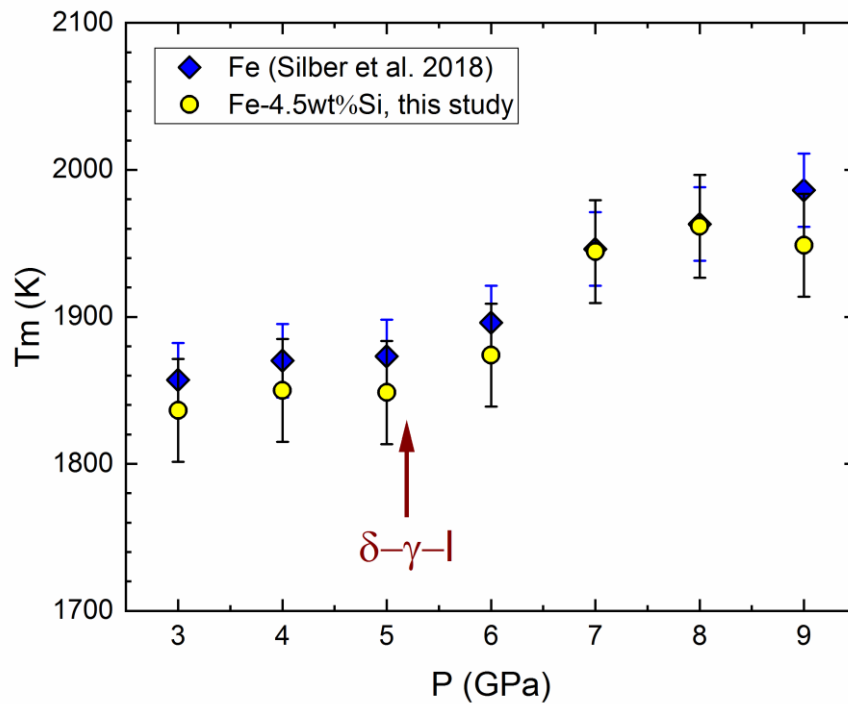


**Figure 4. 3: Simplified  $P$ - $T$  phase diagram of Fe-4.5Si from 3 GPa to 9 GPa and up to 2100 K, interpreted from observed behavior of electrical resistivity. A2 (left corner) corresponds to paramagnetic bcc phase. The transition to mixed phase (3-5 GPa) and fcc phase (6-9 GPa) coincides with the melting boundary of pure Si. Mixed phase which occurs before melting, for pressures 6-9 GPa is also shown. The melting boundary for Fe-4.5Si is slightly lower than for pure Fe, but it follows the same trend.**

The plotted melting points of Fe-4.5Si (Figure 4.4) closely follow the melting curve trend of pure Fe in the given pressure range (Silber et al., 2018) which is perhaps not surprising with the low Si content. However, the presence of 4.5wt% Si suppresses slightly the melting temperature of the alloy which is consistent with the melting  $T$  of Fe-4.5Si at 1atm. It was observed that Fe-4.5Si melts on average at temperatures  $\sim 20$  K below that

of pure Fe. At the moment, I am not aware of any reported melting curve for this particular alloy and at pressures below 20 GPa. However, the comparison of these results with an extrapolated melting curve from a range of values reported in literature for different Fe-Si alloys and much higher pressures, yields a reasonable agreement (e.g., Kuwayama and Hirose, 2004; Kuwayama et al., 2009; Asanuma et al., 2010; Morard et al., 2011; Fischer et al., 2013).

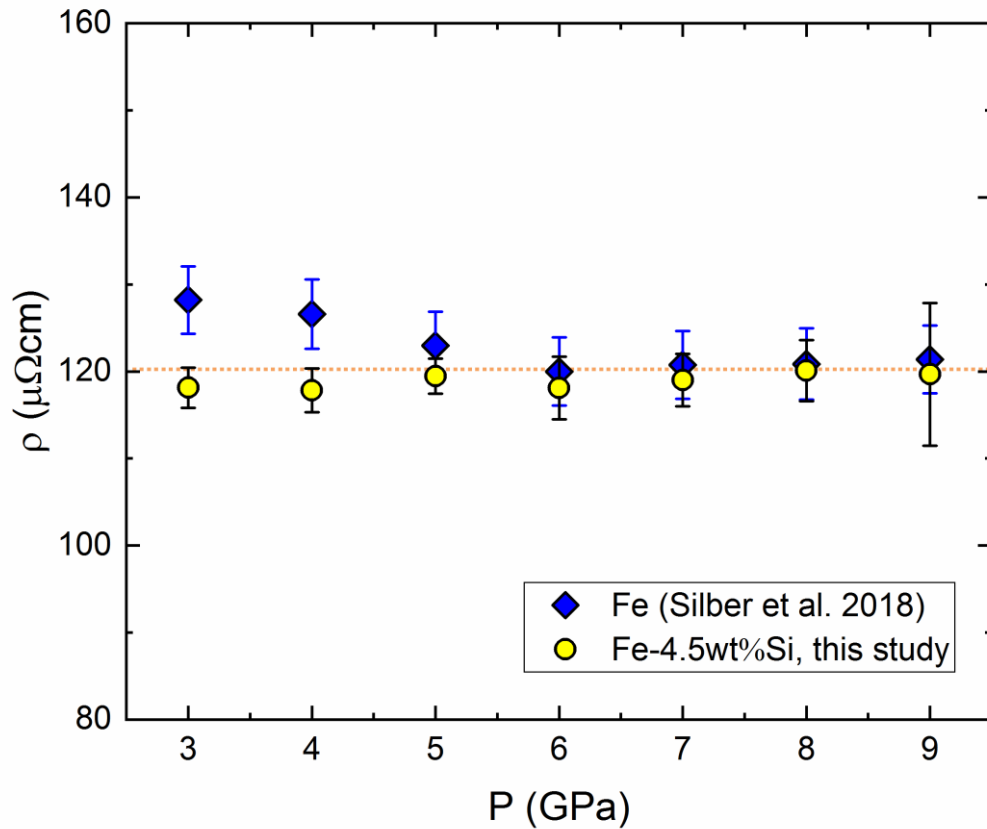
A change in the melting curve at a pressure above approximately 5 GPa (Figure 4.4) was observed. This behaviour is well known in Fe and Fe-alloys, and it is attributed to the structural change associated with the presence of the triple point ( $\delta$ - $\gamma$ -liquid) at 5.2 GPa (Sanloup et al., 2000a, 2011; Terasaki et al., 2010; Shimoyama et al., 2013; Shibazaki et al., 2015; Silber et al., 2018).



**Figure 4. 4:** The melting curve of Fe-4.5Si compared with that of pure Fe (Silber et al., 2018). The change in slope of melting line is clearly seen in both Fe-4.5Si and pure Fe at ~5 GPa indicating the presence of triple point. The presence of this observed phase transition in Fe-4.5Si is analogous to  $\delta$ - $\gamma$ -liquid in pure Fe.

#### 4.4.3. The Electrical Resistivity of liquid Fe-Si Along the Melting Boundary

The most remarkable observation in this work is that  $\rho$  of Fe-4.5Si remains invariant at  $\sim 120 \mu\Omega\text{cm}$  from 3-9 GPa along the melting line (Figure 4.5). This value of  $\rho$  is almost identical to that of pure liquid Fe (within uncertainties) above 6 GPa (Figure 4.5). This behaviour is unexpected as it violates Matthiessen's rule. That is, the additional resistivity arising from the impurity (Si solute) component that Matthiessen's rule predicts is not observed.



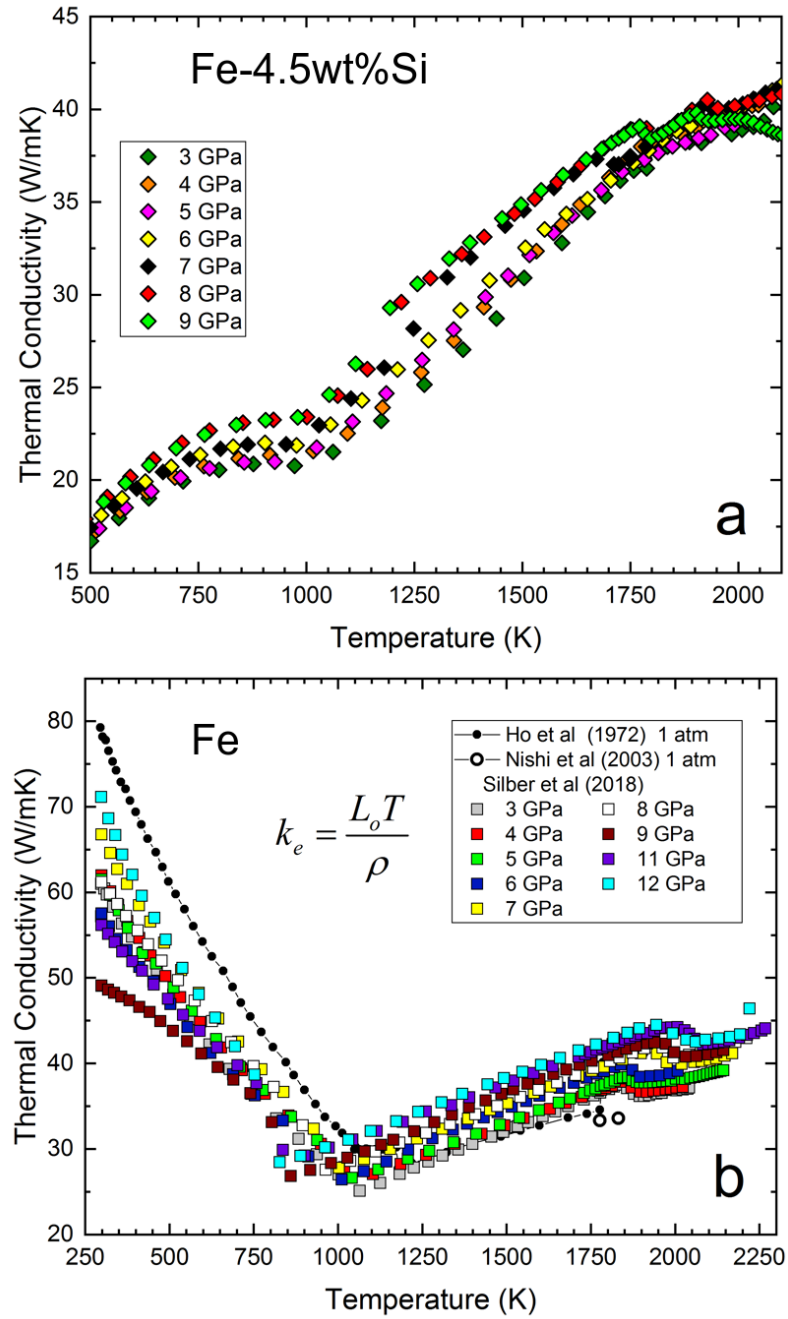
**Figure 4.5:** Electrical resistivity of Fe-4.5Si along the melting boundary (3-9 GPa) compared with that of a pure Fe. For Fe-4.5Si,  $\rho$  remains constant (within experimental uncertainties) at the onset of melt and in specified  $P$  range. Electrical resistivity of Fe-4.5Si diverges from pure Fe from 3-5 GPa and matches  $\rho$  of liquid Fe at  $P \geq 6$  GPa.



Figure 4.5 shows that  $\rho$  of pure Fe along the melting boundary starts at a higher value at 3 GPa and decreases steadily toward the  $\delta$ - $\gamma$ -l triple point at  $\sim 5.2$  GPa, after which it remains constant at  $\sim 120 \mu\Omega\text{cm}$ . On the other hand, the  $\rho$  of liquid Fe-4.5Si remains constant ( $\sim 120 \mu\Omega\text{cm}$ ) throughout the full experimental pressure range along the melting boundary. The divergence between the electrical resistivity of liquid Fe and Fe-4.5Si along the melting boundary prior to  $\sim 5.2$  GPa can be, in part, attributed to the effect of the parent solid phase on the initial structure of liquid (Silber et al., 2018). Prior to reaching the triple point, Fe melts from the bcc phase, while after the phase transition, it melts from the more energetically preferred fcc phase.

However, this explanation is not sufficient to account for the  $\rho$  behaviour of Fe-Si along the melting boundary as it is assumed that it melts from the mixed phase. It is well understood that solid Fe undergoes the phase transition near melting from bcc to fcc phase at 5.2 GPa. Despite the fact that the presence of Si stabilizes the bcc structure of Fe (Cote et al., 2008) and subsequently affects the behaviour of liquid, it does not explain the observed  $\rho$  along the melting line since Fe melting from a bcc structure shows decreasing resistivity along the melting boundary. This suggests the existence of a more subtle mechanism that acts on the atomic scale and modulates the behaviour of charge carriers as discussed later.

For illustrative purposes, the calculated  $\kappa$  of Fe-4.5Si is shown in Figure 4.6a, and contrasted with the  $\kappa$  of pure Fe in Figure 4.6b (Silber et al., 2018).



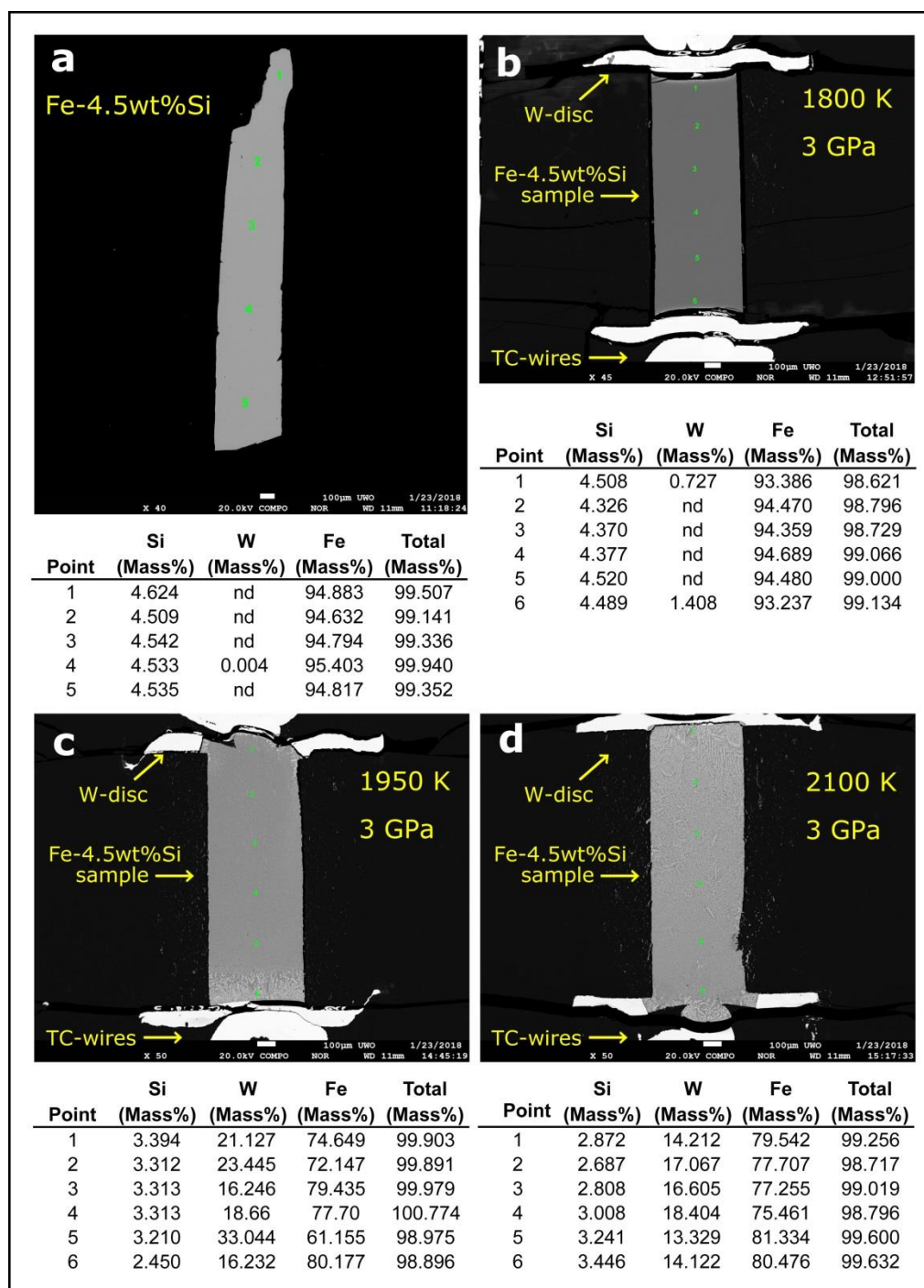
**Figure 4.6:** (a) Thermal conductivity of solid and liquid Fe-4.5Si at pressures 3-9 GPa. For comparison,  $\kappa$  of pure solid and liquid Fe (b), plotted against values of  $\kappa$  obtained at atmospheric  $P$  (Ho et al., 1972; Nishi et al., 2003).

#### 4.4.4. EMP and Sectioned Samples

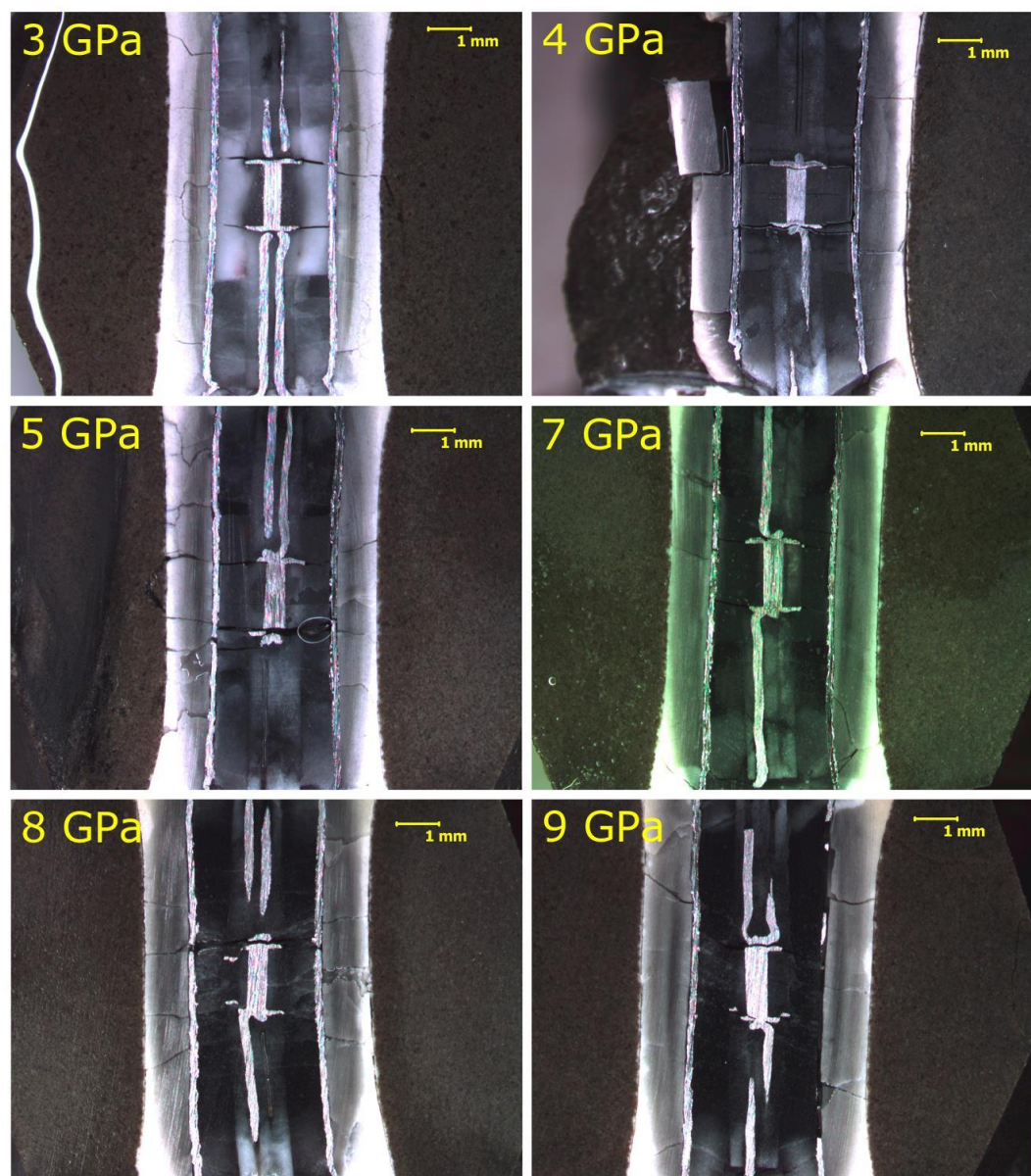
The EMP results are shown in Figure 4.7. The most relevant observation was that there was negligible contamination due to diffusion at melting (Figure 4.7b). This is important since the main goal was to measure  $\rho$  of Fe-Si along the melting boundary. The presence of only very limited surface diffusion of W (Figure 4.7b) in the samples at the melting point adds confidence in our  $\rho$  measurements along the melting boundary. No appreciable diffusion from the container into our samples was detected at the melting points. It should be also noted that no W diffusion is detected throughout the full temperature range in solid Fe-4.5Si due to very short exposure times to high temperatures. This is completely consistent with the earlier observations made in pure Fe (Silber et al., 2018).

However, higher temperatures and longer exposure times promote a higher rate of W diffusion into liquid Fe-Si samples. This is shown in Figures 4.7c and 4.7d, where the gradual progress of diffusion can be seen with rising temperature which also requires long duration in the liquid state. While this reduces confidence in our  $\rho$  data measured at temperatures far above the melting line, lack of diffusion ensured that  $\rho$  data close to the melting boundary was on pure Fe-4.5Si.

Figure 4.8 illustrates the preserved geometry of the Fe-4.5Si samples used in this study. These were compressed to pressures 3-9 GPa and heated to temperatures significantly above the melting point. The recovered geometries were examined and compared with the dimensions of the initially prepared sample. Indeed, the recovered geometries were used to calculate the  $\rho$  via Pouillet's law. It is important that the recovered sample dimensions exhibit only negligible divergence from the original pre-compressed dimensions. However, these limited and almost negligible differences (within the uncertainty in the measured length) were accounted for in the final error calculation.



**Figure 4.7:** The results of EMP-WDS analysis on (a) the starting sample of Fe-4.5Si, and at 3 GPa at (b) the melting point, (c) 1950 K, and (d) 2100 K.



**Figure 4.8:** The preserved geometry of the Fe-4.5Si samples used in this study.

## 4.5. Discussion

### 4.5.1. The Effect of Si on Electrical Resistivity of Fe-4.5Si

The anomalous behaviour of  $\rho$  of solid Fe-4.5Si has been observed for different Si contents in early studies (Yensen, 1915; Baum et al., 1967; Numakura et al., 1972; Nishino et al., 1993) and has been considered in terms of electron scattering of ordered-disordered phases. I confirmed earlier observations of initial peak and followed by decreasing electrical resistivity in the lower temperature range just above Curie temperature. However, above  $T_C$ , a strong temperature dependence and variability of  $\rho$  of solid Fe-4.5Si is observed, which leads to the question the validity of Matthiessen's rule at high temperatures. This conclusion is further corroborated when considering a dramatic change in  $\rho$  at the inferred phase changes (Figures 4.2 and 4.3). The limited validity of Matthiessen's rule was also recognized in recent studies (Gomi et al., 2013, 2016; Gomi and Hirose, 2015; Ohta et al., 2016; Zhang et al., 2018b). This is not unexpected, as there is an appreciable deviation from Matthiessen's rule of the electrical resistivity of Fe-Si solid solutions even at low temperatures above 30 K (Schwerer et al., 1969). Additionally, it was recognized in recent studies that Si impurity in Fe alloy at very high temperatures has only a very limited effect on  $\rho$  (e.g., Gomi et al., 2016; Ohta et al., 2016; Zhang et al., 2018b and references therein). For example, Gomi et al. (2013) reported that increasing the experimentally measured resistivity at ambient temperature by factor of 2 reduces the predicted CMB thermal conductivity value by only 5%. Furthermore, the observed variability of  $\rho$  of solid Fe-4.5Si as a function of temperature and phase transitions, places a significant uncertainty in electrical resistivity of Fe-alloys at high temperatures that may be sought using the linear Bloch–Grüneisen formula.

In terms of the onset of the first solid-solid phase change which takes place at temperature corresponding to the melting line of Si, and consequently decreases with increasing pressure (Figures 4.2 and 4.3), it is useful to take a look at some fundamental properties of liquid Si. Moreover, these properties of Si are also important in understanding the behavior of  $\rho$  of liquid Fe-4.5Si.

Pure liquid Si has entirely different properties from the solid crystal, such as coordination number that changes from 4 in solid (with the diamond structure) to  $\sim 6$  in the liquid state (Waseda and Suzuki, 1975; Gaspard et al., 1984). At the onset of melting, Si becomes denser as indicated by the negative  $dT_{\text{melt}}/dP$  slope (Hu and Spain, 1984; Kimura and Terashima, 1997) and assumes a metallic character, with resistivity 13 orders of magnitude less than at its peak in the solid. From the 1 atm melting point at about 1689 K (Glazov and Shchelikov, 2000),  $\rho$  ( $\sim 72 \mu\Omega\text{cm}$ ) has a negative temperature coefficient of resistivity, where  $\rho$  slightly decreases up to about 1823 K, after which it changes slope and begins to increase slowly. This decrease in  $\rho$  in the initial Si melt also coincides with a reduction in viscosity (Sasaki et al., 1995). This behavior is considered to be an effect of changing structure in the liquid. In principle, molten Si has properties analogous to those of molten metals. Thermal expansion of molten Si near its 1 atm melting  $T$  is on order of most molten metals ( $\sim 1 \cdot 10^{-4} \text{ K}^{-1}$ ) (Sato et al., 2000), while in the solid state Si shows small thermal expansion coefficient, in comparison with metals.

In the pressure region 11.2-12.5 GPa, Si is meta-stable where both simple cubic and body centered tetragonal (bct)  $\beta$ -Sn II structures coexist. At 12.5 GPa, Si enters a phase region with only a bct  $\beta$ -Sn II structure, which is also coincidentally metallic with similar electrical resistivity as the liquid and having strong  $d$ -orbital character (Biswas and Kertesz, 1984; Hu and Spain, 1984). The coordination number of solid bct  $\beta$ -Sn II structure is similar to the liquid and the addition of 2 more neighbors compared to the simple cubic structure is responsible for different energy level ordering that exists in that structure. Higher pressure brings the onset of metastable phases followed by stable phases after 16 GPa (e.g., Funamori and Tsuji, 2002). Interestingly, the pressure of 12.5 GPa is relatively close to the pressure at which Fe transforms from the bcc to hcp structure at room temperature.

In the same context, it is important to emphasize that S and C (as potential light element candidates in the Earth's core) have negative temperature coefficients of resistivity at melting at 1 atm, and C becomes completely metallic with  $\rho$  around  $30 \mu\Omega\text{cm}$  (e.g., Vezzoli, 1972; Heremans et al., 1988). The implication of this will become clear in the next section.

Counterintuitively, the melting temperature of Si decreases with pressure up to the transition to  $\beta$ -Sn II, after which it starts to increase (Bundy, 1964). Moreover, after the onset of melting, liquid Si is characterized by the presence of local structures in the melt (e.g., Waseda et al., 1995). Finally it should be emphasized that liquid Si also undergoes pressure induced structural changes (Funamori and Tsuji, 2002; Kubo et al., 2008). The noteworthy property of liquid Si is that Wiedemann-Franz law holds reasonably well (Magomedov and Gadjiev, 2008).

We can now try to understand the nature of the observed phase transition in Fe-4.5Si from disordered to ordered phase (Figure 4.2) and examine the effect of Si on the structural changes in solid Fe-4.5Si and corresponding effect on electrical resistivity. The fact that the Si melting curve coincides with the first phase change after  $T_C$  does not imply the presence of partial melt in the Fe-4.5Si alloy. However, at that transition temperature, Si attains metallic character and also increases its coordination number, which results in further modification and hybridization of the bonding arrangements with Fe (e.g., Gu et al., 2004). As a result, a transition to a more ordered phase takes place (fcc from 6-9 GPa and mixed phase from 3-5 GPa). Consequently,  $\rho$  dramatically decreases and Fe-4.5Si almost assumes the same character as fcc-Fe as shown by its approach to and eventual overlap with the resistivity of fcc Fe, which can be seen in Figures 4.1 and 4.2. Nevertheless, this explanation is not complete and requires full theoretical treatment which is beyond the scope of this study.

In terms of the phase transition observed just before melting at pressures 6-9 GPa, it is interpreted as a mixed phase. In-situ X-ray diffraction data are needed to resolve fully this structure.

Moreover, the unusual behaviour of Si, both at melting and in the liquid state, is likely responsible for the peculiar absence of larger discontinuity in  $\rho$  of Fe-4.5Si upon melting. It can be reasoned that the thermal expansion of Fe-4.5Si is significantly suppressed on melting (likely due to the fact that presence of Si in Fe-alloys reduces nearest neighbor distances in liquid), thus reducing the typical  $\rho$  signature associated with the first order phase transition. Interestingly, at 3 GPa,  $\rho$  of Fe-4.5Si at melting exhibits a slight dip. For



4 and 5 GPa, there is only a slight discontinuity in otherwise continuous trend in  $\rho$ . The surprising aspect of this behaviour is that it has been generally attributed to Fe-Si alloys with a significantly higher Si content (Baum et al., 1967). While this observation was verified through multiple experiments, more theoretical and experimental work is required to fully understand the melting dynamics of a Fe-alloy with low Si content.

Finally, discussion is needed on the phase transition associated with Fe and its alloys at  $\sim 5.2$  GPa (e.g. well known in Fe-Si and Fe-C alloys) which is also detectable in the liquid state (e.g., Sanloup et al., 2011; Shimoyama et al., 2013). The analogous structural change in Fe-4.5 Si at  $\sim 5.2$  GPa is easily observed in the behavior of the melting line. This is likely a result of the structural transition in solid. This transition, well recognized in solid and liquid pure Fe on the basis of behavior of the temperature coefficient of resistivity (Secco and Schloessin, 1989) and Fe alloys, affects physical properties such as density, viscosity, compressibility and sound velocity (Sanloup et al., 2000b, 2002, 2004, 2011; Terasaki et al., 2010; Shimoyama et al., 2013; Shibazaki et al., 2015; Lai et al., 2017). On the other hand, it should be noted that the evidence for such a transition is not observed in  $\rho$  along the melting boundary, which remains constant. It was noted earlier that addition of even a small amount of Si stabilizes the bcc structure and reduces the nearest and second neighbor distances in liquid (e.g., Shibazaki and Kono, 2018). However, this fact alone is insufficient to address this observed behavior of the liquid.

This suggests that liquid Fe-4.5Si just above the melting boundary does not change structurally around 5.2 GPa in a way to affect the electrical resistivity of the melt. Indeed, this is expected considering that the additional phase change (in the liquid) at the already existing triple point is thermodynamically forbidden. That is, of course, if one assumes that Fe-4.5Si behaves similarly to pure Fe or even Fe-C alloy which indeed exhibit structural changes around 5.2 GPa. Conversely, invariant  $\rho$  of liquid Fe-4.5Si implies the existence of short and perhaps medium range order liquid structures along the melting boundary, which impose a control mechanism on the behaviour of  $\rho$ . This conclusion agrees well with the earlier studies which used X-ray diffraction and numerical simulations to demonstrate the existence of a local structure in liquid Fe-Si, generally detected by the appearance of the shoulder in the first peak in the experimentally

measured total structure factor  $S(Q)$  (e.g., Roik et al., 2014 and references therein). Thus, in order to understand the electrical resistivity of liquid Fe-4.5Si along the melting boundary, and potential implications of such behavior on the dynamics of the Earth's OC, it is important to understand the nature of those local structures in the liquid. Understanding the dynamics of the local structures with short and medium order in liquid alloy is an important step toward resolving their impact on electrical resistivity and by extension, thermal conductivity of the Fe-alloys at core conditions.

Alternatively, one might seek an explanation for invariant  $\rho$  along the melting boundary of Fe-4.5Si in terms of electrical resistivity saturation (thermal, chemical or pressure induced) (e.g., Gomi et al., 2013, 2016; Gomi and Hirose, 2015). The saturation effect does not hold for the results in this study, as there is a steady increase of the electrical resistivity in the liquid alloy with increasing temperature and at all experimental pressures. Thus, it is important to examine the role of local structures in liquid. Before that, we need to reflect on some fundamental properties of liquid transition metals. The familiarity with those properties will be helpful later in understanding the prevalence and dynamics of short and medium range order in molten transition metals.

#### **4.5.2. Electronic Structure of Liquid Transition Metals and Alloys**

Despite a long history of scientific inquiry, the structure and dynamics of liquid metals were relatively poorly understood until the turn of the 21<sup>st</sup> century, when the availability of computational power and improved theoretical methods significantly improved our understanding of these systems (e.g., Li et al., 2017). The classical view of liquid metals suggests that the electrons may be characterized as if they are free particles and their quantum states are not dominated by coherent diffraction from a typical highly ordered lattice structure that exists in solid metals (Ziman, 1970; Mott, 1972). In simple terms, liquid metals possess no long range order, which strongly affects the behavior of  $\rho$ . The scattering of charge carriers in liquid transition metals is still somewhat of a mystery, and no current theoretical and numerical tools can account for the invariant electrical resistivity of liquid Fe, Ni, and Co along the melting boundary (e.g., Silber et al., 2017, 2018; Ezenwa and Secco, 2017). It is generally accepted that the mean free path of an

electron in a liquid metal depends on scattering by the “ions” (Ziman, 1961). Another scattering mechanism involves density fluctuations of the liquid (Ziman, 1961; Faber and Ziman, 1965). Furthermore, Mott (1972) suggested different mean free paths for the faster and lower effective mass and the slower and higher effective mass  $d$  conduction electrons in liquid transition metals where  $s$  electrons are considered to undergo  $s$ - $d$  transitions.

Early experimental and theoretical investigations demonstrated that the electron density of states (DOS) of liquid transition metals Fe, Ni and Co, while losing the presence of sharp peaks, exhibits a remarkable similarity to the electronic structures of the crystalline metals (Jank et al., 1991). The electronic DOS of liquid transition metals clearly shows characteristic bonding- antibonding splitting in the  $d$ -band. This bonding-antibonding splitting is larger for the metals with a partially filled  $d$ -band, such as Fe, and the same behavior is evident in both solid and liquid (Jank et al., 1991). In 3d liquid transition metals, the  $d$ -electrons are also responsible for such low compressibility and internal pressure anomalies (e.g., Steinemann and Keita, 1988), as well as strong cohesion and high melting points in 3d transition metals (Janak and Williams, 1976).

There are strong parallels between pure liquid Fe and liquid Fe-alloys, especially those with low solute concentrations. For example, Gu et al. (2004) calculated electronic structures of molten Fe-Si alloys and showed that the interaction of Fe-Si atoms originated from the hybridization of the Fe  $3d$  and Si  $3p$  bands. The calculated bond strength in Fe-Si alloys demonstrates that the Fe-Si bond is stronger than the bond between Fe atoms (Gu et al., 2004). Calculations by the same authors also confirm that the Si atoms form bonding and anti-bonding states with neighboring Fe atoms. This is one of the key points to understand the formation and dynamics of the local structures in the liquid Fe-Si alloy with short or medium range order, which will be discussed in the next section.

Additionally, liquid metals have spherical Fermi surfaces because the medium is isotropic (Mott, 1972). Pressure application causes a reduced interatomic distance which is inversely proportional to the parameters in inverse space such as Fermi wave vector ( $k_F$ ).

Consequently, compression results an increase in area of the spherical Fermi surface (Venttsel et al., 1974; Vinokurova et al., 1979; Gapotchenko et al., 1988). This is one of the mechanisms responsible for a decrease in  $\rho$  in solid metal with increasing pressure. A characteristic feature of 3d liquid transition metals is the hybridized *s-d* valence electron states. While it is well understood that the electrical resistivity of molten 3d transition metals is strongly modulated by charge carrier scattering and *s-d* hybridization (Mott, 1972; Ballentine et al., 1984), there is currently no established theoretical framework that could account for the behavior of  $\rho$  of liquid Fe-4.5Si (or even pure Co, Ni and Fe) along the melting boundary.

Next, I discuss short and medium range ordering in liquid transition metals and alloys that is responsible for the invariant electrical resistivity of liquid Fe-Si as well Fe, Ni and Co along the melting boundary. To the best of my knowledge, this approach has not been considered previously in the context of electrical resistivity of liquid transition metals and alloys at high pressure.

#### **4.5.3. Short and Medium Range Ordering In Liquid Transition Metals and Alloys**

The presence of an icosahedral short-range order (ISRO) (with the fivefold symmetry) in melts was first postulated by Frank (1952) to explain the observed large undercooling of pure metals. Typically, ISRO clusters consist of 12 atoms with fivefold symmetry on the outside, surrounding the additional atom in the center of the structure. These structures have the same coordination number as the fcc or hcp close packed structures in transition metals, and interact via Lennard-Jones potential. Considering that natural systems adopt a structure with the lowest energy state, it is not surprising that these structures have energy that is 8.4% lower than that of the close-packed arrangements in solid (fcc or hcp) and thus lower the overall energy of the liquid. This was indeed predicted by Frank (1952).

However, these structures were not observed experimentally and numerically in liquid transition metals (e.g., Fe, Ni, Zr) until much later (e.g., Schenk et al., 2002; Lee et al., 2004). Typically, ISROs are identified from analysis of liquid structure factor. The presence of a shoulder on the right-hand (high wavenumber) side of the second

oscillation is indicative of the presence of a fivefold structure (Schenk et al., 2002). These short range clusters may also take different combinatorial geometries, based on the composition of the material from which melt originates (Schenk et al., 2002; Lee et al., 2004). Schenk et al. (2002) noticed that more complex and more densely packed geometry (e.g., a dodecahedron which consists of 33 atoms and can be constructed from aggregates of icosahedral clusters) appears at increasing pressure.

An icosahedral topological short-range order is an ubiquitous component in all liquid 3d transition metals (e.g., Schenk et al., 2002; Zigo et al., 2018). The main reason for such a behavior is that the presence of short and medium range order and distinct atomic clusters with fivefold symmetry in transition metals is considered to be a result of strong directional bonding from incomplete *d* bands and these form local structures in the liquid (e.g., Burdett, 1995). The phenomenon may be interpreted in terms of a Peierls-Jahn-Teller distortion in which a system is stabilized by removing the degeneracy of levels, forming localized bonds, and lowering the energy (Jahn and Teller, 1937; Ross et al., 2007). Thus, it is evident that the formation of those structures in the melt favours 3d transition metals and alloys with similar electronic structures (Schenk et al., 2002; Lee et al., 2004). The underlying mechanism is the hybridization of the *p*-like valence and *d*-like conduction states associated with the formation of ISRO clusters (Boehler and Ross, 2007). This is consistent with other studies which showed that a close relation between atomic and electron structure of liquid metals and alloys exists (e.g., Il'inskii et al., 2002) and that it depends on the electron structure of the substance. The specific properties of the atomic structure of the Fe–Si alloys in the liquid state (formation of the clusters, their composition, atomic packing and range of the existence) is considered to be a function of their electron structure (Il'inskii et al., 2002).

For an alloy which consists of the majority of atoms with a larger atomic radius (e.g., Fe) and smaller concentration of alloyed atoms with the smaller radius (e.g., Si), an ISRO topological SRO different from ISRO may be present for geometric reasons (Holland-Moritz et al., 2006). However, the presence of ISROs is preferred in liquid transition metals or alloys, regardless of whether or not the radii of atoms are similar or appreciably different. As indicated by Holland-Moritz et al. (2006), a small concentration of smaller

atoms in a system of larger atoms is likely to stabilize icosahedral clusters. This is because for a typical icosahedron, the interatomic distance between the atoms on the surface is approximately 5% larger than the distance between the surface atoms and the central atom. Consequently, an icosahedron structure with a smaller atom in the center is energetically favorable. This very strongly suggests that presence of not only Si, but also that of C, O, and S may be favored in ISRO structures in the liquid Fe alloy, especially at high pressure. Therefore it is reasonable to predict that liquid Fe, alloyed with small contents of C, S or O, and perhaps any combination thereof, will exhibit the same behavior as Fe-4.5 Si. Correspondingly, ISRO structures were observed in binary and ternary alloys such as Fe<sub>78</sub>Si<sub>9</sub>B<sub>13</sub> (e.g., Qin et al., 2004; Li et al., 2017).

The presence of local structures in liquid Fe-Si alloys with short and medium range order has been observed with different interpretation (e.g., Il'inskii et al., 2002; Gu et al., 2004; Qin et al., 2004; Mizuno et al., 2013). Coincidentally, the existence of local structures in the melt is well established in liquid Si (e.g., Roik et al., 2014 and references therein). Roik et al. (2014) examined the atomic structure of the Fe-Si melts by X-ray diffraction and Reverse Monte Carlo simulations. They reported the presence of both short-range order (i.e., ISROs) as well as medium range order (MRO) in the liquid Fe-Si alloys. The high Si content in the liquid alloy promotes the presence of MRO structures. That was also shown by Mizuno et al. (2013) who reported that MRO increases with increasing Si content. MRO structures in liquid Fe-Si alloys, attributed to the presence of a Fe-centered clusters, are typically inferred from the presence of the pre-peak in structure factor (asymmetry or at best a shoulder rather than clear splitting in the first peak) (Roik et al., 2014; Mizuno et al., 2013). Indeed, the authors demonstrated the existence of poly-tetrahedral aggregates with a pentagonal symmetry (i.e., icosahedron), analogous to ISROs in liquid 3d transition metals (Roik et al., 2014). It is also important to note that liquid Fe-Si alloys retains an overall Fe-like structure if the Si content is below ~38wt% (Roik et al., 2014).

The liquid Fe-Si alloy is characterized by strong interaction between Fe and Si atoms (Gu et al., 2004). That interaction between Fe and Si is indeed stronger than the interactions between Fe-Fe or Si-Si (Roik et al., 2014). Correspondingly, the calculated electronic

structures of molten Fe-Si alloys indicate that the interaction of Fe-Si atoms originates from the hybridization of Fe  $3d$  and Si  $3p$  bands (e.g., Roik et al., 2009, 2014). The Si atoms form bonding and anti-bonding states with the neighboring Fe atoms, and the Fe-Si bond is stronger than the bond between Fe atoms. The increase in Si content and structural modification of Fe-Si alloy affects the distribution of Fe  $3d$ , Si  $3s$  and  $3p$  orbitals. Roik et al. (2014) also demonstrated that the local atomic order in Fe-Si melts exhibits similarity to that in the parent crystalline phase which is characterized by a strong preference for hetero-atomic nearest-neighbor bonds. This agrees with the argument presented in Silber et al. (2018) which suggests that the structure of solid parent phase has a strong influence on the behavior (and structure) of metallic liquid at high pressures in the vicinity of the melting point. Indeed, earlier research (e.g., Hafner and Kahl, 1984 and references therein) show that the structures of the elements in the liquid state follow characteristic trends which closely resemble the trends of the crystal structures of elements.

The presence of ISRO persists to temperatures significantly above the melting boundary. This was demonstrated recently when ISRO were observed in liquid Ni, 100 K above the melting temperature (Lee et al., 2004). The five-fold symmetry is incompatible with the long-range periodicity, so the poly-tetrahedral short-range order favors the disordered structures such as in the liquid transition metals (Li et al., 2017)

There are two important aspects of ISRO which are related to this study. First, the presence of ISRO increases the viscosity of the melt, because those structures act toward dynamical slowing down of atomic motion within the liquid required for momentum transfer (Lü et al., 2017; Hu et al., 2015). This was again demonstrated recently by Hu et al. (2017) who examined the effects of pressure on the ISROs. They showed that isothermal compression of the melt with ISROs slows down the dynamics of metallic liquid which implies an increase in viscosity. This has been seen in both DAC and shock experiments at pressures corresponding to the OC conditions (e.g., Boehler and Ross, 2015). Depending on the  $P$  and  $T$ , the connected clusters of ISROs of varying sizes and number density may evolve throughout the liquid (Jónsson and Andersen, 1988). In terms of viscosity of the OC, this interpretation agrees well with earlier studies which suggested

high viscosity of the OC alloy (Anderson, 1980; Stevenson et al., 1983; Palmer and Smylie, 2005; Smylie, 1999).

Second, the application of pressure increases the ISRO concentration as well as viscosity (Boehler and Ross, 2007, 2015). ISRO formation is favoured by application of pressure in the liquid because compression squeezes out “free volume,” which leads to denser packing of ISRO local structures (Hu et al., 2017). The concentration of ISRO structures increases with pressure as a result of the pressure- induced modification of *s-d* bands and *s-d* electron transfer (Boehler and Ross, 2015). Notably, ISRO structures with the five-fold symmetry are significantly denser than the surrounding liquid consequently introducing local density anomalies throughout the melt. As noted earlier, this affects the electrical resistivity of the liquid because it decreases the mean free path of electrons and consequently increases their scattering rate. This is discussed in the next section.

The presence of ISROs is also considered to be responsible for the lowering the transition metal melting slopes as demonstrated by Ross et al. (2007). Not surprisingly, the underlying mechanism is the hybridization of the *p*-like valence and *d*-like conduction states associated with the formation of ISRO clusters (Boehler and Ross, 2007).

#### **4.5.4. Implications of ISROs for Electrical Resistivity**

I now examine the effect of ISROs on the invariant  $\rho$  of Ni, Fe along the melting boundary observed by Silber et al. (2017, 2018), and Fe-4.5 Si in this study. The implications for other Fe-alloys are also discussed. It should be noted that this is the first time that the effect of ISRO structures has been examined in the context of electrical resistivity of liquid transition metals and alloys at high pressure. Of course, it is essential to emphasize again that currently there is no theoretical framework that would account for the impact of ISRO structures on the  $\rho$  of a molten metal or alloy, especially at increasing pressure. Thus, I offer a qualitative explanation as more theoretical and experimental work is needed to quantitatively and fully resolve the contribution of ISROs scattering mechanisms and exact dynamics of their interaction with the charge carriers in liquid transition metals.



The effect of these structures in liquid transition metals and alloys on the observed behavior of  $\rho$  along the melting curve can be best described in conceptual terms as follows. ISROs act as the scattering centers throughout the melt. Thus, the presence of ISRO in the liquid reduces the mean free path and increases electron scattering. This implies that a higher concentration of ISROs promotes increase in  $\rho$  of the liquid transition metal. Consequently, the application of pressure increases the concentration of ISROs, which in turn would be expected to increase  $\rho$ .

This qualitative interpretation would lead to continuous increase in electrical resistivity with pressure (as pressure promotes the growth of ISRO) and that is not observed. That is primarily because the increase in pressure reduces the amplitude of ionic motion, modifies bonding arrangements, increases the overall state of order and by extension reduces the electron scattering. Moreover, the application of pressure increases the area of the spherical Fermi surface in liquid metals which means that charge carriers experience reduced scattering due to smaller density of states above Fermi level. This in turn promotes the antagonistic reduction of electrical resistivity with respect to ISROs effect. Our experimental results show that these competing effects appear to offset each other on the  $P$ - and  $T$ -dependent melting boundary. This mechanism is illustrated using the simple equation for electrical conductivity (inverse electrical resistivity) from Mott (1972, 1980):

$$\sigma = S_F e^2 L / 12 \pi^3 \hbar \quad (4.1)$$

Here,  $S_F$  is the area of the Fermi surface,  $e$  is electron charge,  $L$  is electron mean free path, and  $\hbar$  is the Planck constant divided by  $2\pi$ . It is evident that electrical conductivity depends on the size of the Fermi surface (a sphere in the case of liquid metals) and the mean free path. Thus, if the electrical resistivity is to remain constant along the melting boundary, it is required that the product of the length of electron mean free path and the area of the Fermi spherical surface remains constant.

As discussed above, considering the effect of pressure, this can be done if the pressure dependent ISRO structures reduce electron mean free path and increase scattering. This is in addition to the effects of temperature (increases the kinetic energy of the system and

causing thermal expansion) along melting boundary which increase  $\rho$ . Equation (4.1) implies that the pressure induced increase of the area of Fermi sphere surface has to match proportionally the decrease in electron mean free path. Of course, an increase in the Fermi surface area is accompanied by a transition of the system to a dynamically “more orderly” state which counters the effects of ISROs and reduces the  $\rho$ . The net result of these antagonistic effects modulating  $\rho$  is the invariant electrical resistivity along the melting boundary as observed in our experiments.

Although only a crude approach to a far more complex phenomenon, Equation (4.1) shows the opposite effects of pressure on electron mean free path and Fermi surface area. A comprehensive theoretical interpretation of the interplay between ISRO and temperature induced higher rate of electron scattering, as well as the suppressed amplitude of ionic motion, and decreased scattering of electrons above increased Fermi level, and quantitative assessment of their relative contributions, is beyond the scope of this work.

However, the constant resistivity of Ni, Fe and Co observed along their melting boundaries (Silber et al., 2017, 2018; Ezenwa and Secco, 2017) is clearly consistent with this postulate. Further support for this reasoning comes from consideration of the behavior of electrical resistivity of liquid Cu, Ag and Au on their melting boundaries. These noble metals all have a filled  $3d$ -band and consequently, in contrast to liquid Fe, Co and Ni, the local ISRO structures are almost absent in these liquids (Ganesh and Widom, 2006, 2008). This indeed explains the decrease of  $\rho$  along the melting boundaries of these three metals, as observed experimentally by Ezenwa et al. (2017), Littleton et al. (2018) and Berrada et al. (2018), respectively. In the context of Eq (4.1), the increasing size of the Fermi surface, tending to decrease resistivity, is not offset by a corresponding decrease in electron mean free path because of the lack of ISRO scattering centers.

The reasonable question now is: can the invariant electrical resistivity of Fe and Fe-alloys along the melting boundary remain unchanged beyond the  $\gamma$ - $\epsilon$ -liquid triple point at about 100 GPa?

Several factors strongly support this supposition. The first is the energy consideration. The energy of fcc ( $\gamma$ ) and hcp ( $\epsilon$ ) structures is almost identical. This implies that the liquid originating from both fcc and hcp parent phase will experience almost the same decrease in energy associated with the formation of ISRO structures in the liquid state and hence have the same structural and dynamical properties. This suggests an uninterrupted and steady growth in ISRO concentration in the liquid with increasing pressure across the  $\gamma$ - $\epsilon$ -l triple point. Such trend will persist uninterrupted beyond the  $\gamma$ - $\epsilon$ -liquid triple point as a result of energy consideration between solid parent phase and the liquid along the melt boundary. Higher concentration of ISROs suppresses the decrease in electrical resistivity (ordinarily attributed to pressure application) by increased charge carrier scattering. Consequently, this favours invariant electrical resistivity across triple point and along the melting boundary of Fe and Fe-alloys. However, it should be emphasized for the purpose of clarity, that the  $\gamma$ - $\epsilon$ -liquid triple point Fe alloyed with light elements may not have the same  $P$ - $T$  coordinates as for pure Fe.

I also note that the coordination number for fcc and hcp structures is identical at 12. This fact also indicates that the ISRO structures in the liquid originating from either phase will be structurally the same (as 12 coordinated ISROs in the liquid seek the densest packing resembling the packing in the solid parent phase). Next, the electronic density of states is considered. For fcc and hcp solid phase (e.g., Lizárraga et al., 2017), density of states is almost identical, which implies that such strong similarity is carried into the liquid. Moreover, such resemblance ensures the very close scattering properties in liquids originating from both structures. This consequently implies identical electrical resistivity in the liquid originating from both solid parent phases.

#### **4.5.5. Thermal Conductivity of the Outer Core**

I take the ICB as an anchoring point where Fe/Fe-alloy freezes out onto the IC and propose that  $\rho$  of liquid Fe-alloyed with light elements remains unchanged from the value ( $\sim 120 \mu\Omega\text{cm}$ ) obtained in this study and earlier studies (Silber et al., 2018). At the CMB, the situation is certainly more complicated considering the uncertainty in temperature related to the deviation of the temperature gradient from the adiabat (e.g., Davies, 2015).

That uncertainty in temperature may be mitigated by considering resistivity saturation (Gomi et al., 2013, 2016; Gomi and Hirose, 2015). Taking into account the uncertainty in temperature at the CMB, I agree with these authors that the electrical resistivity of liquid Fe-alloy (whatever the combination may be) may not exceed  $\sim 150 \mu\Omega\text{cm}$ .

Assuming that the Wiedemann–Franz law ( $\kappa = LT/\rho$ ) holds at the CMB and ICB conditions, which is predicated on minimal role of the inelastic electron scattering is negligible at the core conditions (e.g., Williams, 2018), I can then evaluate  $\kappa$  at the ICB and at CMB using the Sommerfeld value ( $2.445 \times 10^{-8} \text{ W}^2/\text{K}^2$ ) of the Lorenz number. On the outer core side of the ICB,  $\kappa$  is estimated to be  $112 - 122 \text{ Wm}^{-1}\text{K}^{-1}$  relying on the current uncertainties in ICB temperatures (5500-6000 K) (e.g., Anzellini et al., 2013). On the core side of the CMB,  $\kappa$  is estimated to be between 65 and  $73 \text{ Wm}^{-1}\text{K}^{-1}$  assuming the temperature at the CMB is in the range 4000-4500 K (e.g., Badro et al., 2014; Zhang et al., 2016b) and  $\rho$  of  $\sim 150 \mu\Omega\text{cm}$ . These estimates are in a reasonable agreement with the lower end of the recent theoretical and experimentally obtained values (e.g., Pozzo et al., 2012, 2013; de Koker et al., 2012; Seagle et al., 2013; Gomi et al., 2013, 2016; Gomi and Hirose, 2015).

Comparatively, the  $\kappa$  values derived here are also in a reasonable agreement with estimates of thermal conductivity at the CMB based on models of heat flow through the CMB (e.g., Olson, 2016; Davies, 2015; Davies et al., 2015; Gubbins et al., 2015).

It should be emphasized again that the calculated values of thermal conductivity are based on the assumption that the value of the Lorenz number is valid up to core pressures and temperatures. However, that may not be the case, as discussed by Williams (2018) and Pourovskii et al. (2017). At the core conditions, Pourovskii et al. (2017) calculated that the Lorenz number would be appreciably lower (up to  $\sim 0.65L_0$ ), thus lowering the value of thermal conductivity calculated from the resistivity values.

As indicated earlier, ISROs, similar to impurities, will act as independent scattering centres for the conduction electrons. Nevertheless, the question is: can the presence of ISROs affect the value of the Lorenz number at core pressure and temperature in Fe-alloys? The answer is likely yes! The scattering by ISROs and their clusters (a system of

connected ISROs) may behave analogously to the scattering by impurities in metals as they are likely to disrupt the phase of electron wave, and also disrupt the electrons coherent propagation (Giuliani and Vignale, 2005).

That analogy however has serious implications, as it is known that impurities in some cases cause inelastic electron scattering that preserves charge but not the energy (Taylor, 1962; Koshino, 1963; Giuliani and Vignale, 2005). In a liquid Fe-alloy containing ISRO structures at the core conditions, inelastic scattering from ISROs could result from the presence of local magnetic moments and spin scattering within those structures, which is in line with the discussion by Drchal et al. (2017). The ISRO structures in the melt, due to their densely packed order relative to the rest of the liquid, will affect the magnitude and the consideration of potential experienced by the electrons (e.g., Faber, 1972). In principle, the ISRO-induced localized potential experienced by a conduction electron is significantly greater than the averaged potential by thermally oscillating ions in liquid. Moreover, the concentration and distribution of ISROs and the size of ISRO clusters will affect the screening consideration similar to impurities in solid metals (e.g., Abrikosov, 2017).

If inelastic electron-electron scattering is appreciable as a result of presence of ISROs in Fe alloys at the core conditions, it can then decouple heat transport from charge transport (Williams 2018). Thus, ISRO-caused inelastic electron scattering would render the currently used Wiedemann-Franz scaling law between electrical and thermal conductivity very inaccurate (e.g., Williams, 2018). Indeed, that effect will be likely amplified by not only isolated ISRO structures, but also by connected clusters at a high pressure.

While inelastic scattering does not affect the overall electrical resistivity (e.g., Taylor, 1962), it affects the value of thermal conductivity (Williams, 2018). This indeed is likely to explain a recent directly observed low value of thermal conductivity of Fe at near the core conditions (e.g., Konôpková et al., 2016) as their measurements were taken in the  $P$ - $T$  space that corresponds to the deeply undercooled state of Fe with the maximum concentration of ISROs and potentially highest rate of inelastic electron scattering. Admittedly, more experimental and theoretical work is needed to resolve this uncertainty.

#### 4.5.6. General Implications for Core Evolution and Heat Flow

The adiabatic conductive heat flow ( $q_{\text{cond}}$ ) at the outer core-CMB interface was calculated using the classical expression (e.g., Davies et al., 2015):

$$q_{\text{cond}} = -4\pi r^2 k_e \left[ \frac{\partial T}{\partial r} \right]_{r=r_0} = -4\pi r^2 k_e \frac{g\gamma T}{\phi} \quad (4.2)$$

Here,  $\kappa$  is thermal conductivity obtained in this study and  $r$  is radius of the Earth's outer core ( $r_{\text{oc}} = 3480$  km). The value for the Grüneisen parameter is taken to be  $\gamma = 1.5$  (Davies et al., 2015) while the considered temperature range was specified above. Gravity acceleration  $g$  and seismic parameter  $\phi$  were taken from the preliminary reference Earth model or PREM (Dziewonski and Anderson, 1981). A calculated adiabatic heat flow of 9.4 – 12 TW at the outer core-CMB interface is not that different than estimates derived from mantle circulation models (Olson et al., 2015; Olson, 2016) and suggest that thermal convection may still be possible in the core. The range of values for the adiabatic heat flow at the outer core-CMB interface stems from the uncertainty in temperature and the value of thermal conductivity ( $\kappa_{\text{cmb}} = 65 - 73 \text{ Wm}^{-1}\text{K}^{-1}$ ).

Although this calculated heat flow is lower in comparison with the highest estimates in literature, high values of thermal conductivity demand perhaps an unrealistic power budget for the geodynamo, and also complicate the interpretation of the spatio-temporal evolution of the core.

The adiabatic heat flow reported in this work is high enough to require buoyancy driven core convection from the exsolution of light elements during the IC growth. However, if the energy budget of the core is higher as per some recent estimates (e.g., Gubbins et al., 2015; Davies et al., 2015) then the role of thermal convection cannot be dismissed. Therefore the actual convection in the core may have contribution from both buoyancy and thermally induced flows. Mantle circulation plays an important role in maintaining the convective mechanism in the OC, as it extracts the heat and contributes to the full convection of the core. Indeed, seismic data indicate that the core is well mixed (Davies et al., 2015; Nimmo, 2015a; Labrosse, 2015). However, compositional convection is still

not fully resolved, not only because of the unknown age of the IC, but also because there is significant uncertainty in terms of light element composition in the core (Ozawa et al., 2016; Morard et al., 2017; Mori et al., 2017; Suer et al., 2017; Suehiro et al., 2017; Tateno et al., 2018; Shibazaki and Kono, 2018). For example, it was recently proposed that the exsolution of Mg at the CMB is sufficient to drive compositional convection (O'Rourke and Stevenson, 2016; O'Rourke et al., 2017) from the top down. However, a recent study showed that such a mechanism has insufficient energy to drive the geodynamo because Mg partitioning depends strongly on the O content in the Fe-rich liquid alloy (Du et al., 2017) and its content in the outer core is very small.

Potential stratification at the top of the OC may develop if the heat flow at the core-CMB interface is near adiabatic or subadiabatic. This stratified region is unstable due to the CMB heterogeneities (such as the D'' region), with a higher rate of heat flow. These thermal heterogeneities in the lower mantle would promote lateral instability and thermally-induced movement of fluid, thus disintegrating the stratified layer (Gubbins et al., 2015; Olson et al., 2015). This is supported by a low secular variation of heat flow below the Pacific region, where the lowermost mantle is hot and stabilizing (Gubbins et al., 2015). Moreover, the highest heat flux is observed in the coldest sections of the CMB, such as the region below Indonesia. The subduction zones have been active beneath Indonesia for long enough to have cooled the mantle all the way down to the core (e.g., Gubbins et al., 2015; Olson et al., 2015). In principle, the energy transfer between processes driving the plate tectonics and the geodynamo is controlled by thermal conduction in the lowermost mantle, through the D'' region (Ammann et al., 2014).

Paleomagnetic evidence suggests the presence of the magnetic field as early as 4.2 Gyr (Tarduno et al., 2015). Nevertheless, the age of the IC nucleation may be much less certain than suggested in recent studies which incorporate the effect of the high thermal conductivity (e.g., Davies et al., 2015; Davies, 2015; Nimmo, 2015b; Olson, 2016). A new study shows that the nucleation of the IC is uncertain because of the energy barrier to the formation of the first stable crystals nucleus (Huguet et al., 2018). Using the constraints from the simulations, theory and experiments, the authors show that a spontaneous crystallization in a homogenous liquid Fe alloy at the Earth's core pressures

requires critical supercooling of the order of 1000 K which is too large to be a plausible mechanism for the origin of Earth's inner core (Huguet et al., 2018). Their results indicate that the nucleation of the IC could have been initiated much earlier than currently considered in models with high  $\kappa$ . This finding supports the postulate about the presence of ISROs in the OC alloy and their effect on electrical resistivity and viscosity. This is corroborated in recent computer simulations which showed that the fivefold symmetric ISRO polyhedron tends to increase the interfacial energy between liquid and crystal, leading to the suppression of nucleation in liquids (Taffs and Patrick Royall, 2016). An alternative explanation should perhaps be sought in the hypothesis suggested by Huguet et al. (2018) that involves the role of a giant impact in the IC nucleation.

In terms of dynamical properties of the liquid alloy in the OC, a high viscosity in the OC is expected, because of the increased presence of ISRO discussed in the previous section. This assertion is supported by the assumed high values of viscosity in numerical models (e.g., Gubbins et al., 2015). Indeed, the ISRO induced high viscosity would reconcile the high value of Ekman number, used in current numerical models to maintain the laminar flow. This is reinforced by recent experimental measurements of viscosity of Fe and Fe-alloys. The observed steady increase of viscosity with increasing pressure confirms that the corresponding increase in ISRO concentration, has a direct effect on a suppression of dynamical motion within the liquid and subsequently increases viscosity (Dobson et al., 2000; Rutter et al., 2002a; 2002b; Terasaki et al., 2002, 2006; Funakoshi, 2010; Shimoyama et al., 2013; Kono et al., 2015).

A variety of light elements, such as S, C, and O, are expected to be in the liquid OC in relatively small quantities (e.g., McDonough, 2003; Zhang et al., 2016a; Morard et al., 2017; Tateno et al., 2018). It was established recently that no single light element can be present in OC. Furthermore it has been demonstrated that no singular light element can satisfy the combined compositional, cosmochemical and geophysical constraints in the OC near ICB (Ozawa et al., 2016; Morard et al., 2017; Mori et al., 2017; Suer et al., 2017; Suehiro et al., 2017; Tateno et al., 2018; Shibazaki and Kono, 2018). Indeed, the exact compositional makeup of the light elements in the core is still unresolved. However, this work leads to the conclusion that the transport properties of liquid Fe-alloy



will remain the same at ICB and likely at CMB, regardless of the light element compositional content and proportion in the OC. All light elements, when alloyed with Fe at high pressure have a stabilizing effect on the solid and form closely packed parent structures before melting at high pressures (e.g., Shibazaki and Kono, 2018). Thus, it is reasonable to expect that other combinations of light elements alloyed with liquid Fe, exhibit the same transport properties in liquid as Fe-4.5Si investigated here. Most importantly, in this work, the significant compositionally derived uncertainty in determining the  $\kappa$  in the OC was resolved. Still, the uncertainties that may impact the value of  $\kappa$ , such as exact temperatures at the CMB and ICB (Davies et al., 2015) and the role of inelastic electron scattering, remain presently unresolved. Finally, the findings in this study may play an important role in evaluating transport properties in super-Earth type exoplanets (Wicks et al., 2018).

#### 4.6. Summary and Conclusions

The electrical resistivity of solid and liquid Fe-4.5Si was measured experimentally up to 9GPa in a large volume press. The results demonstrate that the electrical resistivity of the solid decreases with pressure and is highly sensitive to the degree of ordering induced by the temperature dependent phase transitions. The presence of Si is also observed to suppress the magnitude of resistivity jump on melting.

Remarkably, the electrical resistivity of liquid Fe-4.5Si along the melting boundary remains invariant and has the same value as the electrical resistivity of pure liquid Fe of 120  $\mu\Omega\text{cm}$ . These results are interpreted in the context of icosahedral short range (ISRO) structures in the melt whose concentration is proportional to increasing pressure. To the best of my knowledge, this is the first time that the effect of pressure dependent ISRO structures concentration has been used to explain the electrical resistivity of a liquid alloy under compression in the context of the core transport properties. It is postulated that the electrical resistivity of Fe-4.5Si remains constant along the melting boundary to the ICB, which is used as an anchoring point. Based on the recent developments in understanding

the dynamics and structure of liquid transition metals and alloys, we extend our results to pure liquid Fe and Fe-alloys with variable content of light elements in the Earth's outer core. I presented the evidence that pure liquid Fe and molten Fe-alloys (with C, S and O) have the same behavior at ICB as interpreted from this study and from experiments on pure Fe (Silber et al., 2018).

The calculated values of thermal conductivity and heat flow across CMB are consistent with recent theoretical and experimental results. However, the main point of the findings in this work is they eliminate the uncertainty of the identity of the light element(s) by removing a compositional dependence of electrical resistivity of liquid Fe-alloy in the core and place a more firm constraint on the transport properties of the outer core. Furthermore, the implication of the results was discussed with the respect to the outer core viscosity and renewed uncertainty in the inner core nucleation age.

The development of theoretical framework to account for our results is needed along with additional experimental studies to validate our findings and conclusions.

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## Chapter 5

### 5. Conclusions and Outlook

*You cannot teach a man anything;  
you can only help him to find it within himself.*

– Galileo

The primary aim of this thesis was to measure the electrical resistivity of Ni, Fe and Fe-4.5wt% along their melting boundary as a sensible way toward better constraining the transport properties of the Earth's outer core. It was shown that the electrical resistivity of Ni and Fe, as well as Fe-4.5Si, alloy remains invariant at the onset of melting throughout the experimental pressure range in this work. Remarkably, the electrical resistivity ( $\rho$ ) of Fe and Fe-4.5Si along the melting boundary has the same value of  $\sim 120 \mu\Omega\text{cm}$ , which invalidates Matthiessen's rule in the liquid. However, these results also contradict the prediction by Stacey and Loper (2007) who predicted such behaviour only in simple liquid metals along their melting curve.

Based on the structural similarities between solid fcc phase and the melt in both Fe and Ni, the prediction was made that the melt from fcc Fe phase will exhibit the constant electrical resistivity along the melting boundary up to  $\gamma$ - $\epsilon$ -liquid triple point. The same trend is predicted to persist for liquid Ni to much higher pressures due to absence of known triple points. This behaviour was first considered through the contribution of the strong electron-electron scattering to electrical resistivity of Ni and Fe, typical of correlated systems. Similar to heavy fermions, both Ni and Fe follow the Kadowaki-Woods ratio. However the electron-electron scattering along the melting boundary it is not sufficient to account for the invariant electrical resistivity at the onset of melt.

The recent developments in understanding the structure and dynamics of liquid 3d transition metals and alloys were instrumental in interpreting the invariant electrical



resistivity of Fe, Ni and Fe-4.5Si along the melting line in the context of local short range order in liquid with icosahedral symmetry. ISROs favour 3d liquid metals and alloys. In the melt, they are responsible for lowering the energy of the system by about 8.4% and share the coordination number with fcc and hcp structures. Moreover, the concentration of these structures increases with the application of pressure.

ISROs act as scattering centres for electrons and are responsible for the increase in electrical resistivity by decreasing the mean free path of electron in the liquid. The presence of these structures counters the effects of pressure which would typically reduce electrical resistivity of the system. The net effect is the invariant electrical resistivity of Ni, Fe, and Fe-4.5Si along melting boundary as observed in the experiments performed in this work.

Consequently it is postulated here that the electrical resistivity of Fe and Fe-4.5Si will remain invariant along the melting line to inner core  $P$  and  $T$  conditions because the typical change of  $\rho$  between fcc and hcp will not be observed in melt. The primary reason is very similar energy of both solid parent phases and the resulting ISROs concentration in liquid. This behaviour allows the inner core boundary to be used as the anchoring point to calculate thermal conductivity of liquid Fe-alloy using Wiedemann–Franz law. Moreover, based on the supporting evidence from recent literature, the prediction was made that the liquid Fe, alloyed with the small content of light elements in the outer core, will retain the same electrical resistivity along melting boundary as pure Fe and Fe-4.5 Si, up to ICB conditions.

The temperature uncertainty of the Fe-alloy at the core mantle boundary (CMB) dictates that the electrical resistivity of the core-side Fe alloy is bound between 120  $\mu\Omega\text{cm}$  (this study) and 150  $\mu\Omega\text{cm}$  as an upper limit due to the resistivity saturation (Gomi et al., 2013). However, considering that the temperature at the top-most OC exceeds the melting temperature of pure Fe, the  $\rho$  in that region is assumed to be 150  $\mu\Omega\text{cm}$ . This value of  $\rho$  is used for calculation of thermal conductivity ( $\kappa$ ) at CMB.

The calculated  $\kappa$  values in the outer core are predicated on the negligible role of inelastic electron scattering which would otherwise invalidate the Wiedemann–Franz law.

Thermal conductivity at the CMB and ICB calculated in this work is in agreement with recent lower estimates from literature. In comparison with the recent high estimates, the calculated adiabatic heat flow across the CMB points to the possibility that both thermally and compositionally driven convection may act simultaneously to generate the geodynamo.

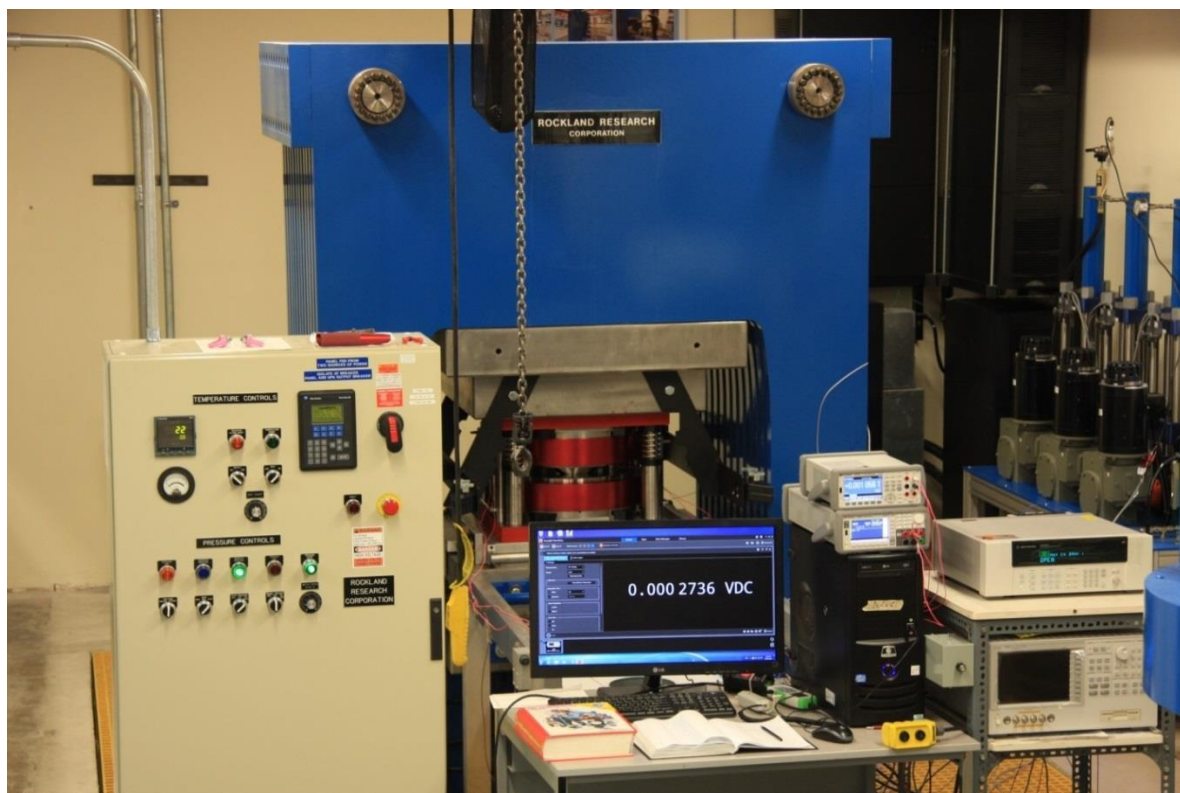
Currently, there is no theoretical framework to precisely quantify the effects of ISROs on the electrons scattering in liquid metals. Consequently, there is need for a theoretical treatment of ISRO effects on transport properties in liquid metals, especially at high pressure. The key unknown is the possibility of strong inelastic scattering at the core conditions, which may potentially reduce the value of the Lorenz number ( $L_0$ ) by up to  $0.65L_0$ . This would consequently reduce the current high estimates of the OC thermal conductivity calculated from the Wiedemann–Franz law to be roughly in line with most recent values of  $\kappa$  obtained in direct measurements on Fe (Konôpková et al., 2016). In such case,  $\kappa$  would likely correspond to earlier theoretical estimates by Stacey and Anderson (2001).

The postulates and predictions made in this work must also be also validated experimentally. The easiest experimental approach would be to measure the electrical resistivity of Fe-alloy with low C content and follow it up by a reasonable combination of ternary Fe-alloys (e.g., Zhang et al., 2016). If such experiment yields constant electrical resistivity of those alloys matching the results obtained in this study that would prove the main hypothesis of this work and would eliminate the compositional uncertainty considered in previous studies of  $\rho$  and  $\kappa$  in the outer core. Synchrotron-based measurements of evolution of the ISRO structures and clusters at increasing pressure would be beneficial to the development of theoretical framework for treatment of ISRO effects in planetary interiors.

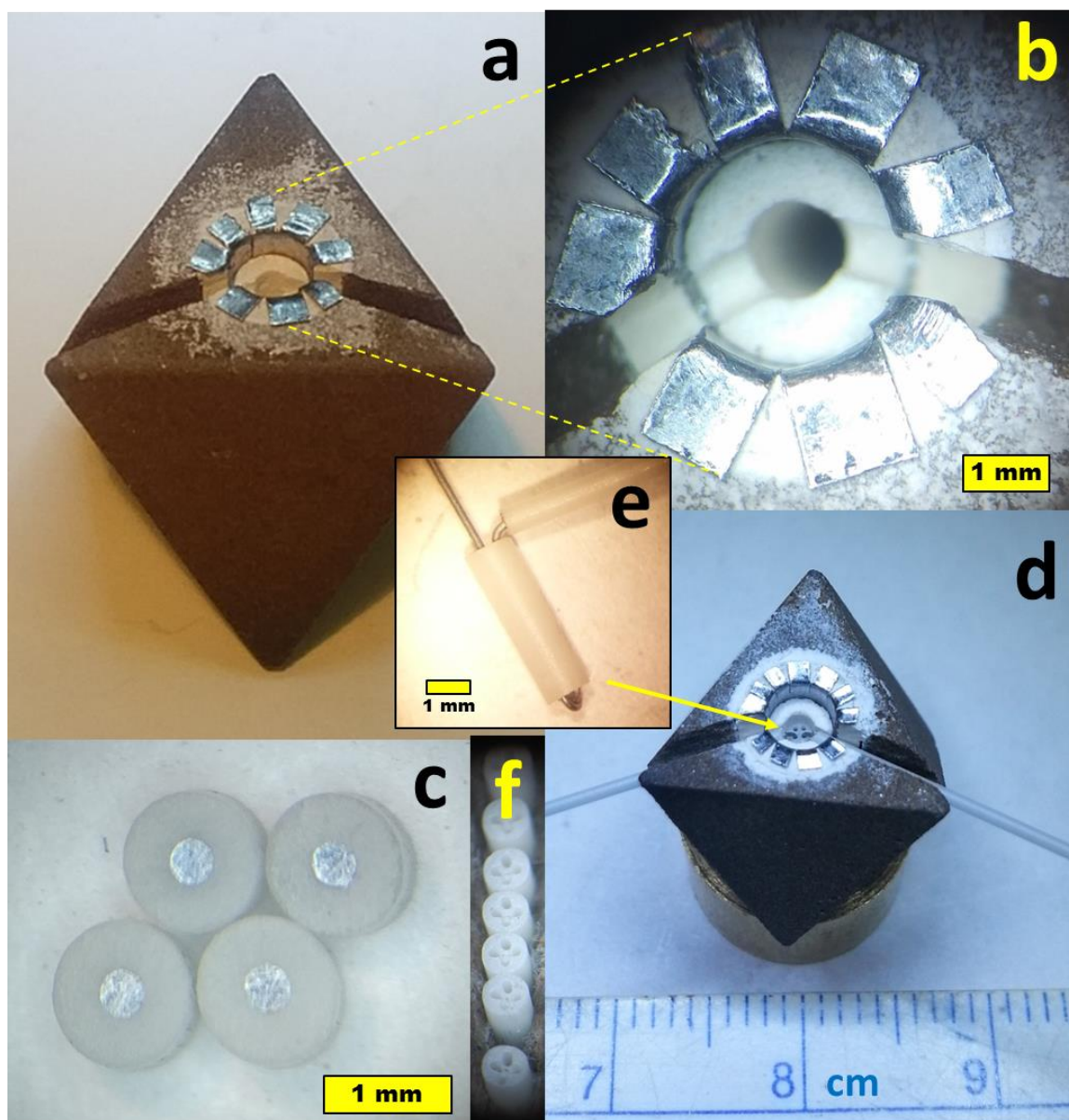
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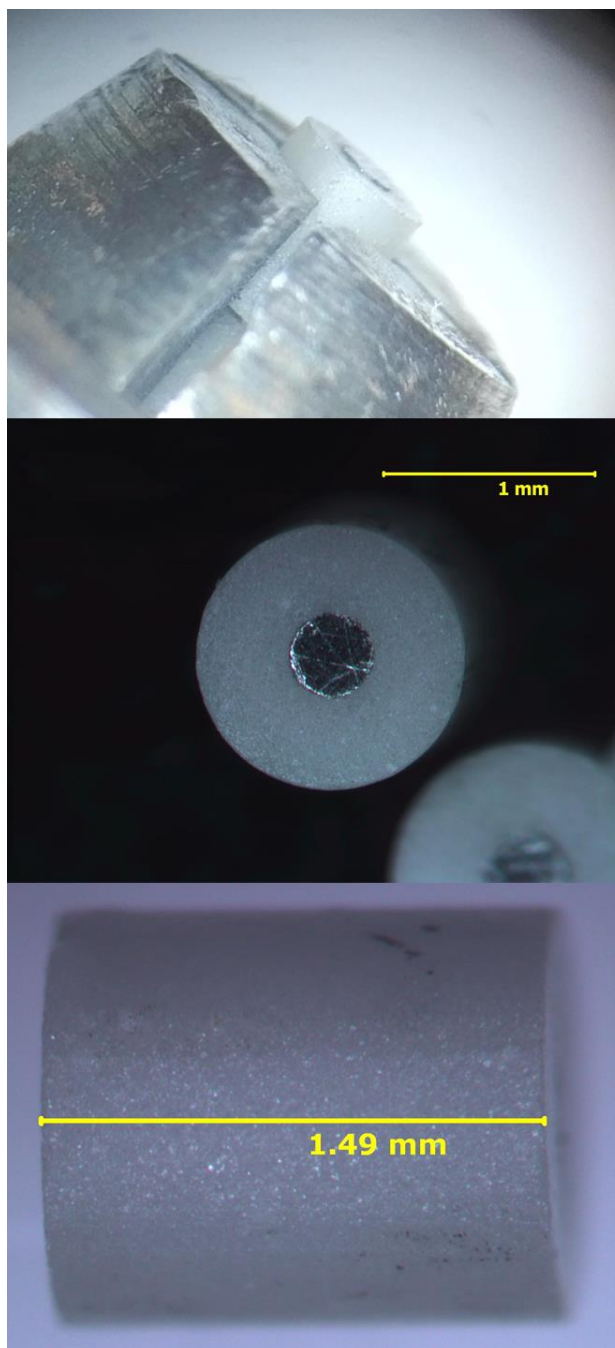
## Appendix



**Figure A. 1: 3000 ton high volume multi anvil press in the Department of Earth Sciences at Western University, London, Ontario, Canada.**

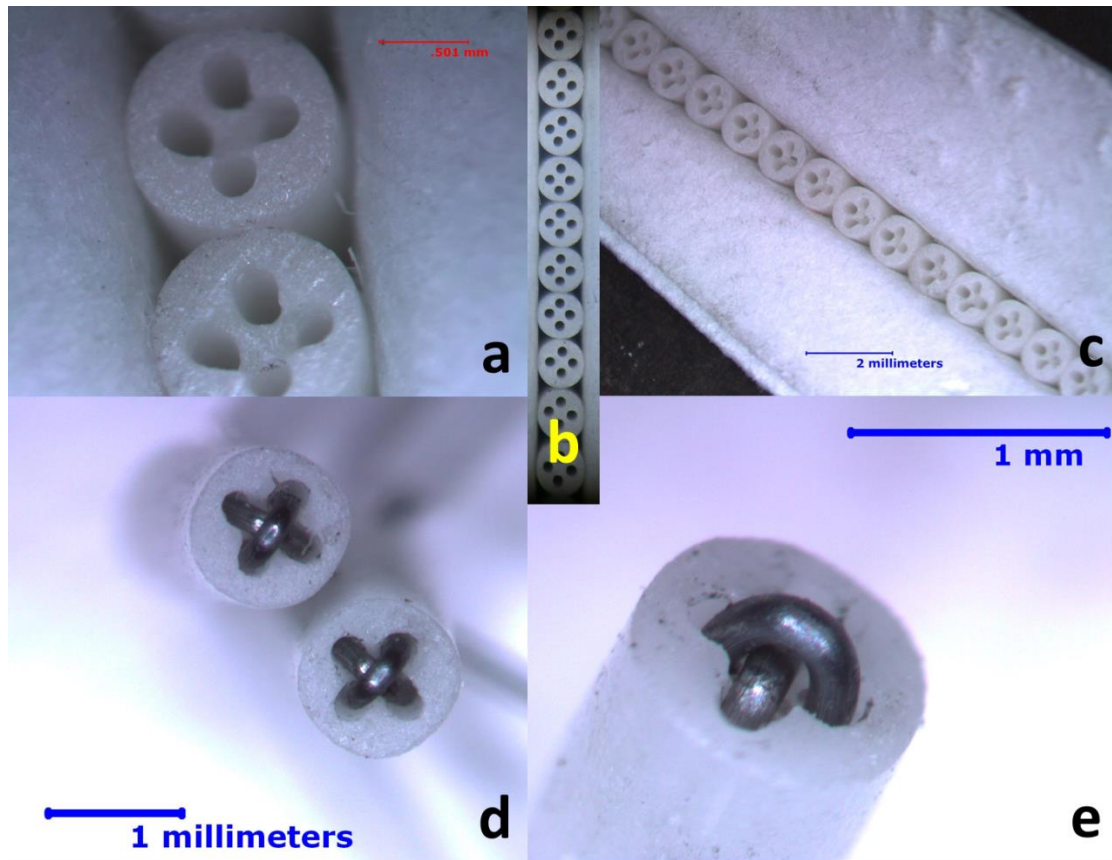


**Figure A.2:** The image in (a) shows the MgO octahedron, with the emplaced Re furnace, ZrO<sub>2</sub>-thermal insulator and boron nitride sleeve, which is seen clearly in panel (b). The sleeve hosts a thick walled ceramic tube with the emplaced sample (c). The 4-hole ceramic tube with the thermocouple wire is depicted in (f) during the assembly (e) and emplaced in octahedron cell during final assembly (d). A measuring tape is placed against the MgO pressure cell for the size comparison. The strip image in (f) shows 4-hole ceramic tubes during the fabrication. For the scale purpose, the diameter of each thick ceramic tube (c) with the emplaced sample is ~1 mm (as shown by the yellow scale bar).

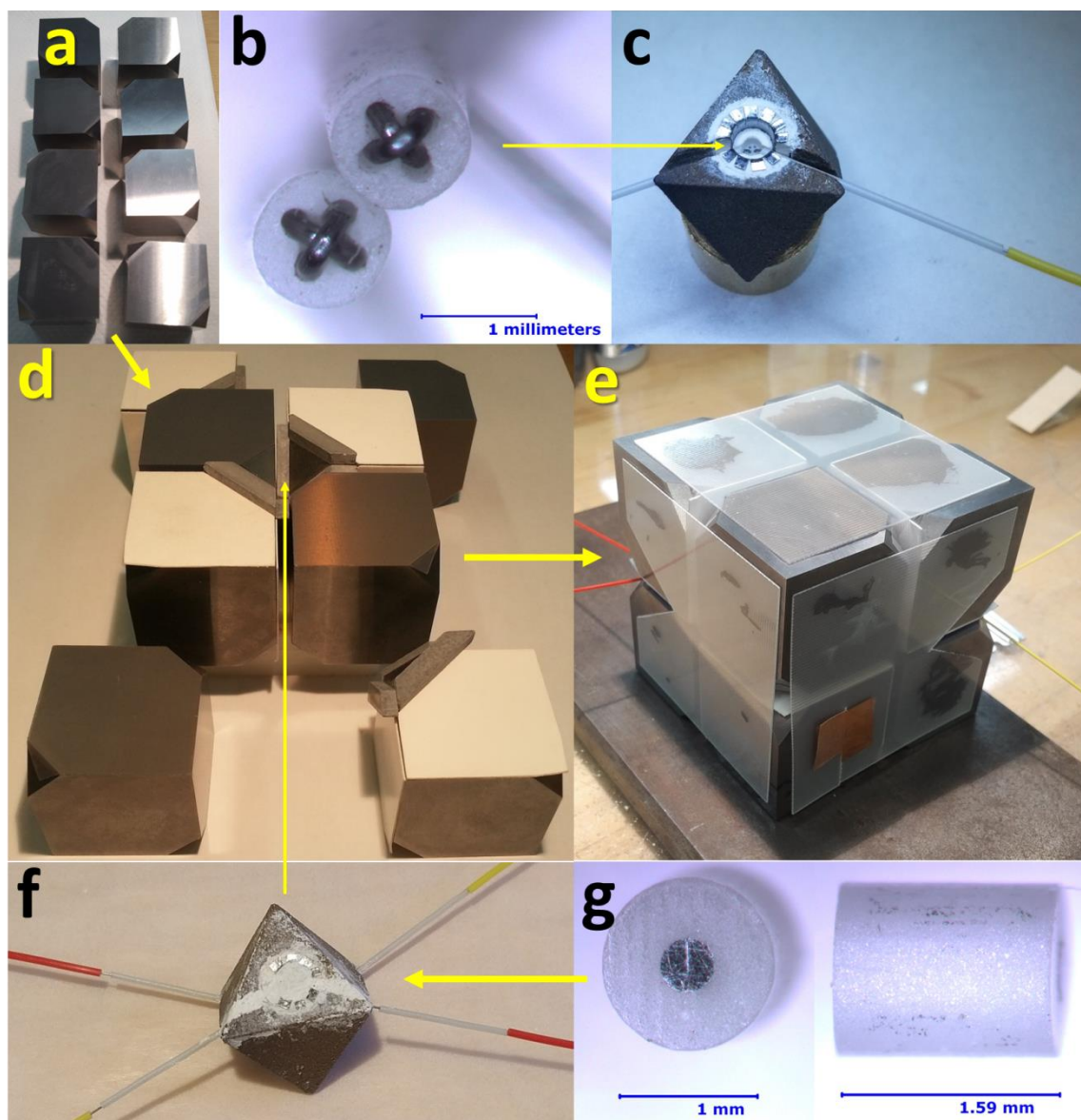


**Figure A.3:** The thick walled ceramic tube is shown during the fabrication process and the sample emplacement (top panel). The finished ceramic tube with the emplaced sample is shown from top down perspective (middle panel) and side view (bottom panel). The entire process of fabrication was done manually, with the tolerances approaching 0.01 mm.



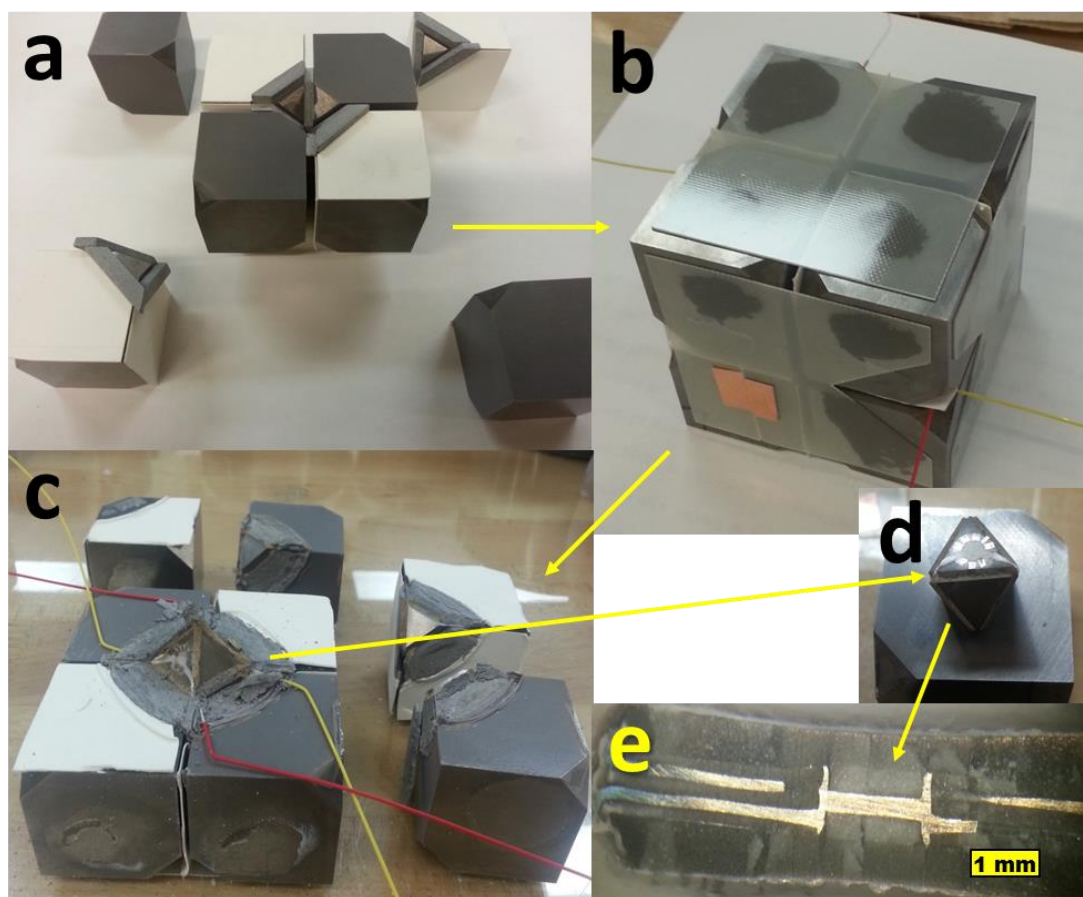


**Figure A.4:** The images in panels (a-c) depict the step in fabricating 4-hole ceramic tubes. Ceramic tubes with the emplaced thermocouple wires are shown in (d-e). This particular phase of fabrication requires that the precision must be maintained within 0.05 mm. The images also illustrate the experimental challenges of manually fabricating these parts to the same reproducible consistency.

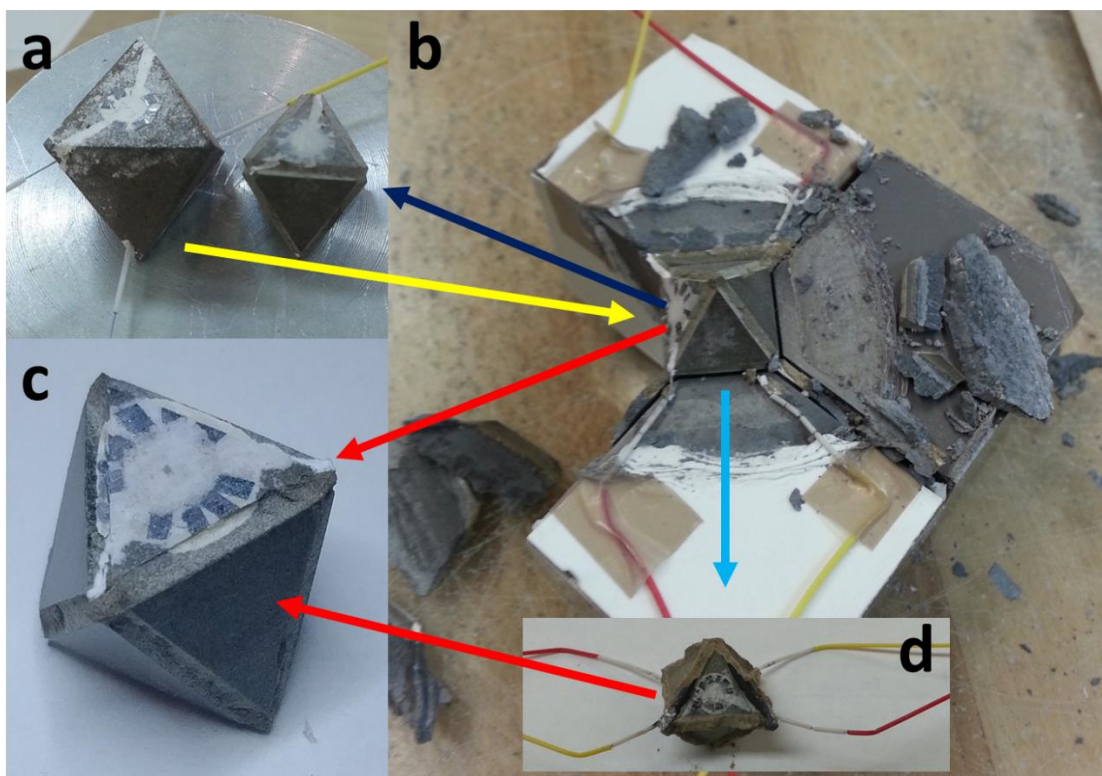


**Figure A.5:** Depicted is the assembly process (a-g), which includes cleaning and sterilizing WC cubes (a), and gasket emplacement (d), followed by the sample pressure cell emplacement (f) and the final assembly (e). Note that the panels are labeled in order of appearance, and not the order of assembly process. The 4-hole ceramic tubes with emplaced thermocouple wires (b), and their position in the MgO pressure cell and BN sleeve (c). Note that the thermocouple wire junction (b) is always oriented toward the sample in the middle of the octahedron (f). Final assembled and cemented cell is shown in (f) and the sample emplaced in the thick walled ceramic tube is shown in (g).

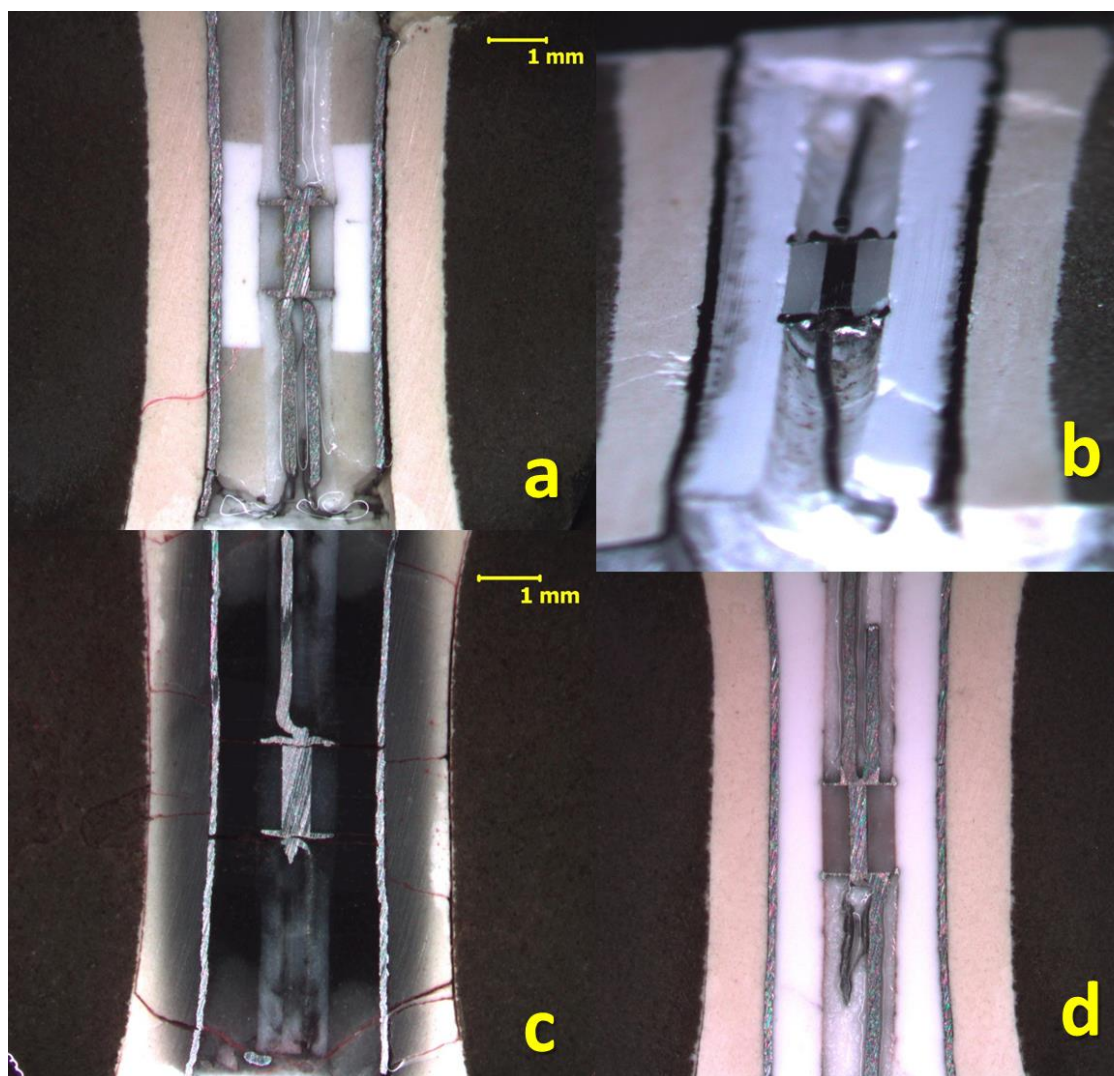




**Figure A.6:** For illustrative purpose, the assembly process is shown again (a-b), this time also displaying the recovered pressure MgO cell (c-d). The preserved geometry of the recovered sample obtained by sectioning the MgO cell is shown in (e). The length of the sample in (e) is 1.5 mm.



**Figure A.7:** The aim of this figure is to contrast the size reduction before (a) and after compression (b-d) to 7 GPa and to demonstrate good survivability of the post-experimentally recovered experimental cell (b-c).



**Figure A.8:** For illustrative purpose, figures (a-d) show several representative examples of recovered sample geometry and survivability of the samples compressed and heated from low (a,b,d) to high temperatures (c) during the method testing and technical development.

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### **Refereed Journal Articles**

**Silber, R. E.**, Secco, R. A., Yong, W. and Littleton, J. (2018) Electrical resistivity of liquid Fe to 12 GPa: Implications for heat flow in cores of terrestrial bodies, *Nature Scientific Reports*, 8, 10758, doi: 10.1038/s41598-018-28921-w

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Silber, E. A., Hocking, W. K., **Silber, R. E.** (2018) *Shock waves generated by overdense meteors in the mesosphere lower thermosphere*, *International Meteor Conference Proceedings*, Petnica, Serbia, 21-24 September, 2017

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**Silber, R. E.** (2013) *Potential for Measurement of Mesospheric Ozone Density from Overdense Meteor Trails with a Monostatic Meteor Radar*, *Electronic Thesis and Dissertation Repository*, Paper 1789, <http://ir.lib.uwo.ca/etd/1789>

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## **Talks and Presentations**

### **Nearly 40 presentations, only selected seven listed**

**Silber, R. E.**, Secco, R., Yong, W., Littleton, J. (2018) *Electrical Resistivity of Solid and Liquid Fe<sub>4.5</sub>wt%Si at 3-9 GPa*, AGU Fall Meeting, Washington, DC, USA, 10-14 December, 2018, abstract # 218453

Yong, W., Littleton, J., Secco, R., **Silber, R. E.** (2018) *Electrical Resistivity of Solid and Liquid Fe at 14 - 24 GPa*, AGU Fall Meeting, Washington, DC, USA, 10-14 December, 2018, abstract # 218453

Silber, E. A., Gritsevich, M., **Silber, R. E.**, Butka, P. (2018) *The production of nitric oxide by centimetre-sized meteoroids in the upper atmosphere*, European Planetary Science Congress 2018, Berlin, Germany, September 16 – 21, 2018, abstract #582.

Silber, E. A., Gritsevich, M., **Silber, R. E.** (2018) *Nitric oxide production by centimeter-sized meteoroids impacting the Earth's atmosphere*, 81st Annual Meeting of The Meteoritical Society, Moscow, Russia, July 22-27, 2018, abstract #6183.

**Silber, R. E.**, Secco, R., Ezenwa, I., Yong, W., Littleton, J. (2017) *Fe, Co, Ni: Electrical Resistivity Along their Melting Boundaries*, AGU Fall Meeting, New Orleans, Louisiana, USA, 11-15 December, 2017, abstract # 218453

Silber, E. A., **Silber, R. E.**, Hocking, W. K. (2017) *Shock waves generated by overdense meteors in the mesosphere lower thermosphere*, International Meteor Conference, Petnica, Serbia, 21-24 September, 2017

Secco, R., **Silber, R. E.**, Ezenwa, I., Yong, W., Littleton, J. (2017) *Electrical Resistivity of Fe, Co and Ni along their melting boundaries*, 55th EHPRG Meeting, Poznan, Poland, 3 – 8 September, 2017

**Silber, R. E.**, Hocking, W. K., Silber, E. A., Gritsevich, M., Niculescu, M. L. (2017) *Detection and Characterization of Meteor Shockwaves Using Radar Observed Meteor Head Echo/Height Correlation*, 32nd URSI GASS, 19-26 August 2017, Montreal, Quebec, Canada

Hocking, W. K., **Silber, R. E.** (2017) *Radio-wave scattering by meteors and the dependence on meteor trail structure*, 32nd URSI GASS, 19-26 August 2017, Montreal, Quebec, Canada (invited talk)

**Silber, R. E.**, Silber, E. A., Gritsevich, M. (2017), *On detection of shockwaves generated by overdense meteors*, The 80th Annual Meeting of the Meteoritical Society, 23-28 July, 2017, Santa Fe, New Mexico, USA, abstract #6256

**Silber, R. E.**, Silber, E. A., Gritsevich, M., Niculescu, M. L., Hocking, W. K. (2017), *On the mechanism of early rapid removal of electrons from postadiabatically expanding overdense meteor trains*, The 80th Annual Meeting of the Meteoritical Society, 23-28 July, 2017, Santa Fe, New Mexico, USA, abstract # 6317

Moreno-Ibáñez, M., Gritsevich, M., Lyytinen, E., Silber, E. A., **Silber, R. E.**, Trigo-Rodríguez, J. M. (2017) *Revised masses for the Canadian meteor network fireballs*, The

80th Annual Meeting of the Meteoritical Society, 23-28 July, 2017, Santa Fe, New Mexico, USA, abstract # 6318

Hocking, W.K., **Silber, R. E.**, Silber, E. A. (2017) *Impact of Ozone and Oxygen on Early Stage Decay of Transitionally- and Over-dense Meteor Trails*, The 15th International Workshop on Technical and Scientific Aspects of MST Radar and the 18th EISCAT International Symposium (MST15/iMST2/EISCAT18), held in The National Institute of Polar Research (NIPR), May 26-31, 2017, Tachikawa, Tokyo, Japan, paper M7-8

**Silber, R. E.**, Secco, R. A. and Yong, W. (2017) *Electrical Resistivity of Molten Ni at High Pressures and Comparison with Preliminary Results on Liquid Fe*, CAP Congress, May 28 - June 2, 2017, Kingston, ON, Canada, abstract #1591

**Silber, R. E.**, Hocking, W. K., Silber, E. A., Gritsevich, M. (2017) *On the Possibility of Constraining Bright Meteor Shock Wave Forming Altitudes – Theoretical Consideration of Relationship to Radar Observed Meteor Head Echo Termination Heights in MLT*, CAP Congress, May 28 - June 2, 2017, Kingston, ON, Canada, abstract #1578

**Silber, R. E.**, Secco, R. A. and Yong, W. (2017) *Electrical Resistivity of Molten Ni at High Pressures*, Fallona Interdisciplinary Showcase, Western University, January 16, 2017

Gritsevich, M., Silber, E. A., Lyytinen, E., Moreno-Ibáñez, M., Trigo-Rodríguez, J. M., Muinonen, K., Penttilä, A., **Silber, R. E.** (2017) *A New Approach to Estimate Meteoroid Impact Hazard Based on Atmospheric Trajectory Analysis*, LPSC 48, held March 20–24, 2017, The Woodlands, TX, USA, abstract 2471

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